

## Session 5

Recall...

It appears we have derived this result for square transmit apertures and arbitrary receive apertures.

**Reciprocity Theorem:** For linear antenna systems,  $P_R/P_T$  remains the same when the roles of the transmit and receive antennas are reversed.

$\Rightarrow P_R/P_T$  proportional to uniformly illuminated area  $A_T$  regardless of shape.

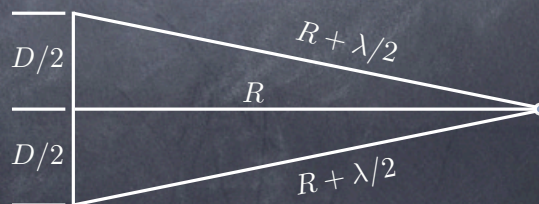
$$\therefore \boxed{\frac{P_R}{P_T} = \frac{A_T A_R}{\lambda^2 R^2}}$$

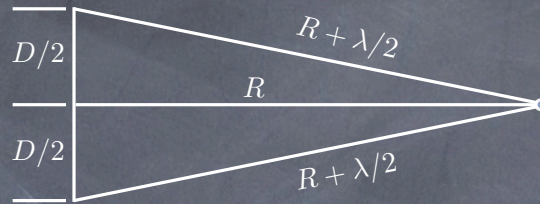
← The Friis Equation

- > Friis equation derived using scalar diffraction—scalar wave equation describes propagation.
- > Valid in other situations described by scalar wave equation:
  - > Acoustic radiation (in non-viscous media)
  - > Polarized light

- > Friis equation holds when antennas are “far apart.” How far?
- > Uniformly illuminated aperture focuses objects at infinity.
- > If we look at an antenna from close in, the edges appear farther away than the

A bad situation:





This bad situation occurs when

$$\left(R + \frac{\lambda}{2}\right)^2 = \left(\frac{D}{2}\right)^2 + R^2$$

$$\Rightarrow R = \frac{D^2 - \lambda^2}{4\lambda} \approx \frac{D^2}{4\lambda}, \quad \text{because } D \gg \lambda$$

Thus we want

$$R \gg \frac{D^2}{4\lambda}$$

Maybe 10 times bigger—or more!

A common approach is to consider a point to be in the far-field when the center and edges of the aperture differ by no more than  $\lambda/8$

If our calculations show

$$\frac{P_R}{P_T} = \frac{A_T A_R}{\lambda^2 R^2} > 1 \quad \Rightarrow \quad \text{Something is wrong!}$$

When such a situation occurs, a large fraction of the transmitted power is received by the receive aperture:

“Hertzian Cable”

This will not occur when  $R$  is such that the antennas are in each others far field.

## Effective Area of an Antenna

- > In deriving the Friis equation, we have assumed uniform aperture illumination.
- > Practically, this is hard to achieve.
- > When we do not have uniform illumination, the effective size of the aperture is smaller than the geometric area.
- > How much smaller?

Suppose  $E(x, y)$  is the field over the aperture (i.e.,  $E(x, y) \neq E_0$ .)

The power  $P_T$  flowing out over the aperture is

$$P_T = \frac{1}{Z_{FS}} \int \int_{A_{TG}} |E(x, y)|^2 dx dy,$$

The electric field at the receive aperture is

$$E_R = B \int \int_{A_{TG}} E(x, y) dx dy$$

↑  
constant

The total power at the receive aperture is

$$P_R = \frac{|E_R|^2}{Z_{FS}} A_R = \frac{A_R B^2}{Z_{FS}} \left| \int \int_{A_{TG}} E(x, y) dx dy \right|^2.$$

Thus we have

$$\frac{P_R}{P_T} = B^2 A_R \frac{\left| \int \int_{A_{TG}} E(x, y) dx dy \right|^2}{\int \int_{A_{TG}} |E(x, y)|^2 dx dy}$$

Now define the *spatial average field* across  $A_{TG}$

$$\bar{E} = \frac{1}{A_{TG}} \int \int_{A_{TG}} E(x, y) dx dy$$

and the *spatial mean-square field* across the aperture as

$$\overline{|E|^2} = \frac{1}{A_{TG}} \int \int_{A_{TG}} |E(x, y)|^2 dx dy$$

Hence

$$\frac{P_R}{P_T} = B^2 A_R A_{TG} \left[ \frac{\overline{|E|^2}}{\left| \bar{E} \right|^2} \right]$$

