### 3.5. Properties

In order to analyze real-world systems, we must be able to relate describe the properties and the relation between the properties of systems. In this section we examine how properties are presented and how they're related for a few important classes of materials. First, however, we must define a few terms:

- The phase of a substance has homogeneous chemical composition and physical structure. The three phases of matter are solid, liquid, and vapor.
- A pure substance is one that is uniform and invariable in chemical composition. A pure substance can exist in more than one phase, but all of the phases must have identical chemical compositions.
- A simple, compressible system is one in which electrical, magnetic, surface tension, gravitational, and motion effects are negligible. Systems consisting of pure water or uniform mixtures of nonreacting gases are examples of simple, compressible systems. The state principle states that any two independent intensive thermodynamic properties will uniquely define the system's state. If additional effects are significant, e.g., gravitational forces and accelerations, then additional properties are required, e.g., elevation and velocity.


## $p-v-T$ Diagrams

For simple, compressible systems, we can show the relationship between pressure, specific volume, and temperature in (3D) $p-v-T$ diagrams (Figures 3.12 and 3.13 ). It's most convenient, however, to show (2D) projections of these diagrams onto the $p-T, p-v$, and $T-v$ planes. Please refer to the following two figures in the following discussion of the important features of these diagrams.

- Three single-phase regions can be identified on the plots: solid, liquid, and vapor.
- The state in these regions is fixed by two independent properties, e.g., $(p, v),(p, T)$, or $(v, T)$.
- Above a critical pressure, temperature, and specific volume, known as the critical point, the difference between liquid and vapor is no longer discernible. The properties at the critical point are referred to as critical properties. Values for the critical pressure and temperature may often be found in the back of textbooks (e.g., Table A-1 in Moran et al., 8th ed.) or online.
- Three two-phase regions in which two phases exist in equilibrium can also be identified in the plots. These regions correspond to solid-vapor, solid-liquid, and liquid-vapor.
- These regions correspond to situations involving melting or freezing (transition from solid to liquid or liquid to solid, respectively); vaporization (boiling - turning to vapor by increasing the temperature while holding pressure constant, or cavitation - turning to vapor by decreasing the pressure while holding the temperature constant) or condensation (transition from vapor to a liquid); and sublimation (transition from a solid to a vapor).
- In these two-phase regions, the pressure and temperature are not independent. Hence, to define a state we need the specific volume, $v$, and either the pressure or the temperature, ( $p$ or $T$ ).
- A single three-phase line, along which solid, liquid, and vapor exist in equilibrium. This line is referred to as the triple line.
- The state at which a phase change begins is known as a saturation state.
- The two-phase (liquid-vapor) dome-shaped region is known as the vapor dome.
- The lines bordering the vapor dome are known as the saturated liquid and saturated vapor lines.
- The point at the top of the dome is known as the critical point, which is at the critical temperature, $T_{c}$, and critical pressure, $p_{c}$, and critical specific volume, $v_{c}$. The critical temperature is the maximum temperature at which liquid and vapor phases can co-exist in equilibrium.
- The projection of the $p-v-T$ diagram onto the $p-T$ plane is known as a phase diagram.
- The two-phase regions are projected as lines in this view.
- The saturation temperature is the temperature at which a phase change takes place at a given pressure. The corresponding pressure is known as the saturation pressure. For each saturation pressure there is a unique corresponding saturation temperature, hence, $T$ and $p$ are not independent during a change of phase.
- The triple line projects to the triple point in a phase diagram.


## In this projection,

- two-phase regions reduce to lines
- triple line reduces to a point $T$ and $p$ are related in the two-phase regions, i.e., there is a unique pressure at a given temperature in the two-phase regions (corresponding to lines in this projection)
(a)


(b)

(c)

Figure 3.12. $p-v-T$ surface and projections for a substance that expands on freezing. (a) 3D view, (b) phase diagram, (c) $p-v$ diagram. Figure 3.2 from Moran et al., 7 th ed.

- The triple point of water occurs at 273.16 K and 0.6113 kPa (abs).
- For a substance that expands on freezing, e.g., water, the solid-liquid phase line tilts toward the left. For a substance that contracts upon freezing, the solid-liquid saturation line tilts toward the right.
- The projection of the $p-v-T$ diagram onto the $p-v$ plane is also useful (Figure 3.14).
- Lines of constant temperature are referred to as isotherms.
- For $T<T_{c}$, the pressure remains constant in the two-phase regions along an isotherm. In the single-phase regions along an isotherm, the pressure decreases with increasing $v$.
- The isotherm is at an inflection point when passing through the critical point.
- The projection of the $p-v-T$ diagram onto the $T-v$ plane is frequently used (Figure 3.15).
- Lines of constant pressure are known as isobars.
- The temperature remains constant with pressure along an isobar in the two-phase region.
- In the single-phase regions, the temperature increases with increasing specific volume along an isobar.
- For pressures greater than the critical pressure, the temperature increases continuously with increasing specific volume along an isobar.

The $p-v-T$ sketches shown in the previous figures are distorted from what they actual plots look like. Figure 3.16 shows an example of a $p-v$ plot for water drawn to scale. Note the use of logarithmic axes.


Figure 3.13. $p-v-T$ surface and projections for a substance that contracts on freezing. (a) 3D view, (b) phase diagram, (c) $p-v$ diagram. Figure 3.2 from Moran et al., 7th ed.


Figure 3.14. Sketch of a $p-v$ plot.


Figure 3.15. Sketch of a $T-v$ plot.


Figure 3.16. A $p-v$ plot for water. Note the logarithmic scales.

Now consider the $T-v$ projection more closely and, specifically, the region near the vapor dome as shown in Figure 3.17.

- The phase of a substance to the left of the vapor dome is known as a liquid, subcooled liquid, or compressed liquid (CL).
- Point "l" in the figure is in this liquid region.
- The term "subcooled" refers to the fact that along an isobar, the temperature is too low for the substance to be a vapor.


Figure 3.17. Sketch of a $T$ - $v$ diagram. Figure 3.3 from Moran et al., 7th ed.

- The term "compressed" refers to the fact that at a given temperature, the pressure is larger than the pressure required to reach the saturation state. The pressure increases moving upward and toward the left across the isobars.
- The phase of a substance to the right of the vapor dome is known as a superheated vapor (SHV).
- The term "superheated" refers the fact that the temperature is larger than what would be required to reach a liquid-vapor saturation state along a given isobar.
- Point "s" is in the superheated vapor region.
- Within the vapor dome (the two-phase, or saturated (S) region), both liquid and vapor can exist in equilibrium. In order to specify how much of the substance is in liquid form versus vapor form, we define the quality of the mixture, x , which is the mass fraction of vapor at a given state, i.e., how much of the total mass is vapor. We'll come back to this term a little later. For now, it's sufficient to know that, from the definition of quality, a quality of zero corresponds to a saturated liquid (no vapor) while a quality of one corresponds to a saturated vapor (all vapor). Similar parameters can be defined for two-phase regions consisting of solid-vapor and solid-liquid.
- There are three similar sounding terms used frequently in the two-phase region, but each of these terms represents a different thing:
- saturated liquid: In this phase, the state is on the saturated liquid line, i.e., at the left edge of the saturated phase, which means it's $100 \%$ liquid, i.e., it has a quality of zero.
- saturated vapor: In this phase, the state is on the saturated vapor line, i.e., at the right edge of the saturated phase, which means it's $100 \%$ vapor, i.e., it has a quality of one.
- saturated: In this phase, the substance contains both liquid and vapor. The state is within the vapor dome. The quality for a saturated substance is between zero and one.

