

1.1 The exact expression for the received Doppler shifted frequency (incorporating relativistic effects) is

$$f_R = f_T \frac{1 - \dot{R}/c}{1 + \dot{R}/c} . \text{ Thus } f_{D,R} = f_R - f_T = \frac{-2\dot{R}/c}{1 + \dot{R}/c} f_T .$$

The common approximation for the Doppler shift in the signal is

$$f_D = -\frac{2\dot{R}}{\lambda} = -2(\dot{R}/c) f_T .$$

Thus the error in the approximation is

$$\begin{aligned} \Delta f_D &= f_D - f_{D,R} = \frac{-2(\dot{R}/c) f_T (1 + \dot{R}/c) + 2(\dot{R}/c) f_T}{1 + \dot{R}/c} \\ &= -\frac{2(\dot{R}/c)^2}{1 + \dot{R}/c} f_T \end{aligned}$$

Thus the relative error is $\epsilon_R = \frac{\Delta f_D}{f_{D,R}} = \frac{(-2(\dot{R}/c)^2 f_T)}{(\frac{2(\dot{R}/c) f_T}{1 + \dot{R}/c})} = \dot{R}/c$

For $\dot{R} = 300 \text{ m/s}$, $\dot{R}/c = 10^{-6}$

$$\therefore \epsilon_R = \boxed{10^{-6}} = \boxed{0.0001 \%}$$

1.2 (a) The total power received by antenna G_2 is

$$P_{\text{TOT},2} = \frac{P_T \lambda^2 G_1 G_2}{(4\pi)^2 R^2} \quad (\text{using the Friis equation written with gains})$$

Half of this power goes to the receiver attached to G_2 and half is retransmitted by the antenna with gain G_2

$$\text{Thus the receiver sees } P_R = \frac{P_T \lambda^2 G_1 G_2}{2(4\pi)^2 R^2} .$$

Thus the scattered power received by antenna G_1 is

$$P_S = \frac{P_R \lambda^2 G_1 G_2}{(4\pi)^2 R^2} = \frac{P_T \lambda^4 G_1^2 G_2^2}{2(4\pi)^4 R^4} \quad (\text{recall the half of the power retransmitted equals } P_R)$$

and thus the ratio of P_R/P_S is

$$\frac{P_R}{P_S} = \boxed{\frac{(4\pi)^2}{G_1 G_2} \left(\frac{R}{\lambda}\right)^2}$$

(b) Taking $G_1 = G_2 = 100$ and $\frac{R}{\lambda} = 10^4$, we have

$$\frac{P_R}{P_S} = \frac{(4\pi)^2}{(100)(100)} (10^4)^2 = \boxed{1.57914 \times 10^6 = 61.98 \text{ dB}}$$

1.3 The police radar receives signal power

$$P_R = \frac{P_T G^2 \lambda^2 \sigma}{(4\pi)^3 R^4} = \frac{P_T (100)^2 (0.02\text{m})^2 \sigma}{(4\pi)^3 (50\text{m})^4} = \frac{P_T \sigma \cdot 10^{-8}}{\pi^3} \left(\frac{1}{\text{W}\cdot\text{m}^2}\right)$$

The radar detector receives power

$$P_D = \frac{A_T A_D P_T}{\lambda^2 R_D^2} = \frac{\left(\frac{\lambda^2 G_T}{4\pi}\right) k \sigma P_T}{4\pi \lambda^2 R_D^2} = \frac{0.025 P_T \sigma}{\pi R_D^2}$$