To find  $B$  in

$$\frac{P_R}{P_T} = B^2 A_R A_{TG} \left[ \frac{|\overline{E}|^2}{|E|^2} \right]$$

we note that when  $E(x, y) = E_0$  (uniform illum.  $\Rightarrow A_{TG} = A_T$ )

$$|\overline{E}|^2 = \overline{|E|^2} \quad \Rightarrow \quad B^2 = \frac{P_R}{P_T} \cdot \frac{1}{A_T A_R}$$

Thus  $A_T$  in the Friis equation is

$$A_T = A_{TG} \left[ \frac{|\overline{E}|^2}{|E|^2} \right] = \eta_T \cdot A_{TG}$$

and by reciprocity

$$A_R = A_{RG} \left[ \frac{|\overline{E}|^2}{|E|^2} \right] = \eta_R \cdot A_{RG}$$

Aperture Efficiency

## Effective Area

- Even antennas that don't have well defined apertures can be assigned effective areas for use in the Friis equation.
- Here we can use EM field theory to compute the field strength due to the transmit antenna at the receive aperture:

$$A_T = \frac{\lambda^2 R^2}{A_R} \cdot \frac{P_R}{P_T}$$

For example, for a half-wave dipole

$$A_T \approx 0.130\lambda^2$$

## Antenna Gain over an Isotropic Radiator

- ⑥ Isotropic Radiator: An antenna that radiates energy uniformly in all directions (transmit).
- ⑥ On receive, it is equally sensitive to energy from all directions (by reciprocity).

If at a distance  $R$  from an isotropic radiator, we place a receive aperture  $A_R$

$$\frac{P_R}{P_T} = \frac{A_R}{4\pi R^2}$$

← surface area of sphere of radius  $R$

$$\frac{P_R}{P_T} = \frac{A_R}{4\pi R^2} = \frac{A_i A_R}{\lambda^2 R^2} \Rightarrow \boxed{A_i = \frac{\lambda^2}{4\pi}}$$

$$\boxed{A_i = \frac{\lambda^2}{4\pi}}$$

- ⑥ Note that the usual requirements for aperture size are not met. )
- ⑥ However, it works in the Friis equation. )
- ⑥ For this reason we will find it useful. )

The *gain* of  $A_T$  over  $A_i$  is

$$G = \frac{(P_R/P_T)_T}{(P_R/P_T)_i} = \frac{(P_R)_T}{(P_R)_i} = \frac{4\pi A_T}{\lambda^2}$$

So in general, the relation between the effective area  $A$  and gain  $G$  of antenna is

$$G = \frac{4\pi A}{\lambda^2}$$

$$A = \frac{\lambda^2 G}{4\pi}$$

Gain is often expressed in dB:

$$G(\text{dB}) = 10 \log_{10} G \quad (\text{dB})$$

## Antenna Gain...

- By reciprocity, the gain of an antenna on transmit is equal to the gain of an antenna on receive.
- The Friis Equation can be written in terms of antenna gains:

$$\frac{P_R}{P_T} = \frac{G_T G_R \lambda^2}{16\pi^2 R^2}$$



# Antenna Directivity and Beam Pattern

For a uniformly illuminated aperture

$$G_T = \frac{4\pi A_{TG}}{\lambda^2}$$

If  $A_{TG}$  is not uniformly illuminated

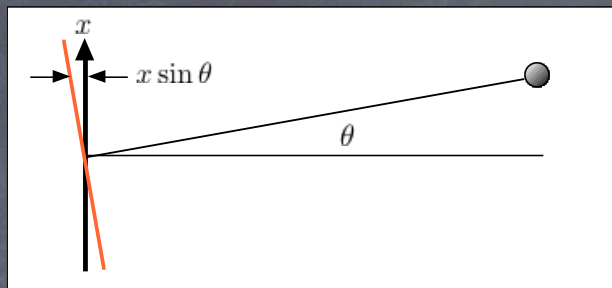
$$G_T = \frac{4\pi A_T}{\lambda^2} = \frac{4\pi A_{TG}}{\lambda^2} \eta$$

If we go off axis by  $\theta$  (azimuth) and  $\phi$  (elevation) the gain is not as large as in direction  $(\theta, \phi) = (0, 0)$ .