Although the property plots are helpful for qualitatively understanding the relationship between properties and phases of a substance, they're not particularly useful for quantitative analysis. Fortunately, tables (and computer databases - see for example http://webbook.nist.gov/chemistry/fluid/ have been prepared that provide quantitative values for the relationship between properties.
Figure 3.18 highlights the saturation (liquid-vapor) region in a $T-v$ diagram. The properties corresponding to this region for water are given in Figure 3.19 as two tables. Recall that the pressure and temperature are related in this two-phase region. Thus, there is a unique temperature, known as the saturation temperature, at each pressure, known as the saturation pressure. The difference between the two tables is that one is
ordered according to convenient temperature increments (top table) while the other is ordered by convenient pressure increments (bottom table).


Figure 3.18. A sketch of a $T-v$ diagram highlighting the region under the vapor dome corresponding to the saturation properties.


Figure 3.19. Example table for the saturation properties for water organized by temperature (top) and pressure (bottom). These tables are from Moran et al., 7th ed.

At each saturation temperature and pressure, the tables provide the specific volume and other properties (specific internal energy, specific enthalpy, and specific entropy) at saturated liquid and saturated vapor conditions. The actual properties of the water will lie somewhere between or equal to the saturated liquid and saturated vapor conditions when the water is in a saturated state, e.g., $v_{\text {sat. liquid }} \leq v \leq v_{\text {sat. vapor }}$.

What the actual property values are depends on the quality of the water (the mass fraction of vapor in the two-phase mixture), a topic to be discussed later.
Figure 3.20 presents super-heated vapor phase region in a $T-v$ plot. Example properties for water in this region are given in Figure 3.21. Recall that the pressure and temperature are independent in this single-phase region and, thus, the table entries are organized based on a given pressure and range of temperatures. For each pressure, the saturation temperature (the temperature at which the vapor touches the vapor dome along the saturated vapor line) is also reported.


Figure 3.20. A sketch of a $T$-v diagram highlighting the super-heated vapor region.

| Properties of Superheated Water Vapor |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} T \\ { }^{\circ} \mathrm{C} \end{gathered}$ | $\underset{m^{3} / \mathrm{kg}}{v}$ | $\begin{gathered} u \\ \mathrm{~kJ} / \mathrm{kg} \end{gathered}$ | $\begin{gathered} h \\ \mathrm{~kJ} / \mathrm{kg} \end{gathered}$ | $\stackrel{s}{\mathrm{kj} / \mathrm{kg} \cdot \mathrm{~K}}$ | $\begin{gathered} v \\ \mathrm{~m}^{3} / \mathrm{kg} \end{gathered}$ | $\begin{gathered} u \\ \mathrm{k} / \mathrm{kg} \end{gathered}$ | $\begin{gathered} \stackrel{h}{\mathrm{k}} / \mathrm{kg} \end{gathered}$ | $\stackrel{s}{\mathrm{~kJ} / \mathrm{kg} \cdot \mathrm{~K}}$ |  |
|  | $\begin{gathered} p=0.06 \mathrm{bar}=0.006 \mathrm{MPa} \\ \left(T_{\text {sat }}=36.16^{\circ} \mathrm{C}\right) \end{gathered}$ |  |  |  | $\begin{gathered} p=0.35 \mathrm{bar}=0.035 \mathrm{MPa} \\ \left(T_{\text {sat }}=72.69^{\circ} \mathrm{C}\right) \end{gathered}$ |  |  |  | Pressure Conversions: <br> $1 \mathrm{bar}=0.1 \mathrm{MPa}$ |
| Sat. | 23.739 | 2425.0 | 2567.4 | 8.3304 | 4.526 | 2473.0 | 2631.4 | 7.7158 | $=10^{2} \mathrm{kPa}$ |
| 80 | 27.132 | 2487.3 | 2650.1 | 8.5804 | 4.625 | 2483.7 | 2645.6 | 7.7564 |  |
| 120 | 30.219 | 2544.7 | 2726.0 | 8.7840 | 5.163 | 2542.4 | 2723.1 | 7.9644 |  |
| 160 | 33.302 | 2602.7 | 2802.5 | 8.9693 | 5.696 | 2601.2 | 2800.6 | 8.1519 |  |
| 200 | 36.383 | 2661.4 | 2879.7 | 9.1398 | 6.228 | 2660.4 | 2878.4 | 8.3237 | $p$ is an absolute pressure <br> $v$ is specific volume <br> $u$ is specific internal energy <br> $h$ is specific enthalpy <br> $s$ is specific entropy |
| 240 | 39.462 | 2721.0 | 2957.8 | 9.2982 | 6.758 | 2720.3 | 2956.8 | 8.4828 |  |
| 280 | 42.540 | 2781.5 | 3036.8 | 9.4464 | 7.287 | 2780.9 | 3036.0 | 8.6314 |  |
| 320 | 45.618 | 2843.0 | 3116.7 | 9.5859 | 7.815 | 2842.5 | 3116.1 | 8.7712 |  |
| 360 | 48.696 | 2905.5 | 3197.7 | 9.7180 | 8.344 | 2905.1 | 3197.1 | 8.9034 |  |
| 400 | 51.774 | 2969.0 | 3279.6 | 9.8435 | 8.872 | 2968.6 | 3279.2 | 9.0291 |  |
| 440 | 54.851 | 3033.5 | 3362.6 | 9.9633 | 9.400 | 3033.2 | 3362.2 | 9.1490 |  |
| 500 | 59.467 | 3132.3 | 3489.1 | 10.1336 | 10.192 | 3132.1 | 3488.8 | 9.3194 |  |

Figure 3.21. Example table for the superheated vapor (SHV) properties for water. This table is from Moran et al., 7th ed.

Figure 3.22 presents the compressed liquid phase region in a $T-v$ plot. Example properties for water in this region are given in Figure 3.23. Recall that the pressure and temperature are independent in this single-phase region and, thus, the table entries are organized based on a given pressure and range of temperatures. For each pressure, the saturation temperature (the temperature at which the liquid touches the vapor dome along the saturated liquid line) is also reported.

