

Processing a Coherent Pulse Train

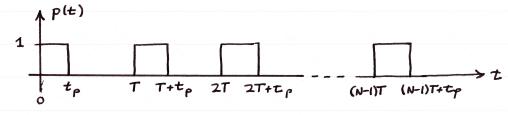
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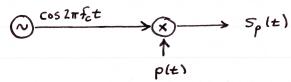
Assume a radar transmits a passband signal of the form

$$S_p(t) = p(t) \cos 2\pi f_c t$$

where

$$P(\xi) = \sum_{n=0}^{N-1} 1_{[o,t_p]} (t-nT).$$





$$r(t) = p(t) \cos \left[2\pi f_c t + \phi(t) \right].$$

(n.b. we have re-oriented the time origin to account for the round - trip delay)

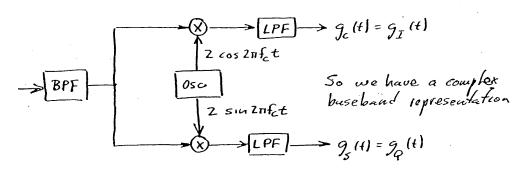
Here, \$11) is due to the Doppler shift:

$$\phi(\epsilon) = +2\pi \int_{D} t = -2\pi \frac{2\dot{R}}{\lambda} t. \qquad (monostatic)$$

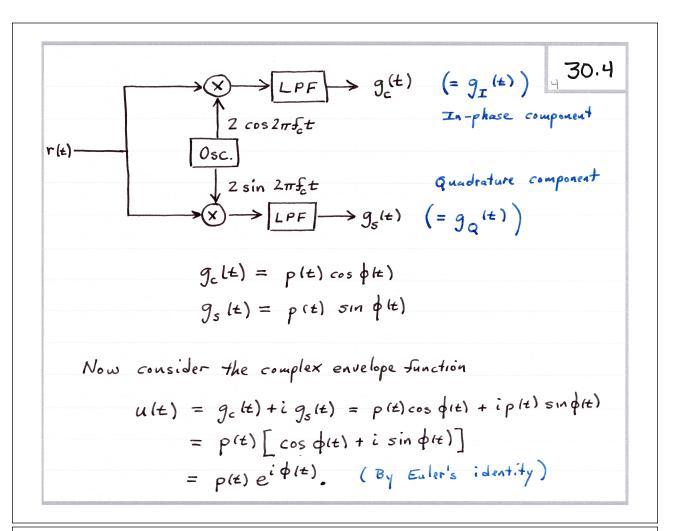
n.b. We are assuming p(t) is narrowband w.r.t. carrier fe and that time dialation/compression of p(t) is negligible. Narrowband Assumption

We would like to find the complex baseband representation of the received signal r(t) via processing:

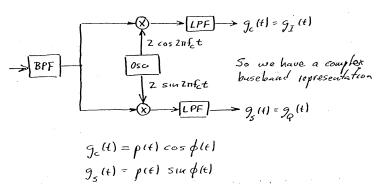
- Pass the signal through a bandpass filter that passes virtually all of the signal, but little outside of the signal's frequency band.
- Use an I/Q demodulator to get the in-phase and quadrature components.



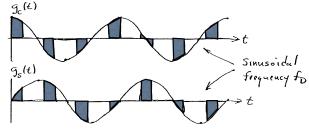
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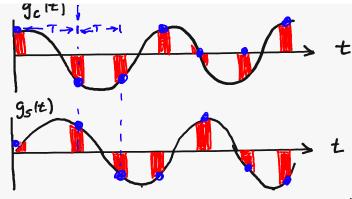
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For $\phi(t) = 2\pi f_D t$ as in our case, the two signals appear as follows:







Now we can form the complex envelope function

$$u(t) = g_c(t) + ig_s(t)$$

If we sample ult) at sampling instants to, t,, ..., tn-1

Such that tn-tn-1 = T, n=1,..., N-1

with to selected within the first pulse (O<to<tp)

we get one complex sample from each pulse return

Note that if we define the complex sequence

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$$U_n = U(t_n) = U(t_0 + nT), n = 0,1,...,N-1$$

and compute the DTFT of $\{U_n, 3\}$, we get

$$U(f) = \sum_{n=0}^{N-1} u_n e^{-i2\pi nTf} = \sum_{n=0}^{N-1} e^{i2\pi f_D(t_0 + nT)} e^{-i2\pi nTf}$$

$$= e^{i2\pi f_D t_0} \sum_{n=0}^{N-1} e^{-i2\pi (f - f_D)nT}$$

For
$$f = f_p \Rightarrow |U(f)| = N$$
,
For $f \not= f_p \Rightarrow |U(f)| \stackrel{\sim}{=} 0$.