It can be written as

$$G(\theta, \phi) = \frac{4\pi A_{TG}}{\lambda^2} \cdot f(\theta, \phi)$$

Aperture Efficiency?  $\leftarrow$



Looking back at the aperture off-axis we see a "virtual aperture" with a phase shift across it.

In general, at angle  $(\theta, \phi)$  we have

$$G(\theta, \phi) = \frac{4\pi A_{TG}}{\lambda^2} \cdot f(\theta, \phi)$$

$$f(\theta, \phi) = \left( \frac{1}{A_{TG}} \right) \frac{\left| \int \int_{A_{TG}} \exp \left\{ i \frac{2\pi}{\lambda} [x \sin \theta + y \sin \phi] \right\} E(x, y) dx dy \right|^2}{\int \int_{A_{TG}} |E(x, y)|^2 dx dy}$$

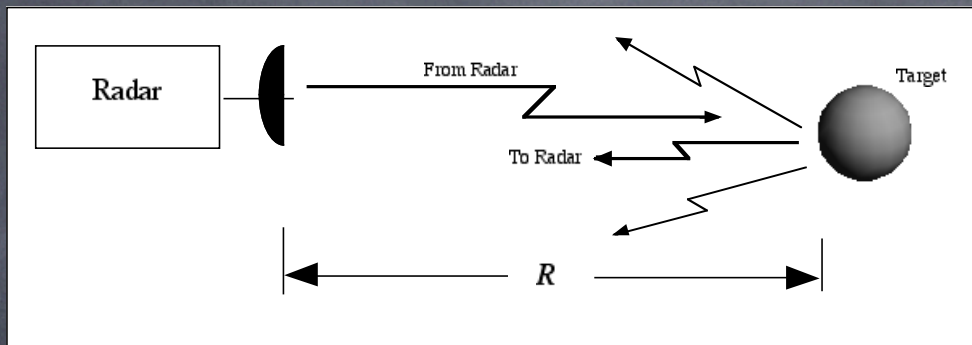
$$f(\theta, \phi) = \left( \frac{1}{A_{\text{TG}}} \right) \frac{\left| \int \int_{A_{\text{TG}}} \exp \left\{ i \frac{2\pi}{\lambda} [x \sin \theta + y \sin \phi] \right\} E(x, y) dx dy \right|^2}{\int \int_{A_{\text{TG}}} |E(x, y)|^2 dx dy}$$

This expression acts like an efficiency, taking on values between 0 and 1.

It provides a measure of the directivity of the antenna for transmitting and receiving power.

We call this quantity the beam pattern of the antenna.

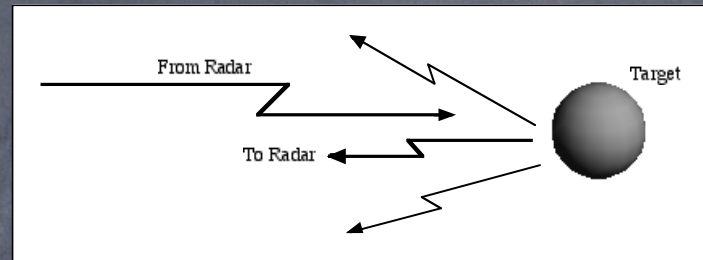
## The Radar Equation



Given that power  $P_T$  is transmitted, what is the received power  $P_R$ ?

To answer this, we must understand the target's behavior.

## Target Scattering Characteristics



Assume target has following characteristics:

- (i) As a receive aperture, it has  $A_R = \sigma \text{ (m}^2\text{)}$ ;
- (ii) It reradiates all of this received energy isotropically.

## Assumed Target Characteristics

- (i) As a receive aperture, it has  $A_R = \sigma \text{ (m}^2\text{)}$ ;
- (ii) It reradiates all of this received energy isotropically.