In what phase (liquid, saturated, vapor, etc.) is water for the following conditions?
a. $T=24^{\circ} \mathrm{C}, p=0.1 \mathrm{bar}(\mathrm{abs})$
b. $\quad p=4 \mathrm{bar}(\mathrm{abs}), T=180^{\circ} \mathrm{C}$
c. $\quad p=20$ bar (abs), $v=0.01 \mathrm{~m}^{3} / \mathrm{kg}$
d. $\quad T=30^{\circ} \mathrm{C}, p=0.04246 \mathrm{bar}$ (abs)
e. $T=30^{\circ} \mathrm{C}, v=1.0043^{*} 10^{-3} \mathrm{~m}^{3} / \mathrm{kg}$
f. $p=25 \operatorname{bar}(\mathrm{abs}), v=0.07998 \mathrm{~m}^{3} / \mathrm{kg}$

## SOLUTION:

a. $\quad T=24{ }^{\circ} \mathrm{C}, p=0.1 \mathrm{bar}$ (abs)

Using Table A. 2 (attached to the end of this example), at $T=24^{\circ} \mathrm{C}, p_{\text {sat }}=0.02985$ bar (abs). Since $p>p_{\text {sat, }}$ the water will be in a compressed liquid phase.

b. $\quad p=4$ bar (abs), $T=180^{\circ} \mathrm{C}$

Using Table A. 3 (attached to the end of this example), at $p=4$ bar (abs), $T_{\text {sat }}=143.6^{\circ} \mathrm{C}$. Since $T>T_{\text {sat }}$, the water will be in a superheated vapor phase.

c. $\quad p=20$ bar (abs), $v=0.01 \mathrm{~m}^{3} / \mathrm{kg}$

Using Table A. 3 (attached to the end of this example), at $p=20$ bar (abs), $v_{\text {sat liquid }}=1.1767 * 10^{-3} \mathrm{~m}^{3} / \mathrm{kg}$ and $v_{\text {sat vapor }}=0.09963 \mathrm{~m}^{3} / \mathrm{kg}$. Since $v_{\text {sat liquid }}<v<v_{\text {sat vapor, }}$, the water will be in a saturated (i.e., two phase) phase.

d. $T=30^{\circ} \mathrm{C}, p=0.04246 \mathrm{bar}$ (abs)

Using Table A. 2 (attached to the end of this example), at $T=30^{\circ} \mathrm{C}, p_{\text {sat }}=0.04246 \mathrm{bar}$ (abs). Since $p=p_{\text {sat }}$, the water will be in a saturated (two-phase) phase.

e. $\quad T=30^{\circ} \mathrm{C}, v=1.0043 * 10^{-3} \mathrm{~m}^{3} / \mathrm{kg}$

Using Table A. 2 (attached to the end of this example), at $T=30^{\circ} \mathrm{C}, v_{\text {sat liquid }}=1.0043^{*} 10^{-3} \mathrm{~m}^{3} / \mathrm{kg}$. Since $v=$ $v_{\text {sat liquid, }}$, the water will be in saturated liquid phase.

f. $\quad p=25 \operatorname{bar}(\mathrm{abs}), v=0.07998 \mathrm{~m}^{3} / \mathrm{kg}$

Using Table A. 3 (attached to the end of this example), at $p=25$ bar (abs), $v_{\text {sat vapor }}=0.07998 \mathrm{~m}^{3} / \mathrm{kg}$. Since $v$ $=v_{\text {sat vapor, }}$, the water will be in a saturated vapor phase.


