Two well-insulated, rigid tanks filled with carbon monoxide (CO) gas are connected by a valve. In tank A, 1 kg of gas is stored at 100 kPa (abs) and 300 K. In tank B, 5 kg of gas are stored at 500 kPa (abs) and 870 K. The valve is opened, and the contents of the two tanks are allowed to mix until equilibrium is attained.

Assuming ideal gas behavior for the carbon monoxide, determine:

- a. the volume of each tank, in m<sup>3</sup>,
- b. the final temperature, in K, and
- c. the final pressure, in kPa (abs).



SOLUTION:



The tank volumes may be found using the Ideal Gas Law,

$$pV = mRT \implies V = \frac{mRT}{p}$$
. (1)  
Using the given data along with,

$$M_{CO} = 12.011 \frac{kg}{kmol} + 16.00 \frac{kg}{kmol} = 28.011 \frac{kg}{kmol'},$$
(2)

$$R_{CO} = \frac{\bar{R}_U}{M_{CO}} = \frac{8.314 \frac{kJ}{km0.K}}{28.011 \frac{kg}{km0.K}} = 0.2968 \frac{kJ}{kg.K},$$
(3)

$$m_{\rm A} = 1 \text{ kg}, T_{\rm A1} = 300 \text{ K}, p_{\rm A1} = 100 \text{ kPa (abs)} => V_{\rm A} = 0.890 \text{ m}^3, m_{\rm B} = 5 \text{ kg}, T_{\rm B1} = 870 \text{ K}, p_{\rm B1} = 500 \text{ kPa (abs)} => V_{\rm B} = 2.582 \text{ m}^3$$

Apply the First Law to the two tanks before (state 1) and after (state 2) the valve is opened,

 $\Delta E_{sys,12} = Q_{into\ sys,12} - W_{by\ sys,12},\tag{2}$ 

where,

$\Delta E_{sys,12} = \Delta U_{sys,12} + \Delta K E_{sys,12} + \Delta P E_{sys,12} = \Delta U_{sys,12} = U_2 - U_1$ (no changes in KE or PE),	(3)
$Q_{into sys,12} = 0$ (the tanks are well-insulated),	(4)
$W_{by \ sys, 12} = 0$ (the tanks are rigid).	(5)

Thus,

$$U_2 = U_1, \tag{6}$$

where,

 $U_1 = m_A u_{A1} + m_B u_{B1}, (7)$ 

 $U_2 = (m_A + m_B)u_2$  (the tanks are mixed and in equilibrium at the end of the process). (8) Using the given data and the Ideal Gas Table for carbon monoxide (Table A-23 in Moran et al., 8<sup>th</sup> ed., Wiley; refer to the end of this document),

 $u_{A1} = u_{CO}(T_{A1} = 300 \text{ K}) = 6229 \text{ kJ/kmol},$   $u_{B1} = u_{CO}(T_{B1} = 870 \text{ K}) = 18858 \text{ kJ/kmol},$  $=> u_2 = 16753 \text{ kJ/kmol} => T_2 = 781 \text{ K}$  (interpolating from the Ideal Gas Table).

Use the Ideal Gas Law to determine the final pressure in the tanks,

$$pV = mRT \implies p_2 = \frac{(m_A + m_B)RT_2}{V_A + V_B}.$$
From the given and calculated data,  $p_2 = 401$  kPa (abs). (9)