If the two receivers have identical sensitivities, they must have equal received power for signal detection. Thus $P_D = P_R$. Setting these two expressions equal and solving for R_D , we get

$$\frac{P_T \sigma \cdot 10^{-8}}{\pi} = \frac{0.025 P_T \sigma}{\pi R_D^2} \text{ m}^2 \Rightarrow R_D^2 = 2.5\pi^2 \times 10^6 \text{ m}^2$$

$$\Rightarrow R_D = 1581\pi \text{ m} = 4967 \text{ m}$$

$$= \boxed{4.967 \text{ km} \approx 5 \text{ km}}$$

1.4 $A_T = \pi r_T^2 = \pi (1\text{m})^2 = \pi \text{ (m}^2\text{)}$

$$A_R = \alpha_R A_{RG} = 0.6 \pi (32\text{m})^2 = (614.4)\pi \text{ (m}^2\text{)}$$

$$= 1930.19 \text{ (m}^2\text{)}$$

$$P_R = \frac{P_T A_T A_R}{\lambda^2 R^2} = \frac{(50\text{ W})(\pi \text{ m}^2)(1930.2 \text{ m}^2)}{(0.1\text{ m})^2 (10^9 \text{ m})^2}$$

$$= \boxed{3.032 \times 10^{-11} \text{ W}}$$

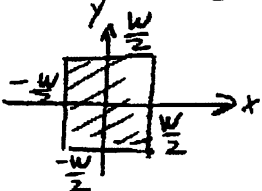
$$1.5 \quad G(\theta, \phi) = \frac{4\pi A_{TG}}{\lambda^2} f(\theta, \phi)$$

$$\text{where } f(\theta, \phi) = \frac{1}{A_{TG}} \cdot \left| \iint_{A_{TG}} \exp \left\{ i \frac{2\pi}{\lambda} [x \sin \theta + y \sin \phi] \right\} E(x, y) dx dy \right|^2$$

$$\iint_{A_{TG}} |E(x, y)|^2 dx dy$$

For small angles θ and ϕ such that $\sin \theta \approx \theta$ and $\sin \phi \approx \phi$, and a uniform aperture illumination of E_0 over the square aperture with sides of length

W as specified we have that

$$f(\theta, \phi) = \frac{1}{W^2} \left| \int_{-W/2}^{W/2} \int_{-W/2}^{W/2} E_0 \exp \left\{ i \frac{2\pi}{\lambda} [x\theta + y\phi] \right\} dx dy \right|^2$$


$$\int_{-W/2}^{W/2} \int_{-W/2}^{W/2} |E_0|^2 dx dy$$

Clearly $\int_{-W/2}^{W/2} \int_{-W/2}^{W/2} |E_0|^2 dx dy = W^2 |E_0|^2$, and

$$\int_{-W/2}^{W/2} \int_{-W/2}^{W/2} E_0 \exp \left\{ i \frac{2\pi}{\lambda} [x\theta + y\phi] \right\} dx dy = E_0 \int_{-W/2}^{W/2} \exp \left\{ i \frac{2\pi}{\lambda} x\theta \right\} dx \int_{-W/2}^{W/2} \exp \left\{ i \frac{2\pi}{\lambda} y\phi \right\} dy$$

$$= E_0 \left[W \frac{\sin(\pi W \theta / \lambda)}{(\pi W \theta / \lambda)} \right] \left[W \frac{\sin(\pi W \phi / \lambda)}{(\pi W \phi / \lambda)} \right]$$

Thus $f(\theta, \phi)$ becomes

$$f(\theta, \phi) = \frac{1}{W^2} \frac{|E_0|^2 W^4 \left[\frac{\sin(\pi W \theta / \lambda)}{(\pi W \theta / \lambda)} \right]^2 \left[\frac{\sin(\pi W \phi / \lambda)}{(\pi W \phi / \lambda)} \right]^2}{|E_0|^2 W^2}$$

$$= \left[\frac{\sin(\pi W \theta / \lambda)}{(\pi W \theta / \lambda)} \right]^2 \left[\frac{\sin(\pi W \phi / \lambda)}{(\pi W \phi / \lambda)} \right]^2$$