| Properties of Saturated Water (Liquid-Vapor): Temperature Table |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pressure Conv $1 \mathrm{bar}=0.1 \mathrm{MP}$ | ) | Spec | Volume /kg | Internal kJ/ | Energy |  | Enthalpy kJ/kg |  |  |  |  |
| Temp. ${ }^{\circ} \mathrm{C}$ | Press. bar | Sat. Liquid $v_{f} \times 10^{3}$ | Sat. <br> Vapor <br> $v_{g}$ | Sat. <br> Liquid <br> $u_{\mathrm{f}}$ | Sat. Vapor $u_{\mathrm{g}}$ | Sat. <br> Liquid $h_{f}$ | Evap. $h_{f g}$ | Sat. <br> Vapor <br> $h_{\mathrm{g}}$ | Sat. <br> Liquid <br> $\boldsymbol{S}_{\mathrm{f}}$ | Sat. <br> Vapor <br> $s_{\mathrm{g}}$ | Temp. ${ }^{\circ} \mathrm{C}$ |
| . 01 | 0.00611 | 1.0002 | 206.136 | 0.00 | 2375.3 | 0.01 | 2501.3 | 2501.4 | 0.0000 | 9.1562 | . 01 |
| 4 | 0.00813 | 1.0001 | 157.232 | 16.77 | 2380.9 | 16.78 | 2491.9 | 2508.7 | 0.0610 | 9.0514 | 4 |
| 5 | 0.00872 | 1.0001 | 147.120 | 20.97 | 2382.3 | 20.98 | 2489.6 | 2510.6 | 0.0761 | 9.0257 | 5 |
| 6 | 0.00935 | 1.0001 | 137.734 | 25.19 | 2383.6 | 25.20 | 2487.2 | 2512.4 | 0.0912 | 9.0003 | 6 |
| 8 | 0.01072 | 1.0002 | 120.917 | 33.59 | 2386.4 | 33.60 | 2482.5 | 2516.1 | 0.1212 | 8.9501 | 8 |
| 10 | 0.01228 | 1.0004 | 106.379 | 42.00 | 2389.2 | 42.01 | 2477.7 | 2519.8 | 0.1510 | 8.9008 | 10 |
| 11 | 0.01312 | 1.0004 | 99.857 | 46.20 | 2390.5 | 46.20 | 2475.4 | 2521.6 | 0.1658 | 8.8765 | 11 |
| 12 | 0.01402 | 1.0005 | 93.784 | 50.41 | 2391.9 | 50.41 | 2473.0 | 2523.4 | 0.1806 | 8.8524 | 12 |
| 13 | 0.01497 | 1.0007 | 88.124 | 54.60 | 2393.3 | 54.60 | 2470.7 | 2525.3 | 0.1953 | 8.8285 | 13 |
| 14 | 0.01598 | 1.0008 | 82.848 | 58.79 | 2394.7 | 58.80 | 2468.3 | 2527.1 | 0.2099 | 8.8048 | 14 |
| 15 | 0.01705 | 1.0009 | 77.926 | 62.99 | 2396.1 | 62.99 | 2465.9 | 2528.9 | 0.2245 | 8.7814 | 15 |
| 16 | 0.01818 | 1.0011 | 73.333 | 67.18 | 2397.4 | 67.19 | 2463.6 | 2530.8 | 0.2390 | 8.7582 | 16 |
| 17 | 0.01938 | 1.0012 | 69.044 | 71.38 | 2398.8 | 71.38 | 2461.2 | 2532.6 | 0.2535 | 8.7351 | 17 |
| 18 | 0.02064 | 1.0014 | 65.038 | 75.57 | 2400.2 | 75.58 | 2458.8 | 2534.4 | 0.2679 | 8.7123 | 18 |
| 19 | 0.02198 | 1.0016 | 61.293 | 79.76 | 2401.6 | 79.77 | 2456.5 | 2536.2 | 0.2823 | 8.6897 | 19 |
| 20 | 0.02339 | 1.0018 | 57.791 | 83.95 | 2402.9 | 83.96 | 2454.1 | 2538.1 | 0.2966 | 8.6672 | 20 |
| 21 | 0.02487 | 1.0020 | 54.514 | 88.14 | 2404.3 | 88.14 | 2451.8 | 2539.9 | 0.3109 | 8.6450 | 21 |
| 22 | 0.02645 | 1.0022 | 51.447 | 92.32 | 2405.7 | 92.33 | 2449.4 | 2541.7 | 0.3251 | 8.6229 | 22 |
| 23 | 0.02810 | 1.0024 | 48.574 | 96.51 | 2407.0 | 96.52 | 2447.0 | 2543.5 | 0.3393 | 8.6011 | 23 |
| 24 | 0.02985 | 1.0027 | 45.883 | 100.70 | 2408.4 | 100.70 | 2444.7 | 2545.4 | 0.3534 | 8.5794 | 24 |
| 25 | 0.03169 | 1.0029 | 43.360 | 104.88 | 2409.8 | 104.89 | 2442.3 | 2547.2 | 0.3674 | 8.5580 | 25 |
| 26 | 0.03363 | 1.0032 | 40.994 | 109.06 | 2411.1 | 109.07 | 2439.9 | 2549.0 | 0.3814 | 8.5367 | 26 |
| 27 | 0.03567 | 1.0035 | 38.774 | 113.25 | 2412.5 | 113.25 | 2437.6 | 2550.8 | 0.3954 | 8.5156 | 27 |
| 28 | 0.03782 | 1.0037 | 36.690 | 117.42 | 2413.9 | 117.43 | 2435.2 | 2552.6 | 0.4093 | 8.4946 | 28 |
| 29 | 0.04008 | 1.0040 | 34.733 | 121.60 | 2415.2 | 121.61 | 2432.8 | 2554.5 | 0.4231 | 8.4739 | 29 |
| 30 | 0.04246 | 1.0043 | 32.894 | 125.78 | 2416.6 | 125.79 | 2430.5 | 2556.3 | 0.4369 | 8.4533 | 30 |
| 31 | 0.04496 | 1.0046 | 31.165 | 129.96 | 2418.0 | 129.97 | 2428.1 | 2558.1 | 0.4507 | 8.4329 | 31 |
| 32 | 0.04759 | 1.0050 | 29.540 | 134.14 | 2419.3 | 134.15 | 2425.7 | 2559.9 | 0.4644 | 8.4127 | 32 |
| 33 | 0.05034 | 1.0053 | 28.011 | 138.32 | 2420.7 | 138.33 | 2423.4 | 2561.7 | 0.4781 | 8.3927 | 33 |
| 34 | 0.05324 | 1.0056 | 26.571 | 142.50 | 2422.0 | 142.50 | 2421.0 | 2563.5 | 0.4917 | 8.3728 | 34 |
| 35 | 0.05628 | 1.0060 | 25.216 | 146.67 | 2423.4 | 146.68 | 2418.6 | 2565.3 | 0.5053 | 8.3531 | 35 |
| 36 | 0.05947 | 1.0063 | 23.940 | 150.85 | 2424.7 | 150.86 | 2416.2 | 2567.1 | 0.5188 | 8.3336 | 36 |
| 38 | 0.06632 | 1.0071 | 21.602 | 159.20 | 2427.4 | 159.21 | 2411.5 | 2570.7 | 0.5458 | 8.2950 | 38 |
| 40 | 0.07384 | 1.0078 | 19.523 | 167.56 | 2430.1 | 167.57 | 2406.7 | 2574.3 | 0.5725 | 8.2570 | 40 |
| 45 | 0.09593 | 1.0099 | 15.258 | 188.44 | 2436.8 | 188.45 | 2394.8 | 2583.2 | 0.6387 | 8.1648 | 45 |


