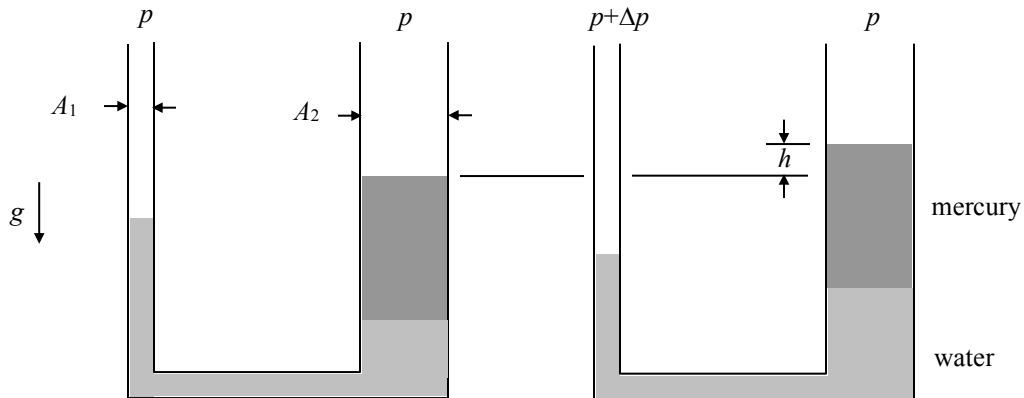


Determine the deflection,  $h$ , in the manometer shown below in terms of  $A_1$ ,  $A_2$ ,  $\Delta p$ ,  $g$ , and  $\rho_{\text{H}_2\text{O}}$ . Determine the sensitivity of this manometer. The manometer sensitivity,  $s$ , is defined here as the change in the elevation difference,  $h$ , with respect to a change in the applied pressure,  $\Delta p$ :

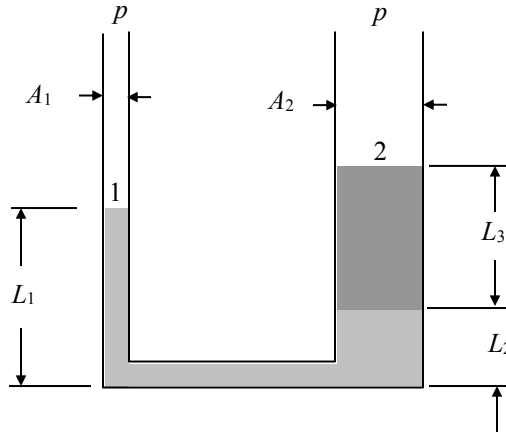
$$s \equiv \frac{dh}{d(\Delta p)}$$

Manometers with larger sensitivity will give larger changes in  $h$  for the same  $\Delta p$ .



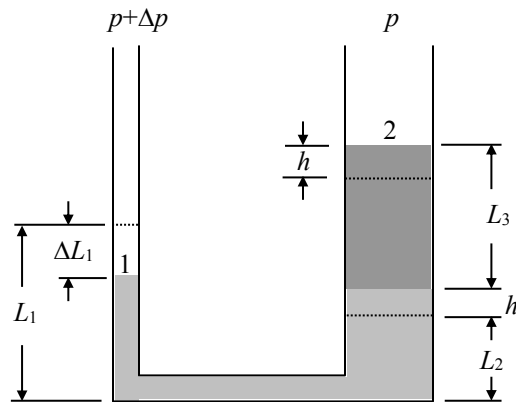
SOLUTION:

First analyze the initial system.



$$\begin{aligned} \underline{p_2} &= \underline{p_1} + \rho_{\text{H}_2\text{O}} g L_1 - \rho_{\text{H}_2\text{O}} g L_2 - \rho_{\text{Hg}} g L_3 \\ \underline{p} &= \underline{p} \\ L_1 - L_2 &= S G_{\text{Hg}} L_3 \end{aligned} \quad (1)$$

Now analyze the displaced system.