Thus we have

$$G(\theta, \phi) = \frac{4\pi W^2}{\lambda^2} \left[\frac{\sin(\pi W \theta / \lambda)}{(\pi W \theta / \lambda)} \right]^2 \left[\frac{\sin(\pi W \phi / \lambda)}{(\pi W \phi / \lambda)} \right]^2$$

$$1.6. \quad E(\theta, \phi) = \frac{4\pi A_{TG}}{\lambda^2} f(\theta, \phi)$$

where

$$f(\theta, \phi) = \frac{1}{A_{TG}} \cdot \frac{\left| \iint_{A_{TG}} \exp\left\{i\frac{2\pi}{\lambda} [x \sin\theta + y \sin\phi]\right\} E(x, y) dx dy \right|^2}{\iint_{A_{TG}} |E(x, y)|^2 dx dy} \quad \dots (*)$$

In this case, $A_{TG} = \pi \left(\frac{D}{2}\right)^2 = \frac{\pi D^2}{4}$, and

$$\iint_{A_{TG}} |E(x, y)|^2 dx dy = \frac{\pi D^2}{4} |E_0|^2$$

The numerator is given by

$$\begin{aligned} & \iint_{A_{TG}} \exp\left\{i\frac{2\pi}{\lambda} (x \sin\theta + y \sin\phi)\right\} E_0 dx dy \\ &= E_0 \iint_{A_{TG}} \exp\left\{-i2\pi \left[x \left(-\frac{\sin\theta}{\lambda}\right) + y \left(-\frac{\sin\phi}{\lambda}\right)\right]\right\} dx dy \\ &= E_0 G\left(-\frac{\sin\theta}{\lambda}, -\frac{\sin\phi}{\lambda}\right) \quad \dots (**) \end{aligned}$$

where

$$G(u, v) = \iint_{\mathbb{R}^2} g(x, y) \exp\{-i2\pi [ux + yv]\} dx dy$$

is the 2-dimensional Fourier transform of the unit-magnitude disk of radius $a = D/2$ given by

$$g(x, y) = \frac{1}{[0, a]} (\sqrt{x^2 + y^2}) = \begin{cases} 1, & \sqrt{x^2 + y^2} \leq a \\ 0, & \sqrt{x^2 + y^2} > a. \end{cases}$$

So our next task is to compute the two-dimensional Fourier transform $G(u, v)$ of $g(x, y)$.

$$\text{Let } g(x, y) = \frac{1}{[0, a]} (\sqrt{x^2 + y^2}) = \begin{cases} 1, & \sqrt{x^2 + y^2} \leq a \\ 0, & \sqrt{x^2 + y^2} > a \end{cases}$$

We wish to find the two-dimensional Fourier transform

$$G(u, v) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} g(x, y) \exp\{-i2\pi(ux + vy)\} dx dy$$

We note that if we write $g(x, y)$ in polar coordinates with

$$x = r \cos \psi$$

$$y = r \sin \psi$$

we have

$$g_p(r, \psi) = g(r \cos \psi, r \sin \psi) = \hat{g}(r) = \frac{1}{[0, a]}(r)$$

because $g(x, y)$ is circularly symmetric.

Because $g(x, y)$ is circularly symmetric, $G(u, v)$ is also circularly symmetric in u and v . Thus it follows that we can write

$$u = \rho \cos \beta$$

$$v = \rho \sin \beta.$$

We can then write

$$\begin{aligned} G(u, v) &= \mathcal{G}(\rho, \beta) \\ &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} g(r \cos \psi, r \sin \psi) \exp\{-i2\pi(u r \cos \psi + v r \sin \psi)\} \left| \frac{\partial(x, y)}{\partial(r, \psi)} \right| dr d\psi \\ &= \int_0^{\infty} \int_0^{2\pi} r \hat{g}(r) \exp\{-i2\pi(\rho \cos \beta r \cos \psi + \rho \sin \beta r \sin \psi)\} dr d\psi \\ &= \int_0^{\infty} r \hat{g}(r) \int_0^{2\pi} \exp\{-i2\pi r \rho \cos(\psi - \beta)\} d\psi dr \end{aligned}$$

