## Fall 2005 EE595S Homework Assignment Number 5 Solution

Problem 1

N/A.

Problem 2

N/A. See text for start/end points.

Problem 3

Our control law is

$$v_{qs}^{r*} = \underbrace{\omega_r L_d i_{ds}^r + \omega_r \lambda_m}_{v_{qs,ff}^{r*}} + \underbrace{K \left(1 + \frac{1}{\tau s}\right) \left(i_{qs}^{r*} - i_{qs}^r\right)}_{v_{sg,fg}^{r*}}$$

which yields a transfer function of

$$i_{qs}^{r} = \frac{K(\tau s + 1)}{(r_s + K)\tau s + K} i_{qs}^{r*} + \frac{\tau s}{(r_s + K)\tau s + K} \Delta v_{qs}^{r}$$

In order to be able to neglect the low pass filter on the transfer function, we should set the closed loop pole so as the transfer function has a cut-off frequency an order of magnitude lower than the closed loop pole. Thus we have

$$\frac{(r_s + K)\tau 2\pi 200}{K} = 1$$

However, we have two degrees of freedom, K and  $\tau$ . From our control law and transfer function observe two considerations. First, as we keep K small, it will keep current ripple from entering our current command. Second, if we keep K large relative to  $r_s$ , then in will reduce the sensitivity of the control performance on the machine parameters. As a compromise, let's choose  $K = 10r_s$  which yields a value of 2 Ohms. Then we can set

$$\tau = \frac{K}{(r_s + K)2\pi 200} = 0.72 \text{ ms}$$

Consider an indirect current control as shown in Fig. 3.5-1 and 3.5-2 of [2]. Suppose the switching frequency is 20 kHz, and that the low pass filter has a cut-off frequency of 2 kHz. Further suppose that  $r_s = 0.2$  Ohms. Select an appropriate value of K and  $\tau$ . Plot the magnitude and phase of the transfer function between  $i_{qs}^{r^*}$  (input) and  $i_{qs}^r$  (output) as well as  $\Delta v_{qs}^r$  (input) and  $i_{qs}^r$  (output).

### Problem 4

I would be a wound rotor induction motor because I like well defined current paths.

### Problem 5

N/A. See text for start/end points.

### Problem 6

N/A. See text for start/end points.

# Problem 7

N/A. See text for start/end points.

### Problem 8

Barring an algebraic error, the result is:  $T_e = -\frac{3}{2} \frac{P}{2} \frac{\omega_r r_r' L_M^2}{r_r'^2 + \omega_r^2 L_{rr}^2} i_{dc}^2$ 

### Reference

- [1] Analysis of Electric Machinery and Drive Systems
- [2] Analysis and Design of Permanent Magnet Synchronous Machines