$$\begin{aligned} \underline{p_2} &= \underline{p_1} + \rho_{\text{H}_2\text{O}} g (L_1 - \Delta L_1) - \rho_{\text{H}_2\text{O}} g (L_2 + h) - \rho_{\text{Hg}} g L_3 \\ \underline{p} &= \underline{p + \Delta p} \\ -\frac{\Delta p}{\rho_{\text{H}_2\text{O}} g} &= (L_1 - \Delta L_1 - L_2 - h) - S G_{\text{Hg}} L_3 \end{aligned} \quad (2)$$

Substitute Eqn. (1) into Eqn. (2).

$$\begin{aligned} -\frac{\Delta p}{\rho_{\text{H}_2\text{O}} g} &= (L_1 - \Delta L_1 - L_2 - h) - (L_1 - L_2) \\ \frac{\Delta p}{\rho_{\text{H}_2\text{O}} g} &= \Delta L_1 + h \end{aligned} \quad (3)$$

Note also that the displaced volume will also be conserved.

$$\Delta L_1 A_1 = h A_2$$

$$\Delta L_1 = h \frac{A_2}{A_1} \quad (4)$$

Substitute Eqn. (4) into Eqn. (3).

$$\frac{\Delta p}{\rho_{\text{H}_2\text{O}} g} = h \frac{A_2}{A_1} + h$$

$$h = \frac{1}{1 + \frac{A_2}{A_1}} \left( \frac{\Delta p}{\rho_{\text{H}_2\text{O}} g} \right) \quad (5)$$

Note that the density of the secondary fluid (i.e., mercury) does not factor into the displaced height.

The manometer sensitivity,  $s$ , is defined as the change in the elevation difference,  $h$ , with respect to a change in the applied pressure,  $\Delta p$ .

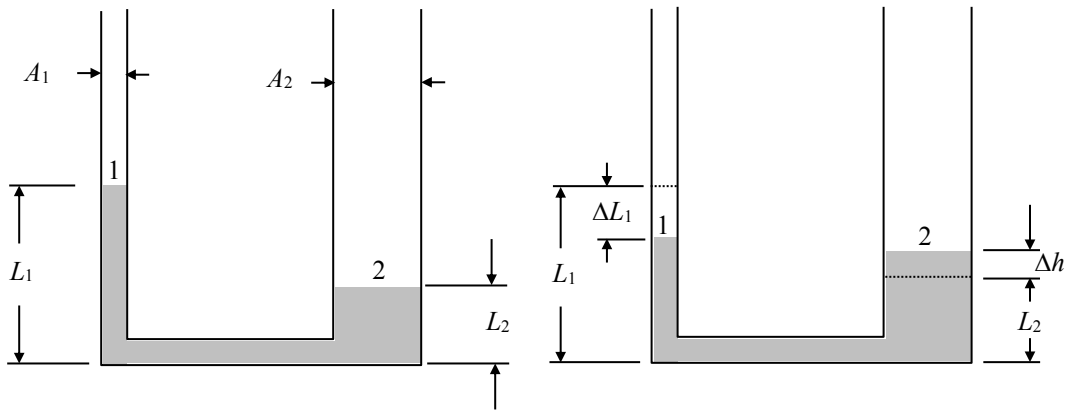
$$s \equiv \frac{dh}{d(\Delta p)} \quad (6)$$

Manometers with larger sensitivity will give larger changes in  $h$  for the same  $\Delta p$ . Using Eqn. (5), the sensitivity of this manometer is:

$$s = \frac{1}{1 + \frac{A_2}{A_1}} \left( \frac{1}{\rho_{\text{H}_2\text{O}} g} \right) \quad (7)$$

To increase the manometer's sensitivity, one should decrease the area ratio,  $A_2/A_1$ , and use a lower density fluid than water.

Why doesn't Eqn. (5) involve the properties of mercury? In fact, the properties of the secondary fluid (*i.e.* the mercury) do influence the system. Consider the change in potential energy of the water during the displacement as shown in the plots below.



