A system consists of a copper tank with a mass of $13 \mathrm{~kg}, 4 \mathrm{~kg}$ of liquid water, and an electrical resistor of negligible mass. The system is insulated on its outer surface. Initially, the temperature of the copper is 27 ${ }^{\circ} \mathrm{C}$ and the temperature of the water is $50^{\circ} \mathrm{C}$. The electrical resistor transfers 100 kJ of energy to the system. Eventually the system comes to equilibrium. Determine the final equilibrium temperature in ${ }^{\circ} \mathrm{C}$.


SOLUTION:
Apply the First Law to a system consisting of the copper, water, and resistor,

$$
\begin{equation*}
\Delta E_{\text {sys }}=Q_{\substack{\text { into } \\ \text { sys }}}+\underset{\substack{\text { into } \\ \text { sys }}}{W_{\text {sys }}}=\Delta U_{\text {sys }}+\underset{\substack{\text { into } \\ \text { sys }}}{W_{\text {st }}} \tag{1}
\end{equation*}
$$

where the change in total energy in the system consists only of the change
 in internal energy. There is no heat transfer into or out of the system since the copper tank is insulated, i.e., $Q_{\text {into sys }}=0$. The work into the system is the electrical work into the resistor, $W_{\text {into sys }}=100 \mathrm{~kJ}$. The change in internal energy is,

$$
\begin{equation*}
\Delta U_{\mathrm{sys}}=m_{\mathrm{Cu}} \Delta u_{\mathrm{Cu}}+m_{\mathrm{H}_{2} \mathrm{O}} \Delta u_{\mathrm{H}_{2} \mathrm{O}} . \text { (The resistor mass is negligible.) } \tag{2}
\end{equation*}
$$

Treating the copper and water as incompressible substances,

$$
\begin{align*}
& \Delta u_{\mathrm{Cu}}=c_{\mathrm{Cu}} \Delta T_{\mathrm{Cu}}=c_{\mathrm{Cu}}\left(T_{2, \mathrm{Cu}}-T_{1, \mathrm{Cu}}\right),  \tag{3}\\
& \Delta u_{\mathrm{H}_{2} \mathrm{O}}=c_{\mathrm{H}_{2} \mathrm{O}} \Delta T_{\mathrm{H}_{2} \mathrm{O}}=c_{\mathrm{H}_{2} \mathrm{O}}\left(T_{2, \mathrm{H}_{2} \mathrm{O}}-T_{1, \mathrm{H}_{2} \mathrm{O}}\right) . \tag{4}
\end{align*}
$$

Note that the final temperatures of the water and copper will be the same, i.e., $T_{2, \mathrm{Cu}}=T_{2, \mathrm{H} 2 \mathrm{O}}=T_{2}$.
Simplifying Eq. (1), making use of Eqs. (2) - (4),

$$
\begin{align*}
& m_{\mathrm{Cu}} c_{\mathrm{Cu}}\left(T_{2}-T_{1, \mathrm{Cu}}\right)+m_{\mathrm{H}_{2} \mathrm{O}} c_{\mathrm{H}_{2} \mathrm{O}}\left(T_{2}-T_{1, \mathrm{H}_{2} \mathrm{O}}\right)=W_{\substack{\text { into } \\
\text { sys }}},  \tag{5}\\
& \left(m_{\mathrm{Cu}} c_{\mathrm{Cu}}+m_{\mathrm{H}_{2} \mathrm{O}} c_{\mathrm{H}_{2} \mathrm{O}}\right) T_{2}=W_{\substack{\text { into } \\
\text { sys }}}+m_{\mathrm{Cu}} c_{\mathrm{Cu}} T_{1, \mathrm{Cu}}+m_{\mathrm{H}_{2} \mathrm{O}} c_{\mathrm{H}_{2} \mathrm{O}} T_{1, \mathrm{H}_{2} \mathrm{O}},  \tag{6}\\
& T_{2}=\frac{W_{\substack{\text { into } \\
\text { sys }}}+m_{\mathrm{Cu}} c_{\mathrm{Cu}} T_{1, \mathrm{Cu}}+m_{\mathrm{H}_{2} \mathrm{O}} c_{\mathrm{H}_{2} \mathrm{O}} T_{1, \mathrm{H}_{2} \mathrm{O}}}{m_{\mathrm{Cu}} c_{\mathrm{Cu}}+m_{\mathrm{H}_{2} \mathrm{O}} c_{\mathrm{H}_{2} \mathrm{O}}} . \tag{7}
\end{align*}
$$