| TABLE A-3 |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1- Properties of Saturated Water (Liquid-Vapor): Pressure Table |  |  |  |  |  |  |  |  |  |  |  |
| Pressure Conversions:$1 \text { bar }=0.1 \mathrm{MPa}$$=10^{2} \mathrm{kPa}$ |  | Specific Volume $\mathrm{m}^{3} / \mathrm{kg}$ |  | Internal Energy kJ/kg |  | Enthalpy kJ/kg |  |  | Entropy <br> $\mathbf{k J} / \mathbf{k g} \cdot \mathbf{K}$ |  | Press. bar |
| Press. bar | Temp. ${ }^{\circ} \mathrm{C}$ | Sat. Liquid $v_{f} \times 10^{3}$ | Sat. <br> Vapor <br> $v_{g}$ | Sat. Liquid $u_{\mathrm{f}}$ | Sat. <br> Vapor <br> $u_{g}$ | Sat. <br> Liquid <br> $h_{f}$ | Evap. $h_{\mathrm{fg}} \ldots$ | Sat. Vapor $h_{\mathrm{g}}$ | Sat. <br> Liquid <br> $\boldsymbol{S}_{\mathrm{f}}$ | Sat. Vapor $s_{\mathrm{g}}$ |  |
| 0.04 | 28.96 | 1.0040 | 34.800 | 121.45 | 2415.2 | 121.46 | 2432.9 | 2554.4 | 0.4226 | 8.4746 | 0.04 |
| 0.06 | 36.16 | 1.0064 | 23.739 | 151.53 | 2425.0 | 151.53 | 2415.9 | 2567.4 | 0.5210 | 8.3304 | 0.06 |
| 0.08 | 41.51 | 1.0084 | 18.103 | 173.87 | 2432.2 | 173.88 | 2403.1 | 2577.0 | 0.5926 | 8.2287 | 0.08 |
| 0.10 | 45.81 | 1.0102 | 14.674 | 191.82 | 2437.9 | 191.83 | 2392.8 | 2584.7 | 0.6493 | 8.1502 | 0.10 |
| 0.20 | 60.06 | 1.0172 | 7.649 | 251.38 | 2456.7 | 251.40 | 2358.3 | 2609.7 | 0.8320 | 7.9085 | 0.20 |
| 0.30 | 69.10 | 1.0223 | 5.229 | 289.20 | 2468.4 | 289.23 | 2336.1 | 2625.3 | 0.9439 | 7.7686 | 0.30 |
| 0.40 | 75.87 | 1.0265 | 3.993 | 317.53 | 2477.0 | 317.58 | 2319.2 | 2636.8 | 1.0259 | 7.6700 | 0.40 |
| 0.50 | 81.33 | 1.0300 | 3.240 | 340.44 | 2483.9 | 340.49 | 2305.4 | 2645.9 | 1.0910 | 7.5939 | 0.50 |
| 0.60 | 85.94 | 1.0331 | 2.732 | 359.79 | 2489.6 | 359.86 | 2293.6 | 2653.5 | 1.1453 | 7.5320 | 0.60 |
| 0.70 | 89.95 | 1.0360 | 2.365 | 376.63 | 2494.5 | 376.70 | 2283.3 | 2660.0 | 1.1919 | 7.4797 | 0.70 |
| 0.80 | 93.50 | 1.0380 | 2.087 | 391.58 | 2498.8 | 391.66 | 2274.1 | 2665.8 | 1.2329 | 7.4346 | 0.80 |
| 0.90 | 96.71 | 1.0410 | 1.869 | 405.06 | 2502.6 | 405.15 | 2265.7 | 2670.9 | 1.2695 | 7.3949 | 0.90 |
| 1.00 | 99.63 | 1.0432 | 1.694 | 417.36 | 2506.1 | 417.46 | 2258.0 | 2675.5 | 1.3026 | 7.3594 | 1.00 |
| 1.50 | 111.4 | 1.0528 | 1.159 | 466.94 | 2519.7 | 467.11 | 2226.5 | 2693.6 | 1.4336 | 7.2233 | 1.50 |
| 2.00 | 120.2 | 1.0605 | 0.8857 | 504.49 | 2529.5 | 504.70 | 2201.9 | 2706.7 | 1.5301 | 7.1271 | 2.00 |
| 2.50 | 127.4 | 1.0672 | 0.7187 | 535.10 | 2537.2 | 535.37 | 2181.5 | 2716.9 | 1.6072 | 7.0527 | $2.50{ }^{*}$ |
| 3.00 | 133.6 | 1.0732 | 0.6058 | 561.15 | 2543.6 | 561.47 | 2163.8 | 2725.3 | 1.6718 | 6.9919 | 3.00 |
| 3.50 | 138.9 | 1.0786 | 0.5243 | 583.95 | 2546.9 | 584.33 | 2148.1 | 2732.4 | 1.7275 | 6.9405 | 3.50 |
| 4.00 | 143.6 | 1.0836 | 0.4625 | 604.31 | 2553.6 | 604.74 | 2133.8 | 2738.6 | 1.7766 | 6.8959 | 4.00 |
| 4.50 | 147.9 | 1.0882 | 0.4140 | 622.25 | 2557.6 | 623.25 | 2120.7 | 2743.9 | 1.8207 | 6.8565 | 4.50 |
| 5.00 | 151.9 | 1.0926 | 0.3749 | 639.68 | 2561.2 | 640.23 | 2108.5 | 2748.7 | 1.8607 | 6.8212 | 5.00 |
| 6.00 | 158.9 | 1.1006 | 0.3157 | 669.90 | 2567.4 | 670.56 | 2086.3 | 2756.8 | 1.9312 | 6.7600 | 6.00 |
| 7.00 | 165.0 | 1.1080 | 0.2729 | 696.44 | 2572.5 | 697.22 | 2066.3 | 2763.5 | 1.9922 | 6.7080 | 7.00 |
| 8.00 | 170.4 | 1.1148 | 0.2404 | 720.22 | 2576.8 | 721.11 | 2048.0 | 2769.1 | 2.0462 | 6.6628 | 8.00 |
| 9.00 | 175.4 | 1.1212 | 0.2150 | 741.83 | 2580.5 | 742.83 | 2031.1 | 2773.9 | 2.0946 | 6.6226 | 9.00 |
| 10.0 | 179.9 | 1.1273 | 0.1944 | 761.68 | 2583.6 | 762.81 | 2015.3 | 2778.1 | 2.1387 | 6.5863 | 10.0 |
| 15.0 | 198.3 | 1.1539 | 0.1318 | 843.16 | 2594.5 | 844.84 | 1947.3 | 2792.2 | 2.3150 | 6.4448 | 15.0 |
| 20.0 | 212.4 | 1.1767 | 0.09963 | 906.44 | 2600.3 | 908.79 | 1890.7 | 2799.5 | 2.4474 | 6.3409 | 20.0 |
| 25.0 | 224.0 | 1.1973 | 0.07998 | 959.11 | 2603.1 | 962.11 | 1841.0 | 2803.1 | 2.5547 | 6.2575 | 25.0 |
| 30.0 | 233.9 | 1.2165 | 0.06668 | 1004.8 | 2604.1 | 1008.4 | 1795.7 | 2804.2 | 2.6457 | 6.1869 | 30.0 |
| 35.0 | 242.6 | 1.2347 | 0.05707 | 1045.4 | 2603.7 | 1049.8 | 1753.7 | 2803.4 | 2.7253 | 6.1253 | 35.0 |
| 40.0 | 250.4 | 1.2522 | 0.04978 | 1082.3 | 2602.3 | 1087.3 | 1714.1 | 2801.4 | 2.7964 | 6.0701 | 40.0 |
| 45.0 | 257.5 | 1.2692 | 0.04406 | 1116.2 | 2600.1 | 1121.9 | 1676.4 | 2798.3 | 2.8610 | 6.0199 | 45.0 |
| 50.0 | 264.0 | 1.2859 | 0.03944 | 1147.8 | 2597.1 | 1154.2 | 1640.1 | 2794.3 | 2.9202 | 5.9734 | 50.0 |
| 60.0 | 275.6 | 1.3187 | 0.03244 | 1205.4 | 2589.7 | 1213.4 | 1571.0 | 2784.3 | 3.0267 | 5.8892 | 60.0 |
| 70.0 | 285.9 | 1.3513 | 0.02737 | 1257.6 | 2580.5 | 1267.0 | 1505.1 | 2772.1 | 3.1211 | 5.8133 | 70.0 |
| 80.0 | 295.1 | 1.3842 | 0.02352 | 1305.6 | 2569.8 | 1316.6 | 1441.3 | 2758.0 | 3.2068 | 5.7432 | 80.0 |
| 90.0 | 303.4 | 1.4178 | 0.02048 | 1350.5 | 2557.8 | 1363.3 | 1378.9 | 2742.1 | 3.2858 | 5.6772 | 90.0 |
| 100. | 311.1 | 1.4524 | 0.01803 | 1393.0 | 2544.4 | 1407.6 | 1317.1 | 2724.7 | 3.3596 | 5.6141 | 100. |
| 110. | 318.2 | 1.4886 | 0.01599 | 1433.7 | 2529.8 | 1450.1 | 1255.5 | 2705.6 | 3.4295 | 5.5527 | 110. |



Figure 3.22. A sketch of a $T-v$ diagram highlighting the compressed liquid region.