Now the Bessel function of the first kind, order zero, can be written as

$$J_0(a) = \frac{1}{2\pi} \int_0^{2\pi} \exp\{-ia \cos(\psi - \beta)\} d\psi \quad (G \& R \ 8.411.1)$$

Thus it follows that

$$\hat{g}(\rho, \beta) = \hat{g}_2(\rho) = 2\pi \int_0^{\infty} r \hat{g}(r) J_0(2\pi\rho r) dr$$

This is true for any circularly symmetric $g(x, y) = \hat{g}(\sqrt{x^2 + y^2}) = \hat{g}(r)$. For our particular $g(x, y) = \hat{g}(r) = \frac{1}{[0, a]}$ this becomes

$$\hat{g}_2(\rho, \beta) = \hat{g}_2(\rho) = 2\pi \int_0^a r J_0(2\pi\rho r) dr.$$

Now using the identity

$$\int_0^x z J_0(z) dz = x J_1(x),$$

where $J_1(\cdot)$ is the Bessel function of the first kind, order one, we have

$$\begin{aligned} \hat{g}_2(\rho) &= 2\pi \int_0^a r J_0(2\pi\rho r) dr \\ &= 2\pi \int_0^{2\pi\rho a} \frac{z}{2\pi\rho} J_0(z) \frac{dz}{2\pi\rho} = \frac{2\pi}{(2\pi\rho)^2} \int_0^{2\pi\rho a} z J_0(z) dz \\ &= \frac{2\pi}{(2\pi\rho)^2} \cdot 2\pi\rho a \cdot J_1(2\pi\rho a) \\ &= \frac{a}{\rho} \cdot J_1(2\pi\rho a) \end{aligned}$$

Now noting that $\rho = \sqrt{u^2 + v^2}$, we have

$$G(u, v) = \frac{a}{\sqrt{u^2 + v^2}} J_1(2\pi a \sqrt{u^2 + v^2})$$

Now going back to equation (***) in our aperture problem, we have

$$\begin{aligned}
 E_0 G\left(-\frac{\sin\theta}{\lambda}, -\frac{\sin\phi}{\lambda}\right) &= E_0 \frac{a\lambda}{\sqrt{\sin^2\theta + \sin^2\phi}} \cdot J_1\left(\frac{2\pi}{\lambda} a \sqrt{\sin^2\theta + \sin^2\phi}\right) \\
 &= \frac{E_0 \lambda D}{2\sqrt{\sin^2\theta + \sin^2\phi}} \cdot J_1\left(\frac{\pi D}{\lambda} \sqrt{\sin^2\theta + \sin^2\phi}\right)
 \end{aligned}$$

Now substituting into equation (**), we get

$$\begin{aligned}
 G(\theta, \phi) &= \frac{4\pi}{\lambda^2} \cdot \frac{|E_0|^2 \lambda^2 D^2}{4(\sin^2\theta + \sin^2\phi)} \cdot J_1^2\left(\frac{\pi D}{\lambda} \sqrt{\sin^2\theta + \sin^2\phi}\right) \\
 &= \frac{4}{(\sin^2\theta + \sin^2\phi)} \cdot J_1^2\left(\frac{\pi D}{\lambda} \sqrt{\sin^2\theta + \sin^2\phi}\right) \\
 &= \frac{4 \cdot J_1^2\left(\frac{\pi D}{\lambda} \sqrt{\sin^2\theta + \sin^2\phi}\right)}{(\sin^2\theta + \sin^2\phi)}
 \end{aligned}$$

$$= \frac{4\pi^2 D^2}{\lambda^2} \left[\frac{J_1\left(\frac{\pi D}{\lambda} \sqrt{\sin^2\theta + \sin^2\phi}\right)}{\frac{\pi D}{\lambda} \sqrt{\sin^2\theta + \sin^2\phi}} \right]^2$$

$$\therefore G(\theta, \phi) = \frac{4\pi^2 D^2}{\lambda^2} \left[\frac{J_1\left(\frac{\pi D}{\lambda} \sqrt{\sin^2\theta + \sin^2\phi}\right)}{\frac{\pi D}{\lambda} \sqrt{\sin^2\theta + \sin^2\phi}} \right]^2$$