Substitute the given values,

$$
\begin{aligned}
& W_{\text {into sys }}=100 \mathrm{~kJ} \\
& c_{\mathrm{Cu}, 300 \mathrm{~K}}=0.385 \mathrm{~kJ} /(\mathrm{kg} . \mathrm{K}) \quad \text { (from thermodynamic table, e.g., Table A-19 of Moran et al., } 7^{\text {th }} \text { ed.) } \\
& c_{\mathrm{H} 2 \mathrm{O}, 300 \mathrm{~K}}=4.179 \mathrm{~kJ} /(\text { kg. } \mathrm{K}) \text { (from thermodynamic table, e.g., Table A-19 of Moran et al., } 7^{\mathrm{th}^{\text {th }} \mathrm{ed} \text {.) }} \begin{array}{l}
m_{\mathrm{Cu}}=13 \mathrm{~kg} \\
m_{\mathrm{H} 2 \mathrm{O}}=4 \mathrm{~kg} \\
T_{1, \mathrm{Cu}}=27^{\circ} \mathrm{C}=300 \mathrm{~K} \\
T_{1, \mathrm{H} \mathrm{HO}}=50^{\circ} \mathrm{C}=323 \mathrm{~K} \\
\Rightarrow T_{2}=322 \mathrm{~K}=49.3^{\circ} \mathrm{C}
\end{array}
\end{aligned}
$$

## TABLE A-19

Properties of Selected Solids and Liquids: $\boldsymbol{c}_{\boldsymbol{p}}, \rho$, and $\kappa$

| Substance | $\begin{aligned} & \text { Specific } \\ & \text { Heat, } c_{p} \\ & (\mathbf{k} / / \mathbf{k g} \cdot K) \end{aligned}$ | Density, $\stackrel{\rho}{\left(\mathrm{kg} / \mathrm{m}^{3}\right)}$ | Thermal Conductivity, $\kappa$ (W/m $\cdot \mathrm{K}$ ) |
| :---: | :---: | :---: | :---: |
| Selected Solids, 300K |  |  |  |
| Aluminum | 0.903 | 2700 | 237 |
| Coal, anthracite | 1.260 | 1350 | 0.26 |
| Copper | 0.385 | 8930 | 401 |
| Granite | 0.775 | 2630 | 2.79 |
| Iron | 0.447 | 7870 | 80.2 |
| Lead | 0.129 | 11300 | 35.3 |
| Sand | 0.800 | 1520 | 0.27 |
| Silver | 0.235 | 10500 | 429 |
| Soil | 1.840 | 2050 | 0.52 |
| Steel (AISI 302) | 0.480 | 8060 | 15.1 |
| Tin | 0.227 | 7310 | 66.6 |

## Building Materials, 300K

| Brick, common | 0.835 | 1920 | 0.72 |
| :--- | ---: | ---: | ---: |
| Concrete (stone mix) | 0.880 | 2300 | 1.4 |
| Glass, plate | 0.750 | 2500 | 1.4 |
| Hardboard, siding | 1.170 | 640 | 0.094 |
| Limestone | 0.810 | 2320 | 2.15 |
| Plywood | 1.220 | 545 | 0.12 |
| Softwoods (fir, pine) | 1.380 | 510 | 0.12 |


| Insulating Materials, 300K |  |  |  |
| :---: | :---: | :---: | :---: |
| Blanket (glass fiber) | - | 16 | 0.046 |
| Cork | 1.800 | 120 | 0.039 |
| Duct liner (glass fiber, coated) | 0.835 | 32 | 0.038 |
| Polystyrene (extruded) | 1.210 | 55 | 0.027 |
| Vermiculite fill (flakes) | 0.835 | 80 | 0.068 |
| Saturated Liquids |  |  |  |
| Ammonia, 300K | 4.818 | 599.8 | 0.465 |
| Mercury, 300K | 0.139 | 13529 | 8.540 |
| Refrigerant 22, 300K | 1.267 | 1183.1 | 0.085 |
| Refrigerant 134a, 300K | 1.434 | 1199.7 | 0.081 |
| Unused Engine Oil, 300K | 1.909 | 884.1 | 0.145 |
| Water, 275 K | 4.211 | 999.9 | 0.574 |
| 300 K | 4.179 | 996.5 | 0.613 |
| 325 K | 4.182 | 987.1 | 0.645 |
| 350K | 4.195 | 973.5 | 0.668 |
| 375K | 4.220 | 956.8 | 0.681 |
| 400K | 4.256 | 937.4 | 0.688 |

Sources: Drawn from several sources, these data are only representative. Values can vary depending on temperature, purity, moisture content, and other factors.
Table from Moran et al., $7^{\text {th }}$ ed.