| Properties of Compressed Liquid Water |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\left(\begin{array}{l} 0 \times 10^{3} \\ m^{3} / \mathrm{kg} \end{array}\right.$ | $\mathrm{kJ} / \mathrm{kg}$ | $\stackrel{\stackrel{h}{\mathrm{hj} / \mathrm{kg}}}{ }$ | $\stackrel{s}{\mathrm{~kJ} / \mathrm{kg} \cdot \mathrm{~K}}$ | $\begin{gathered} v \times 1 \mathbf{1 0}^{\mathbf{3}} \\ \mathrm{m}^{\mathbf{3} / \mathrm{kg}} \end{gathered}$ | $\begin{gathered} u \\ \mathrm{k} / \mathrm{kg} \end{gathered}$ | $\begin{gathered} h \\ \mathrm{kj} / \mathrm{kg} \end{gathered}$ | $\begin{gathered} s \\ \mathbf{k j} / \mathbf{k g} \cdot \mathbf{k} \end{gathered}$ |  |
|  |  | $\frac{25 \mathrm{~b}}{\left(T_{\text {sat }}\right.}=$ | $\begin{aligned} & 2.5 \mathrm{MPa} \\ & \\ & \left.\hline 9^{\circ} \mathrm{C}\right) \end{aligned}$ |  |  | $\begin{gathered} p=\mathbf{5 0} \mathbf{b a} \\ \quad\left(T_{\text {sat }}=\right. \end{gathered}$ | $\begin{aligned} & =5.0 \mathrm{MPa} \\ & 63.99^{\circ} \mathrm{C} \text { ) } \end{aligned}$ |  | Pressure Conversions: $1 \mathrm{bar}=0.1 \mathrm{MPa}$ |
| 20 | 1.0006 | 83.80 | 86.30 | 2961 | . 9995 | 83.65 | 88.65 | . 2956 | $=10^{2} \mathrm{kPa}$ |
| 40 | 1.0067 | 167.25 | 169.77 | . 5715 | 1.0056 | 166.95 | 171.97 | . 5705 |  |
| 80 | 1.0280 | 334.29 | 336.86 | 1.0737 | 1.0268 | 333.72 | 338.85 | 1.0720 |  |
| 100 | 1.0423 | 418.24 | 420.85 | 1.3050 | 1.0410 | 417.52 | 422.72 | 1.3030 | $v$ is specific volume |
| 140 | 1.0784 | 587.82 | 590.52 | 1.7369 | 1.0768 | 586.76 | 592.15 | 1.7343 | (Note that $v$ entries are |
| 180 | 1.1261 | 761.16 | 763.97 | 2.1375 | 1.1240 | 759.63 | 765.25 | $2.134 \mathrm{P}$ | multiplied by 1000 , e.g., |
| 200 | 1.1555 | 849.9 | 852.8 | 2.3294 | 1.1530 | 848.1 | 853.9 | 2.3255 | $\underline{v}\left(2.5 \mathrm{MPa}, 2{ }^{\circ} \mathrm{C}\right)=$ |
| 220 | 1.1898 | 940.7 | 943.7 | 2.5174 | 1.1866 | 938.4 | 944.4 | 2.5128 | $1.0006 * 10^{-3} \mathrm{~m}^{3} / \mathrm{kg}$. |
| Sat. | 1.1973 | 959.1 | 962.1 | 2.5546 | 1.2859 | 1147.8 | 1154.2 | 2.9202 | $u$ is specific internal energy |

Figure 3.23. Example table for the compressed liquid (CL) properties for water. This table is from Moran et al., 7th ed.

### 3.5.1. Linear Interpolation

In order to save space, the properties in the tables are listed in coarse increments, e.g., increments of 2.5 MPa and 20 or $40^{\circ} \mathrm{C}$. To approximate property values between the ones stated in the tables, we can use linear interpolation. Linear interpolation is the process of estimating the values of a property assuming a linear relationship between neighboring data points. Hence, to estimate the value of a property $P$ at a value $V$ given the property's values at neighboring points $V_{S}$ and $V_{L}$, corresponding to points in the table just smaller than and larger than the value $V$ of interest, we can use the equation of a line (Figure 3.24),

$$
\begin{equation*}
P-P_{S}=\left(\frac{P_{L}-P_{S}}{V_{L}-V_{S}}\right)\left(V-V_{S}\right) \tag{3.50}
\end{equation*}
$$

where $P_{S}$ and $P_{L}$ are the property values at $V_{S}$ and $V_{L}$, respectively.

What is the specific volume of compressed liquid water at 5.0 MPa (abs) and $60^{\circ} \mathrm{C}$ ?

## SOLUTION:

Since there is no specific volume data at $60^{\circ} \mathrm{C}$ at 5.0 MPa in Table A-5 shown below, we can approximate the specific volume at $60^{\circ} \mathrm{C}$ using linear interpolation,

$$
\begin{equation*}
v_{60^{\circ} \mathrm{C}}-v_{40^{\circ} \mathrm{C}}=\left(\frac{v_{80}{ }^{\circ}-v_{40}{ }^{\circ} \mathrm{C}}{T_{80}{ }^{\circ}-v_{40}{ }^{\circ} \mathrm{C}}\right)\left(T_{60^{\circ} \mathrm{C}}-T_{40^{\circ} \mathrm{C}}\right), \tag{1}
\end{equation*}
$$

where

$$
\begin{array}{ll}
v_{40}{ }^{\circ} \mathrm{C} & =1.0056^{*} 10^{-3} \mathrm{~m}^{3} / \mathrm{kg} \\
v_{40}{ }^{\circ} \mathrm{C} & =1.0268^{*} 10^{-3} \mathrm{~m}^{3} / \mathrm{kg} \\
T_{40}{ }^{\circ} \mathrm{C} & =40^{\circ} \mathrm{C} \\
T_{60}{ }^{\circ} \mathrm{C} & =60^{\circ} \mathrm{C} \\
T_{80}{ }^{\circ} \mathrm{C} & =80^{\circ} \mathrm{C} \\
\Rightarrow v_{60}{ }^{\circ} \mathrm{C} & =1.0162^{*} 10^{-3} \mathrm{~m}^{3} / \mathrm{kg}
\end{array}
$$

