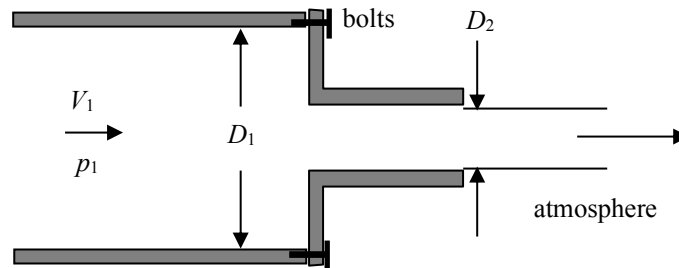
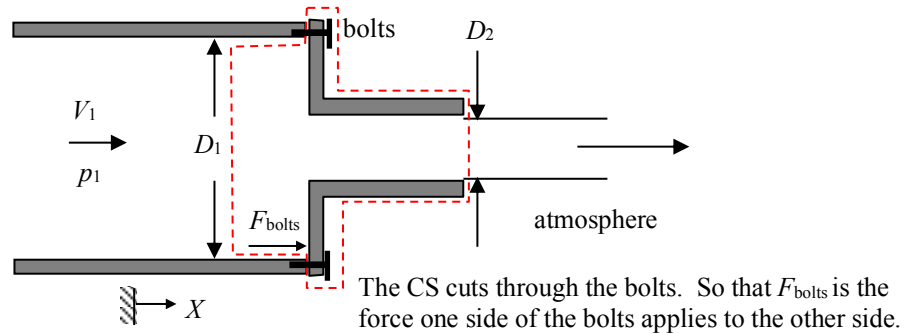


A fluid enters a horizontal, circular cross-sectioned, sudden contraction nozzle. At section 1, which has diameter D_1 , the velocity is uniformly distributed and equal to V_1 . The gage pressure at 1 is p_1 . The fluid exits into the atmosphere at section 2, with diameter D_2 . Determine the force in the bolts required to hold the contraction in place. Neglect gravitational effects and assume that the fluid is inviscid.



SOLUTION:

Apply conservation of linear momentum in the X -direction to the fixed control volume shown below.



$$\frac{d}{dt} \int_{CV} u_X \rho dV + \int_{Cs} u_X (\rho \mathbf{u}_{rel} \cdot d\mathbf{A}) = F_{B,X} + F_{S,X} \quad (1)$$

where

$$\frac{d}{dt} \int_{CV} u_X \rho dV = 0 \quad (\text{steady flow})$$

$$\int_{Cs} u_X (\rho \mathbf{u}_{rel} \cdot d\mathbf{A}) = \rho V_1 \left(V_1 \hat{\mathbf{i}} \cdot -\frac{\pi D_1^2}{4} \hat{\mathbf{i}} \right) + \rho V_2 \left(V_2 \hat{\mathbf{i}} \cdot \frac{\pi D_2^2}{4} \hat{\mathbf{i}} \right) = -\rho V_1^2 \frac{\pi D_1^2}{4} + \rho V_2^2 \frac{\pi D_2^2}{4}$$

(Note that V_2 is unknown for now.)

$$F_{B,X} = 0$$

$$F_{S,X} = p_{1,\text{gage}} \frac{\pi D_1^2}{4} + F_{\text{bolts}}$$

(Note that $p_{2,\text{gage}} = 0$ since $p_{2,\text{abs}} = p_{\text{atm}}$. We could have also worked the problem using absolute pressures everywhere. The pressure force on the left hand side would be $p_{1,\text{abs}} \pi D_1^2 / 4$ and the pressure force on the right hand side would be $p_{\text{atm}} \pi D_1^2 / 4$ (note that the diameter is D_1 and not D_2 .)

Substitute and re-arrange.

$$-\rho V_1^2 \frac{\pi D_1^2}{4} + \rho V_2^2 \frac{\pi D_2^2}{4} = p_{1,\text{gage}} \frac{\pi D_1^2}{4} + F_{\text{bolts}}$$

$$F_{\text{bolts}} = -\rho V_1^2 \frac{\pi D_1^2}{4} + \rho V_2^2 \frac{\pi D_2^2}{4} - p_{1,\text{gage}} \frac{\pi D_1^2}{4} \quad (2)$$

To determine V_2 , apply conservation of mass to the same control volume.

$$\frac{d}{dt} \int_{CV} \rho dV + \int_{Cs} \rho \mathbf{u}_{rel} \cdot d\mathbf{A} = 0 \quad (3)$$

where

$$\begin{aligned} \frac{d}{dt} \int_{CV} \rho dV &= 0 \\ \int_{Cs} \rho \mathbf{u}_{rel} \cdot d\mathbf{A} &= -\rho V_1 \frac{\pi D_1^2}{4} + \rho V_2 \frac{\pi D_2^2}{4} \end{aligned}$$

Substitute and simplify.

$$\begin{aligned} -\rho V_1 \frac{\pi D_1^2}{4} + \rho V_2 \frac{\pi D_2^2}{4} &= 0 \\ V_2 &= V_1 \left(\frac{D_1}{D_2} \right)^2 \end{aligned} \quad (4)$$

Substitute Eqn. (4) into Eqn. (2) and simplify.

$$\begin{aligned} F_{bolts} &= -\rho V_1^2 \frac{\pi D_1^2}{4} + \rho V_1^2 \left(\frac{D_1}{D_2} \right)^4 \frac{\pi D_2^2}{4} - p_{1,gage} \frac{\pi D_1^2}{4} \\ F_{bolts} &= \rho V_1^2 \frac{\pi D_1^2}{4} \left[\left(\frac{D_1}{D_2} \right)^2 - 1 \right] - p_{1,gage} \frac{\pi D_1^2}{4} \end{aligned} \quad (5)$$

Note that F_{bolts} was assumed to be positive when acting in the $+X$ direction (causing compression in the bolts). If $F_{bolts} < 0$ then the bolts will be in tension.