$$\begin{aligned} \Delta PE_{\text{left, H}_2\text{O}} &= \underbrace{\rho_{\text{H}_2\text{O}} A_1 (L_1 - \Delta L_1)}_{=m_{\text{after}}} g \underbrace{\frac{1}{2} (L_1 - \Delta L_1)}_{=L_{\text{CM, after}}} - \underbrace{\rho_{\text{H}_2\text{O}} A_1 L_1}_{=m_{\text{before}}} g \underbrace{\frac{1}{2} L_1}_{=L_{\text{CM, before}}} \\ &= \frac{1}{2} \rho_{\text{H}_2\text{O}} g A_1 (L_1 - \Delta L_1)^2 - \frac{1}{2} \rho_{\text{H}_2\text{O}} g A_1 L_1^2 \\ &= \frac{1}{2} \rho_{\text{H}_2\text{O}} g A_1 (-2L_1 \Delta L_1 + \Delta L_1^2) \end{aligned}$$

$$\begin{aligned}
\Delta PE_{\text{right,H}_2\text{O}} &= \underbrace{\rho_{\text{H}_2\text{O}} A_2 (L_2 + h)}_{=m_{\text{after}}} g \underbrace{\frac{1}{2} (L_2 + h)}_{=L_{\text{CM,after}}} - \underbrace{\rho_{\text{H}_2\text{O}} A_2 L_2}_{=m_{\text{before}}} g \underbrace{\frac{1}{2} L_2}_{=L_{\text{CM,before}}} \\
&= \frac{1}{2} \rho_{\text{H}_2\text{O}} g A_2 (L_2 + h)^2 - \frac{1}{2} \rho_{\text{H}_2\text{O}} g A_2 L_2^2 \\
&= \frac{1}{2} \rho_{\text{H}_2\text{O}} g A_2 (2L_2 h + h^2) \\
\Delta PE_{\text{total,H}_2\text{O}} &= \frac{1}{2} \rho_{\text{H}_2\text{O}} g A_1 (-2L_1 \Delta L_1 + \Delta L_1^2) + \frac{1}{2} \rho_{\text{H}_2\text{O}} g A_2 (2L_2 h + h^2) \\
&= \frac{1}{2} \rho_{\text{H}_2\text{O}} g (-2L_1 \Delta L_1 A_1 + \Delta L_1^2 A_1 + 2L_2 h A_2 + h^2 A_2)
\end{aligned}$$

Substitute Eqn. (4).

$$\begin{aligned}
\Delta PE_{\text{total,H}_2\text{O}} &= \frac{1}{2} \rho_{\text{H}_2\text{O}} g \left[ -2L_1 h \frac{A_2}{A_1} A_1 + h^2 \left( \frac{A_2}{A_1} \right)^2 A_1 + 2L_2 h A_2 + h^2 A_2 \right] \\
\Delta PE_{\text{total,H}_2\text{O}} &= \frac{1}{2} \rho_{\text{H}_2\text{O}} g A_2 h \left[ \left( 1 + \frac{A_2}{A_1} \right) h + 2(L_2 - L_1) \right] \quad (8)
\end{aligned}$$

The change in potential energy of the water will depend not only on  $h$ , but also on the initial state of the water,  $L_2-L_1$ . From Eqn. (1) we see that  $L_1-L_2$  is related to the specific gravity of the secondary fluid.

Another way to solve the problem is to apply the 1<sup>st</sup> Law of Thermodynamics to the system (consisting of the fluids within the manometer):

$$\Delta E_{\text{system}} = Q_{\text{into system}} + W_{\text{on system}} \quad (9)$$

where  $Q_{\text{into system}} = 0$  (assuming adiabatic conditions – a reasonable assumption) and the only work on the system is the pressure work causing the displacement:

$$W_{\text{pressure on system}} = (p + \Delta p) A_1 \Delta L_1 - p A_2 h \quad (10)$$

Note that using Eqn. (4), Eqn. (10) becomes:

$$W_{\text{pressure on system}} = \Delta p A_1 \Delta L_1 \quad (11)$$

The total change in the system's energy (which is the potential energy) is:

$$\begin{aligned}
\Delta PE_{\text{left}} &= \underbrace{\rho_{\text{H}_2\text{O}} A_1 (L_1 - \Delta L_1)}_{=m_{\text{after}}} g \underbrace{\frac{1}{2} (L_1 - \Delta L_1)}_{=L_{\text{CM,after}}} - \underbrace{\rho_{\text{H}_2\text{O}} A_1 L_1}_{=m_{\text{before}}} g \underbrace{\frac{1}{2} L_1}_{=L_{\text{CM,before}}} \\
&= \frac{1}{2} \rho_{\text{H}_2\text{O}} A_1 g (L_1^2 - 2L_1 \Delta L_1 + \Delta L_1^2 - L_1^2) \\
&= -\frac{1}{2} \rho_{\text{H}_2\text{O}} A_1 g (2L_1 \Delta L_1 - \Delta L_1^2)
\end{aligned} \quad (12)$$