| TABLE A-5 |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Properties of Compressed Liquid Water |  |  |  |  |  |  |  |  | Pressure Conversions:$\begin{aligned} 1 \mathrm{bar} & =0.1 \mathrm{MPa} \\ & =10^{2} \mathrm{kPa} \end{aligned}$ |
| $\begin{gathered} \boldsymbol{T} \\ { }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{gathered} v \times \mathbf{1 0}^{\mathbf{3}} \\ \mathrm{m}^{3} / \mathrm{kg} \end{gathered}$ | $\begin{gathered} u \\ \mathrm{kj} / \mathrm{kg} \end{gathered}$ | $\begin{gathered} h \\ \mathrm{~kJ} / \mathrm{kg} \end{gathered}$ | $\stackrel{s}{\mathrm{~kJ} / \mathrm{kg} \cdot \mathrm{~K}}$ | $\begin{aligned} & v \times 10^{3} \\ & \mathbf{m}^{3} / \mathbf{k g} \end{aligned}$ | $\begin{gathered} u \\ \mathbf{k} / \mathrm{kg} \end{gathered}$ | $\begin{gathered} h \\ \mathrm{kj} / \mathrm{kg} \end{gathered}$ | $\begin{gathered} \mathbf{s} \\ \mathbf{k J} / \mathbf{k g} \cdot \mathbf{K} \end{gathered}$ |  |
|  | $\begin{gathered} p=25 \mathrm{bar}=2.5 \mathrm{MPa} \\ \left(T_{\text {sat }}=223.99^{\circ} \mathrm{C}\right) \end{gathered}$ |  |  |  | $\begin{gathered} p=50 \mathrm{bar}=5.0 \mathrm{MPa} \\ \left(T_{\text {sat }}=263.99^{\circ} \mathrm{C}\right) \end{gathered}$ |  |  |  |  |
| 20 | 1.0006 | 83.80 | 86.30 | . 2961 | . 9995 | 83.65 | 88.65 | .2956 |  |
| 40 | 1.0067 | 167.25 | 169.77 | . 5715 | 1.0056 | 166.95 | 171.97 | . 5705 |  |
| 80 | 1.0280 | 334.29 | 336.86 | 1.0737 | 1.0268 | 333.72 | 338.85 | 1.0720 |  |
| 100 | 1.0423 | 418.24 | 420.85 | 1.3050 | 1.0410 | 417.52 | 422.72 | 1.3030 |  |
| 140 | 1.0784 | 587.82 | 590.52 | 1.7369 | 1.0768 | 586.76 | 592.15 | 1.7343 |  |
| 180 | 1.1261 | 761.16 | 763.97 | 2.1375 | 1.1240 | 759.63 | 765.25 | 2.1341 |  |
| 200 | 1.1555 | 849.9 | 852.8 | 2.3294 | 1.1530 | 848.1 | 853.9 | 2.3255 |  |
| 220 | 1.1898 | 940.7 | 943.7 | 2.5174 | 1.1866 | 938.4 | 944.4 | 2.5128 |  |
| Sat. | 1.1973 | 959.1 | 962.1 | 2.5546 | 1.2859 | 1147.8 | 1154.2 | 2.9202 |  |

(Table from Moran et al., $7^{\text {th }}$ ed.)

What is the specific internal energy of compressed liquid water at 3.0 MPa and $60^{\circ} \mathrm{C}$ ?

## SOLUTION:

For this case, there is no table entry for either 3.0 MPa or $60^{\circ} \mathrm{C}$ so we must linearly interpolate with respect to both temperature and pressure (called bilinear interpolation),

$$
\begin{align*}
& u_{2.5 \mathrm{MPa}, 60}{ }^{\circ} \mathrm{C}-u_{2.5 \mathrm{MPa}, 40^{\circ} \mathrm{C}}=\left(\frac{u_{2.5 \mathrm{MPa}, 80^{\circ} \mathrm{C}}-u_{2.5 \mathrm{MPa}, 40^{\circ} \mathrm{C}}}{T_{2.5 \mathrm{MPa}, 80^{\circ} \mathrm{C}}-T_{2.5 \mathrm{MPa}, 40^{\circ} \mathrm{C}}}\right)\left(T_{2.5 \mathrm{MPa}, 60^{\circ} \mathrm{C}}-T_{2.5 \mathrm{MPa}, 40^{\circ} \mathrm{C}}\right),  \tag{1}\\
& u_{5.0 \mathrm{MPa}, 60{ }^{\circ} \mathrm{C}}-u_{5.0 \mathrm{MPa}, 40^{\circ} \mathrm{C}}=\left(\frac{u_{5.0 \mathrm{MPa}, 80^{\circ} \mathrm{C}}-u_{5.0 \mathrm{MPa}, 40^{\circ} \mathrm{C}}}{T_{5.0 \mathrm{MPa}, 80^{\circ} \mathrm{C}}-T_{5.0 \mathrm{MPa}, 40^{\circ} \mathrm{C}}}\right)\left(T_{5.0 \mathrm{MPa}, 60^{\circ} \mathrm{C}}-T_{5.0 \mathrm{MPa}, 40^{\circ} \mathrm{C}}\right), \\
& u_{3.0 \mathrm{MPa}, 60{ }^{\circ} \mathrm{C}}-u_{2.5 \mathrm{MPa}, 60^{\circ} \mathrm{C}}=\left(\frac{u_{5.0 \mathrm{MPa}, 60^{\circ} \mathrm{C}}-u_{2.5 \mathrm{MPa}, 60^{\circ} \mathrm{C}}}{p_{5.0 \mathrm{MPa}, 60^{\circ} \mathrm{C}}-p_{2.5 \mathrm{MPa}, 60^{\circ} \mathrm{C}}}\right)\left(p_{3.0 \mathrm{MPa}, 60{ }^{\circ} \mathrm{C}}-p_{2.5 \mathrm{MPa}, 600^{\circ} \mathrm{C}}\right),
\end{align*}
$$

where,

$$
\begin{array}{ll}
u_{2.5 \mathrm{MPa}, 40^{\circ} \mathrm{C}} & =167.25 \mathrm{~kJ} / \mathrm{kg} \\
u_{2.5 \mathrm{MPa}, 80^{\circ} \mathrm{C}} & =334.29 \mathrm{~kJ} / \mathrm{kg} \\
u_{5.0 \mathrm{MPa}, 40^{\circ} \mathrm{C}} & =166.95 \mathrm{~kJ} / \mathrm{kg} \\
u_{5.0} \mathrm{MPa}, 80^{\circ} \mathrm{C} & =333.72 \mathrm{~kJ} / \mathrm{kg} \\
T_{2.5 \mathrm{MPa}, 40^{\circ} \mathrm{C}} \quad=T_{5.0 \mathrm{MPa}, 40^{\circ} \mathrm{C}}=40^{\circ} \mathrm{C} \\
T_{2.5 \mathrm{MPa}, 60^{\circ} \mathrm{C}} \quad=T_{5.0 \mathrm{MPa}, 60^{\circ} \mathrm{C}}=60^{\circ} \mathrm{C} \\
T_{2.5 \mathrm{MPa}, 80^{\circ} \mathrm{C}} \quad=T_{5.0 \mathrm{MPa}, 80^{\circ} \mathrm{C}=80^{\circ} \mathrm{C}}^{p_{2.5 \mathrm{MPa}, 60^{\circ} \mathrm{C}} \quad=2.5 \mathrm{MPa}} \\
p_{3.0 \mathrm{MPa}, 60^{\circ} \mathrm{C}} \quad=3.0 \mathrm{MPa} \\
p_{5.0} \mathrm{MPa}, 60^{\circ} \mathrm{C} & =5.0 \mathrm{MPa} \\
\Rightarrow u_{2.5} \mathrm{MPa}, 60^{\circ} \mathrm{C} & =250.77 \mathrm{~kJ} / \mathrm{kg}, u 5.0 \mathrm{MPa}, 60^{\circ} \mathrm{C}=250.34 \mathrm{~kJ} / \mathrm{kg} \Rightarrow U_{3.0 \mathrm{MPa}, 60^{\circ} \mathrm{C}}=250.68 \mathrm{~kJ} / \mathrm{kg}
\end{array}
$$

Note that the same result would be achieved if we interpolated first with respect to pressure and then with respect to temperature.