For $\theta, \phi \ll 1$, we can approximate this by

$$G(\theta, \phi) \approx \frac{4\pi^2 D^2}{\lambda^2} \left[\frac{J_1\left(\frac{\pi D}{\lambda} \sqrt{\theta^2 + \phi^2}\right)}{\frac{\pi D}{\lambda} \sqrt{\theta^2 + \phi^2}} \right]^2$$

$$\text{h.b.} \quad \lim_{z \rightarrow 0} \frac{J_1(z)}{z} = \frac{1}{2}$$

$$\Rightarrow G(0,0) = \frac{4\pi^2 D^2}{\lambda^2} \cdot \left(\frac{1}{2}\right)^2 = \frac{\pi^2 D^2}{\lambda^2}$$

and the gain of an aperture of area A_{TG} is

$$G = \frac{4\pi A_{TG}}{\lambda^2} = \frac{4\pi}{\lambda^2} \pi \left(\frac{D}{2}\right)^2 = \frac{4\pi^2 D^2}{\lambda^2 4} = \frac{\pi^2 D^2}{\lambda^2}$$

✓ check.

* An alternative method for computing the 2-dimensional Fourier transform of a function that is constant on a disk of radius a :

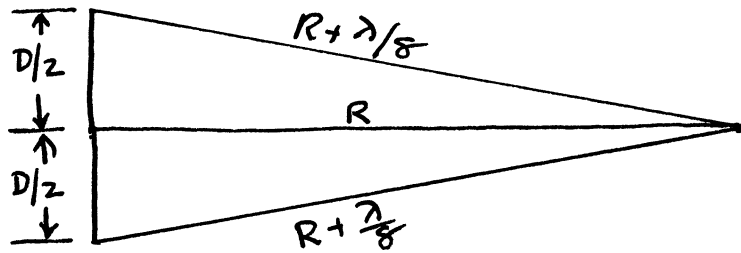
$$\begin{aligned} F(u,v) &= \iint_{\{(x,y): \sqrt{x^2+y^2} \leq a\}} K e^{-i2\pi(ux+vy)} dx dy \\ F(u,v) &= K \int_{-a}^a e^{-i2\pi vy} \int_{-\sqrt{a^2-y^2}}^{\sqrt{a^2-y^2}} e^{-i2\pi ux} dx dy \\ &= K \int_{-a}^a e^{-i2\pi vy} \left[\frac{e^{-i2\pi ux}}{-i2\pi u} \right]_{-\sqrt{a^2-y^2}}^{\sqrt{a^2-y^2}} dy \\ &= K \int_{-a}^a e^{-i2\pi vy} \left[\frac{e^{-i2\pi u\sqrt{a^2-y^2}} - e^{i2\pi u\sqrt{a^2-y^2}}}{-i2\pi u} \right] dy \\ &= \frac{K}{\pi u} \int_{-a}^a e^{-i2\pi vy} \sin[2\pi u\sqrt{a^2-y^2}] dy \\ &= \frac{2K}{\pi u} \int_0^a \cos(2\pi vy) \cdot \sin[2\pi u\sqrt{a^2-y^2}] dy \end{aligned}$$

using Table of integrals (e.g. Gr, p.399, entry 3.711)

$$\frac{Ka}{\sqrt{u^2+v^2}} \cdot J_1[2\pi a\sqrt{u^2+v^2}] = Ka \frac{J_1(2\pi a g)}{g}$$

where $g = \sqrt{u^2+v^2}$

1.7 A diagram of the situation under consideration appears as follows:



So if we solve for R in this diagram, we get the range at which the far-field starts.