$$\begin{aligned}
\Delta PE_{\text{right}} &= \underbrace{\rho_{\text{H}_2\text{O}} A_2 (L_2 + h) g \frac{1}{2} (L_2 + h) - \rho_{\text{H}_2\text{O}} A_2 L_2 g \frac{1}{2} L_2}_{=\Delta PE_{\text{H}_2\text{O}}} + \underbrace{\rho_{\text{Hg}} A_2 L_3 gh}_{\Delta PE_{\text{Hg}}} \\
&= \frac{1}{2} \rho_{\text{H}_2\text{O}} A_2 g (L_2^2 + 2L_2 h + h^2 - L_2^2) + \rho_{\text{Hg}} A_2 L_3 gh \\
&= \frac{1}{2} \rho_{\text{H}_2\text{O}} A_2 g (2L_2 h + h^2) + \rho_{\text{Hg}} A_2 L_3 gh
\end{aligned}$$

$$\begin{aligned}
\Delta PE_{\text{system}} &= \Delta PE_{\text{left}} + \Delta PE_{\text{right}} \\
&= -\frac{1}{2} \rho_{\text{H}_2\text{O}} A_1 g (2L_1 \Delta L_1 - \Delta L_1^2) + \frac{1}{2} \rho_{\text{H}_2\text{O}} A_2 g (2L_2 h + h^2) + \rho_{\text{Hg}} A_2 L_3 gh \quad (13)
\end{aligned}$$

Substitute Eqns. (11) and (13) into Eqn. (9) gives:

$$-\frac{1}{2} \rho_{\text{H}_2\text{O}} A_1 g (2L_1 \Delta L_1 - \Delta L_1^2) + \frac{1}{2} \rho_{\text{H}_2\text{O}} A_2 g (2L_2 h + h^2) + \rho_{\text{Hg}} A_2 L_3 gh = \Delta p A_1 \Delta L_1 \quad (14)$$

$$\frac{\Delta p}{\rho_{\text{H}_2\text{O}} g} = -L_1 + \frac{1}{2} \Delta L_1 + \frac{A_2}{A_1} \frac{1}{\Delta L_1} \left( L_2 h + \frac{1}{2} h^2 + SG_{\text{Hg}} L_3 h \right) \quad (15)$$

Substitute Eqn. (1).

$$\begin{aligned}\frac{\Delta p}{\rho_{\text{H}_2\text{O}}g} &= -L_1 + \frac{1}{2}\Delta L_1 + \frac{A_2}{A_1} \frac{1}{\Delta L_1} \left( L_2 h + \frac{1}{2}h^2 + L_1 h - L_2 h \right) \\ &= -L_1 + \frac{1}{2}\Delta L_1 + \frac{1}{2} \frac{A_2}{A_1} \frac{h^2}{\Delta L_1} + \frac{A_2}{A_1} \frac{L_1 h}{\Delta L_1}\end{aligned}\quad (16)$$

Substitute Eqn. (4) and simplify:

$$\frac{\Delta p}{\rho_{\text{H}_2\text{O}}g} = -L_1 + \frac{1}{2}h \frac{A_2}{A_1} + \frac{1}{2} \frac{A_2}{A_1} \frac{h^2}{h \frac{A_2}{A_1}} + \frac{A_2}{A_1} \frac{L_1 h}{h \frac{A_2}{A_1}} = -L_1 + \frac{1}{2}h \frac{A_2}{A_1} + \frac{1}{2}h + L_1 = \frac{1}{2} \left( 1 + \frac{A_2}{A_1} \right) h \quad (17)$$

$$\therefore h = \frac{2}{1 + \frac{A_2}{A_1}} \left( \frac{\Delta p}{\rho_{\text{H}_2\text{O}}g} \right) \quad (\text{This is the same as Eqn. (5)!})$$