## TABLE A-5

## Properties of Compressed Liquid Water

| $\begin{gathered} T \\ { }^{\circ} \mathrm{C} \end{gathered}$ | $\begin{gathered} v \times 10^{3} \\ \mathrm{~m}^{3} / \mathrm{kg} \end{gathered}$ | $\begin{gathered} u \\ \mathrm{~kJ} / \mathrm{kg} \end{gathered}$ | h <br> kJ/kg | $\stackrel{s}{\mathrm{~kJ} / \mathrm{kg} \cdot \mathrm{~K}}$ | $\begin{gathered} v \times 10^{3} \\ \mathrm{~m}^{3} / \mathrm{kg} \end{gathered}$ | $\begin{gathered} u \\ \mathrm{~kJ} / \mathrm{kg} \end{gathered}$ | $h$ kJ/kg | $\stackrel{s}{\mathrm{~kJ} / \mathrm{kg} \cdot \mathrm{~K}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} p=25 \mathrm{bar}=2.5 \mathrm{MPa} \\ \left(T_{\text {sat }}=223.99^{\circ} \mathrm{C}\right) \end{gathered}$ |  |  |  | $\begin{gathered} p=50 \mathrm{bar}=5.0 \mathrm{MPa} \\ \left(T_{\text {sat }}=263.99^{\circ} \mathrm{C}\right) \end{gathered}$ |  |  |  |
| 20 | 1.0006 | 83.80 | 86.30 | . 2961 | . 9995 | 83.65 | 88.65 | . 2956 |
| 40 | 1.0067 | 167.25 | 169.77 | . 5715 | 1.0056 | 166.95 | 171.97 | . 5705 |
| 80 | 1.0280 | 334.29 | 336.86 | 1.0737 | 1.0268 | 333.72 | 338.85 | 1.0720 |
| 100 | 1.0423 | 418.24 | 420.85 | 1.3050 | 1.0410 | 417.52 | 422.72 | 1.3030 |
| 140 | 1.0784 | 587.82 | 590.52 | 1.7369 | 1.0768 | 586.76 | 592.15 | 1.7343 |
| 180 | 1.1261 | 761.16 | 763.97 | 2.1375 | 1.1240 | 759.63 | 765.25 | 2.1341 |
| 200 | 1.1555 | 849.9 | 852.8 | 2.3294 | 1.1530 | 848.1 | 853.9 | 2.3255 |
| 220 | 1.1898 | 940.7 | 943.7 | 2.5174 | 1.1866 | 938.4 | 944.4 | 2.5128 |
| Sat. | 1.1973 | 959.1 | 962.1 | 2.5546 | 1.2859 | 1147.8 | 1154.2 | 2.9202 |


(Table from Moran et al., $7^{\text {th }}$ ed.)


Figure 3.24. Schematic showing how to linearly interpolate a property value.

### 3.5.2. Quality

Recall that Figure 3.19 presented two tables for saturated water properties (aka, water in two-phase, liquidvapor equilibrium along the saturated liquid and the saturated vapor lines). The pressure and temperature are uniquely related in this two-phase region (and along the saturated liquid and vapor lines). The top table (Table A-2) presents the property data organized according to temperature while the bottom table (Table A-3) presents the same data organized according to pressure. The subscripts " f " and " g " in the table refer to "fluid" and "gas", which is a historical notation. It is better to refer to the properties as being either at the saturated liquid state (subscript " f " in the table) or in the saturated vapor state (subscript "g" in the table). Similar tables exist for two-phase solid-liquid and solid-vapor.
Within the two-phase liquid-vapor region (i.e, the vapor dome), the fraction of mass that is vapor is given by the quality, $x$, which is defined as,

$$
\begin{equation*}
x:=\frac{m_{v}}{m_{l}+m_{v}} \tag{3.51}
\end{equation*}
$$

where $m_{v}$ and $m_{l}$ are the masses of vapor and liquid, respectively. Note that the fraction of mass that is liquid is,

$$
\begin{equation*}
\frac{m_{l}}{m_{l}+m_{v}}=\frac{m_{l}+m_{v}-m_{v}}{m_{l}+m_{v}}=\frac{m_{l}+m_{v}}{m_{l}+m_{v}}-\frac{m_{v}}{m_{l}+m_{v}}=1-x \tag{3.52}
\end{equation*}
$$

Hence, a quality of zero corresponds to a saturated liquid (all liquid, $m_{v}=0$ ) while a quality of one corresponds to a saturated vapor (all vapor, $m_{l}=0$ ). The quality can be used to determine the value of properties within the two-phase region, given the saturated liquid and saturated vapor properties. For example, the specific volume of a mixture (subscript " m ") of liquid (subscript " l ") and vapor (subscript " v ") in equilibrium (i.e., in the vapor dome), assuming the quality $x$ is known, is,

$$
\begin{gather*}
V_{m}=V_{l}+V_{v}  \tag{3.53}\\
v_{m}=\frac{V_{m}}{m_{m}}=\frac{V_{l}+V_{v}}{m_{m}}=\frac{V_{l}}{m_{m}}+\frac{V_{v}}{m_{m}} \tag{3.54}
\end{gather*}
$$

where $V_{m}$ is the total volume of the mixture. The quantity $m_{m}$ is the total mass of the mixture, i.e., $m_{m}=m_{l}+m_{v}$. Hence,

$$
\begin{equation*}
v_{m}=\frac{V_{l}}{m_{l}+m_{v}}+\frac{V_{v}}{m_{l}+m_{v}}=\frac{m_{l} v_{l}}{m_{l}+m_{v}}+\frac{m_{v}+v_{v}}{m_{l}+m_{v}}=\left(\frac{m_{l}}{m_{l}+m_{v}}\right) v_{l}+\left(\frac{m_{v}}{m_{l}+m_{v}}\right) v_{v} \tag{3.55}
\end{equation*}
$$

where the volume is related to the specific volume via $V=m v$. Making use of Eqs. (3.51) and (3.52),

$$
\begin{equation*}
v_{m}=(1-x) v_{l}+x v_{v} \tag{3.56}
\end{equation*}
$$

Thus, the specific volume of a mixture of liquid and vapor can be thought of as the specific volume of the saturated liquid multiplied by its mass fraction $\left((1-x) v_{l}\right)$ plus the specific volume of the saturated vapor