By the Pythagorean Theorem, we have

$$(R + \lambda/8)^2 = R^2 + \frac{D^2}{4} \Rightarrow R^2 + \frac{R\lambda}{4} + \frac{\lambda^2}{64} = R^2 + \frac{D^2}{4}$$

$$\Rightarrow \frac{R\lambda}{4} + \frac{\lambda^2}{64} = \frac{D^2}{4} \Rightarrow \frac{R\lambda}{4} = \frac{D^2}{4} - \frac{\lambda^2}{64} \approx \frac{D^2}{4}, \text{ since } D^2 \gg \lambda^2$$

$$\therefore \boxed{R_{FF} \approx \frac{D^2}{\lambda}}$$

$$(a) \quad R_{FF} = \frac{(3\text{m})^2}{0.075\text{m}} = \frac{9\text{m}^2}{0.075\text{m}} = \boxed{120\text{m}}$$

$$(b) \quad R_{FF} = \frac{(100\text{m})^2}{0.075\text{m}} = \boxed{133333\text{m} \approx 133\text{km}}$$

$$(c) \quad R_{FF} = \frac{(30\text{m})^2}{0.01\text{m}} = \frac{900\text{m}^2}{0.01\text{m}} = 90000\text{m} = \boxed{90\text{km}}$$

$$(d) \quad R_{FF} = \frac{(3\text{m})^2}{6000\text{\AA}} = \frac{9\text{m}^2}{6 \times 10^{-9}\text{m}} = \boxed{1,500,000\text{m} = 15,000\text{km}}$$

1.8(a) The field strength on the aperture is $E_0 \exp\{-r^2/a^2\}$
 The total power falling on the aperture of diameter D is

$$\begin{aligned}
 P_D &= \iint_{\{x,y: x^2+y^2 \leq D^2/4\}} |E_0|^2 \exp\left(-\frac{r^2}{a^2}\right) dx dy = \int_0^{2\pi} \int_0^{D/2} |E_0|^2 \exp\left\{-\frac{r^2}{a^2}\right\} \left|\frac{d(x,y)}{d(r,\theta)}\right| dr d\theta \\
 &= 2\pi |E_0|^2 \int_0^{D/2} \exp\left\{-\frac{r^2}{a^2}\right\} |r| dr = 2\pi |E_0|^2 \left[\frac{-a^2 e^{-2r^2/a^2}}{4} \right]_0^{D/2} \\
 &= 2\pi |E_0|^2 \cdot \left(\frac{a^2}{4}\right) \left[1 - e^{-D^2/4a^2}\right] = \frac{\pi a^2 |E_0|^2}{2} \left[1 - e^{-D^2/4a^2}\right]
 \end{aligned}$$

The total power emitted from the feed is

$$P_{TOT} = P_D \Big|_{D=\infty} = \frac{\pi a^2 |E_0|^2}{2}$$

Thus the fraction of the power falling on the aperture is

$$\alpha(D) = \frac{P_D}{P_{TOT}} = 1 - e^{-D^2/4a^2}$$

(b) The aperture efficiency for the power falling on the aperture is

$$\eta_T = \frac{|\bar{E}|^2}{|\overline{|E|^2}} \quad \bar{E} = \frac{1}{A_{TG}} \iint_{A_{TG}} E(x,y) dx dy$$

$$A_{TG} = \frac{\pi D^2}{4} \quad |\overline{|E|^2}| = \frac{1}{A_{TG}} \iint_{A_{TG}} |E(x,y)|^2 dx dy$$

$$\begin{aligned}
 \bar{E} &= \frac{4}{\pi D^2} \iint_{A_{TG}} E_0 e^{-r^2/a^2} dx dy = \frac{4E_0}{\pi D^2} \int_0^{2\pi} \int_0^{D/2} \exp\left(-\frac{r^2}{a^2}\right) |r| dr \\
 &= \frac{8E_0}{D^2} \int_0^{D/2} r \exp\left[-\frac{r^2}{a^2}\right] dr = \frac{8E_0}{D^2} \cdot \left(\frac{a^2}{2}\right) \left[1 - e^{-D^2/4a^2}\right]
 \end{aligned}$$