		-								966	TAB	LE A-23	ie'aos								
TABLE A-23											(Con	tinued)						$\overline{h}$ and $\overline{u}$ in	kJ/kmol. 3° i	in	
Enthalpy $\overline{h}(T)$ and internal energy $\overline{u}(T)$ , in kJ/kmol. Abso												Car	bon Dioxide	e, CO <sub>2</sub>	Carb	on Monoxi	de, CO	W	ater Vapor, H	12	
	Carbon Dioxide, CO <sub>2</sub>				Carbon Monoxide, CO Water Vapor, H <sub>2</sub> O						1 2 2 2	$(\overline{h}_l^\circ = -393,520 \text{ kJ/kmol})$			$(\overline{h}_{t}^{\circ} =$	-110,530 l	$(\bar{h}_{\rm f}^{\circ} = -241,820 \text{ kJ/H})$				
	$(h_{\rm f}^{\rm o} = -393,520 \text{ kJ/kmol})$			$(h_l^\circ = -110,530 \text{ kJ/kmol})$			$(h_l^\circ = -241,820 \text{ kJ/km})$		0 kJ/km	km π(	7(K)	Ћ	Ū	<u></u> 5°	ħ	Ū	<u>5</u> °	ħ	Ū		
T(K)	ħ	ū	<u>5</u> °	Ћ	Ū	<u>5</u> °	Ћ	Ū		600		600	22,280	17,291	243.199	17,611	12,622	218.204	20,402	15,413	
0	0	0	0	0	0	0	0		0		610	22,754	17,683	243.983	17,915	12,843	218.708	20,765	15,693		
220	6,601	4,772	202.966	6,391	4,562	188.683	7,295	5,46	6 178		620	23,231	18,076	244.758	18,221	13,066	219.205	21,130	15,975		
230	6,938	5,026	204.464	6,683	4,771	189.980	7,628	5,715	180		630	23,709	18,4/1	245.524	18,527	13,289	219.695	21,495	16,257		
240	7,280	5,285	205.920	6,975	4,979	191.221	7,961	5,965	181		640	24,190	18,869	246.282	18,833	13,512	220.179	21,862	10,541		
250	7,627	5,548	207.337	7,266	5,188	192.411	8,294	6,215	182		650	24,674	19,270	247.032	19,141	13,736	220.656	22,230	16,826		
260	7,979	5,817	208.717	7,558	5,396	193.554	8,627	6,466	184.		670	25,160	19,672	247.773	19,449	13,962	221.127	22,600	17,112		
270	8,335	6,091	210.062	7,849	5,604	194.654	8,961	6,716	185.		680	26,138	20,078	240.307	20.069	14,107	221.592	22,970	17,399		
280	8,697	6,369	211.376	8,140	5,812	195.173	9,296	6,968	186.6		690	26,631	20,894	249.952	20,008	14,414	222.032	23,542	17,000		
290	9,063	6,651	212.660	8,432	6,020	196.735	9,631	7,219	187.7		700	27 125	21 305	250 662	20,600	14 970	222.002	24.000	10,210		
298	9,364	0,885	213.685	8,669	6,190	197.543	9,904	7,425	188.7.		710	27.622	21,505	250.005	20,090	14,870	222.955	24,088	18,268		
300	9,431	6,939	213.915	8,723	6,229	197.723	9,966	7,472	188.92		720	28,121	22,134	252.065	21,315	15,328	223.390	24,404	18,854		
320	10,186	7,230	216.351	9,014	6 6 4 5	198.678	10,302	7 078	190.03		730	28,622	22,552	252.755	21,628	15.558	224.265	25,218	19 148		
330	10,570	7,826	217.534	9,597	6,854	200,500	10,976	8.232	192.136		740	29,124	22,972	253.439	21,943	15,789	224.692	25.597	19.444		
340	10,959	8,131	218.694	9,889	7,062	201.371	11,314	8,487 1	193.144		750	29,629	23,393	254.117	22.258	16.022	225 115	25 077	10 7/1		
350	11,351	8,439	219.831	10,181	7,271	202.217	11,652	8,742 1	94.125		760	30,135	23,817	254.787	22,573	16,255	225.533	26 358	20.030		
360	11,748	8,752	220.948	10,473	7,480	203.040	11,992	8,998 1	95.081	(r	770	30,644	24,242	255.452	22,890	16,488	225.947	26,741	20,039		
370	12,148	9,068	222.044	10,765	7,689	203.842	12,331	9,255 15	96.012		780	31,154	24,669	256.110	23,208	16,723	226.357	27,125	20,639		
390	12,960	9,718	224.182	11,351	8,108	205.383	13.014	9,515 19	7 807		790	31,665	25,097	256.762	23,526	16,957	226.762	27,510	20,941		
400	13,372	10,046	225.225	11,644	8,319	206.125	13.356 1	0.030 19	8.673		800	32,179	25,527	257.408	23,844	17,193	227.162	27 896	21 245	1	
410	13,787	10,378	226.250	11,938	8,529	206.850	13,699 1	0,290 19	9.521		810	32,694	25,959	258.048	24,164	17,429	227.559	28,284	21,245	1	
420	14,206	10,714	227.258	12,232	8,740	207.549	14,043 1	0,551 200	0.350		820	33,212	26,394	258.682	24,483	17,665	227.952	28.672	21.855		
430	14,628	11,053	228.252	12,526	8,951	208.252	14,388 1	0,813 20	1.160		830	33,730	26,829	259.311	24,803	17,902	228.339	29,062	22,162		
450	15 483	11 742	230 194	13 116	0.375	200.502	15 090 1	1,073 201	1.333		040	34,251	27,267	259.934	25,124	18,140	228.724	29,454	22.470	1	
460	15,916	12,091	231.144	13,412	9,587	210.243	15,428 1	1.603 203	.497		850	34,773	27,706	260.551	25,446	18,379	229.106	20.846	22 770	1	
470	16,351	12,444	232.080	13,708	9,800	210.880	15,777 1	1,869 204	.247		970	35,296	28,125	261.164	25,768	18 617	229.482	30 240	22,779	1	
480	16,791	12,800	233.004	14,005	10,014	211.504	16,126 12	135 204	.982	_ L	880	35,821	28,588	261.770	26,091	18,858	229.856	30,635	23,090	1	
490	17,232	13,158	233.916	14,302	10,228	212.117	16,477 12	,403 205	.705		890	36 976	29,031	262.371	26,415	19,099	230.227	31.032	23 715	1	
510	17,678	13,521	234.814	14,600	10,443	212.719	16,828 12	,671 206.	.413		900	010,070	29,476	262.968	26,740	19,341	230.593	31,429	24.029	1	
520	18,576	14,253	236.575	15,197	10,874	213.890	17,534 13	211 207.	799		910	37,405	29,922	263.559	27,066	19,583	230.957	31 828	24 245	l	
530	19,029	14,622	237.439	15,497	11,090	214.460	17,889 13	,482 208.	475		920	38.467	30,369	264.146	27,392	19,826	231.317	32.228	24,545	1	
54	19,485	14,996	238.292	15,797	11,307	215.020 1	8,245 13	,755 209.	139		930	39,000	31,268	264.728	27,719	20,070	231.674	32,629	24,980		
550	19,945	15,372	239.135	16,097	11,524	215.572 1	8,601 14	028 209.	795		940	39,535	31,719	265.877	28,046	20,314	232.028	33,032	25,300	1	
57	0 20,870	16,131	240.789	16,701	11,961	216.649 1	9,318 14,	579 211.0	075	1	950	40,070	32,171	266.444	28,703	20,359	232.379	33,436	25,621	2	
58	0 21,337	16,515	.241.602	17,003	12,181	217.175 1	9,678 14,	856 211.7	702	1	970	40,607	32,625 33,081	267.007	29,033	21,051	233.072	33,841	25,943	21	
59	0 21,807	16,902	242.405	17,307	12,401	217.693 2	0,039   15,	134 212.3	320		990	41.685	33.537	268.119	29,362	21,298	233.413	34,653	26,588	23	

Tables from Moran et al., 8<sup>th</sup> ed., Wiley.