$$\Rightarrow |\bar{E}|^2 = \frac{16 |E_0|^2 a^4}{D^4} \left[1 - e^{-D^2/4a^2}\right]^2 = \frac{16 |E_0|^2}{(D/a)^4} \left[1 - e^{-\frac{(D/a)^2}{4}}\right]^2$$

$$\begin{aligned} \overline{|E|^2} &= \frac{1}{A_{TG}} \iint |E(x,y)|^2 dx dy = \frac{4|E_0|^2}{\pi D^2} \int_0^{D/2} \int_0^{2\pi} |\exp(-\frac{r^2}{a^2})|^2 \cdot r dr d\theta \\ &= \frac{8|E_0|^2}{D^2} \int_0^{D/2} r \cdot \exp(-\frac{2r^2}{a^2}) dr = \frac{2|E_0|^2}{(D/a)^2} \left[1 - e^{-\frac{D^2}{2a^2}} \right] \end{aligned}$$

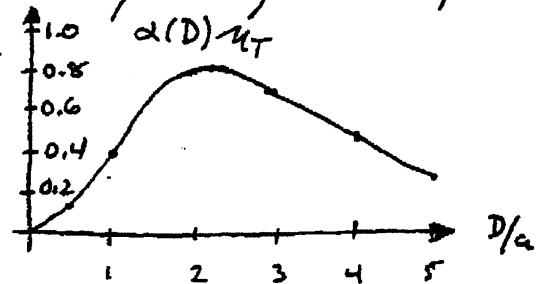
Hence the aperture efficiency of the aperture is

$$\eta_T = \frac{\overline{|E|^2}}{|E|^2} = \frac{8}{(D/a)^2} \cdot \frac{\left[1 - e^{-\frac{(D/a)^2}{4}} \right]^2}{\left[1 - e^{-\frac{(D/a)^2}{2}} \right]}$$

(c) The overall aperture efficiency is given by

$$\alpha(D)\eta_T = \frac{8}{(D/a)^2} \left[1 - e^{-\frac{(D/a)^2}{4}} \right]^2$$

This is the ratio of the effective area of the antenna to the geometric area.



(d) To find the value of D/a that maximizes $\alpha(D)\eta_T$, we need to find the value of the inflection point near 2. Taking the derivative of $\alpha(D)\eta_T$ w.r.t. $u = D/a$ and setting it equal to 0, we get

$$\begin{aligned} \frac{d}{du} (\alpha(D)\eta_T) &= \frac{8 e^{-u^2/4} (1 - e^{-u^2/4})}{u^3} - \frac{16 (1 - e^{-u^2/4})^2}{u^3} \\ &= \frac{8(1 - e^{-u^2/4})(2e^{-u^2/4} - u^2 - 2)}{e^{-u^2/4} u^3} = 0. \quad \text{Either } (1 - e^{-u^2/4}) = 0 \text{ or } (2e^{-u^2/4} - u^2 - 2) = 0 \end{aligned}$$

The first gives $u = D/a = 0$ (not interesting). The second is an even fn of u (via u^2) so it has roots $\pm(2 + \epsilon)$. Solving numerically for the positive (meaningful) root, we get

$$u = \boxed{D/a = 2.24181}$$

The fraction of the energy falling on the dish in this case is

$$\alpha(D) \Big|_{D/a=2.24181} = \left. 1 - \exp\left(-\frac{1}{2}\left(\frac{D}{a}\right)^2\right) \right|_{D/a=2.24181} = \boxed{0.919}$$

u.b. The total overall aperture efficiency (in order to use Friis Eq.) is

$$\alpha(D)\eta_T \Big|_{D/a=2.24181} = \left. \frac{8}{(D/a)^2} \left[1 - e^{-\frac{(D/a)^2}{4}} \right]^2 \right|_{D/a=2.24181} = 0.815$$