N - IU(F) |

The F_oT

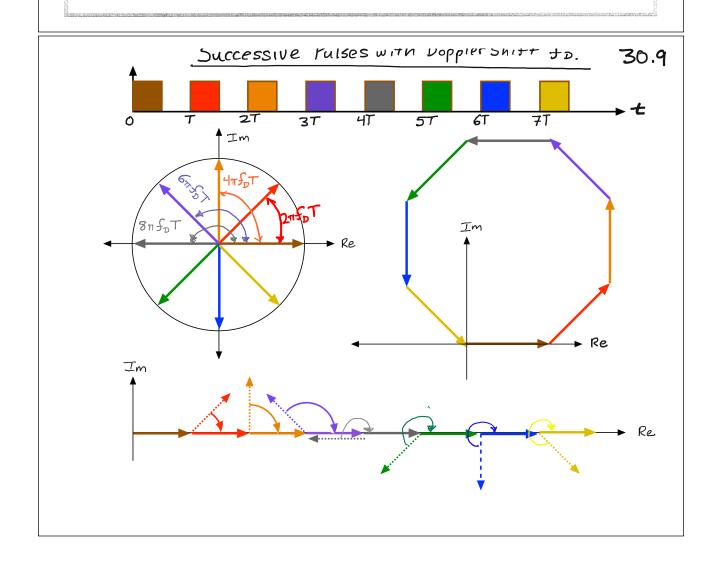
n.b where we pick to determines the told where we pick to determines the delay to first pulse return.)

We could calculate the DFT of the sequence U_n :

$$U_{k} = \sum_{n=0}^{N-1} u_{n} e^{-i\frac{2\pi nk}{N}}, k = 0, 1, ..., N-1.$$

Here again, we would get a large magnitude when $\frac{k}{N} = Tf_D$:

$$U_{k} = \begin{cases} N \cdot e^{i2\pi f_{p} t_{o}}, & k = NTf_{p} \\ 0, & \text{elsewhere.} \end{cases}$$



So for ease of implementation, the DFT (computed using an FFT algorithm) is commonly used to determine the Doppler of a target located at delay to corresponding to the initial sampling time to.

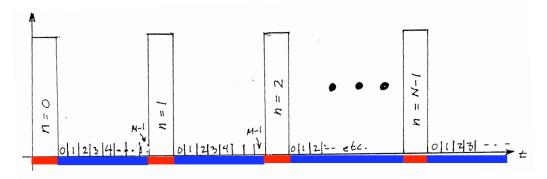
This is the beginning (and main idea) on which we build the delay-Doppler processor.

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The Pulse Waveform Delay-Doppler Processor

In general, we are interested in looking at the returns from all possible ranges (delays).

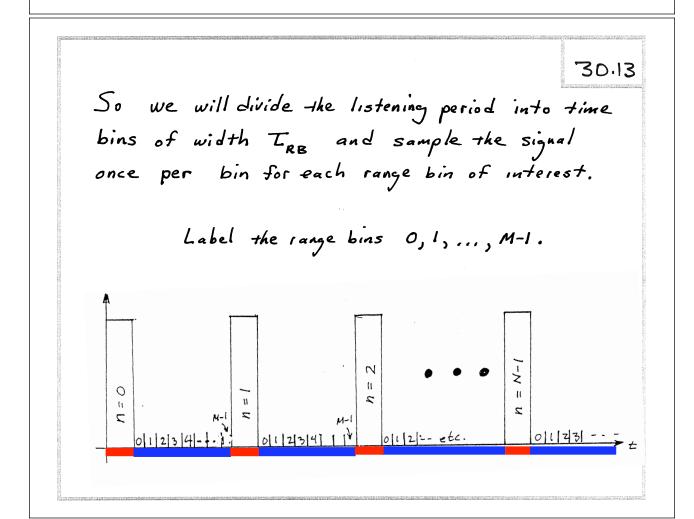
The situation appears as follows:



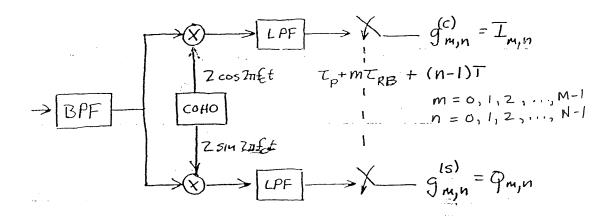
Because we transmit finite-bandwidth signals, we only have limited range or delay resolution.

Recall what $\beta_s(\tau, \nu)$ looks like.

So we will divide the listening period into bins of duration τ_{RB} .



We can get the sample returns from each of the range bins (both I and Q components to represent the complex baseband signal) by processing the received signal as follows:



n.b., τ_p is the transmitted pulse duration.

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Once we have carried out this procedure, we can think of the I and Q samples $\{I_{m,n}, Q_{m,n}\}$ as being arranged in an array as follows:

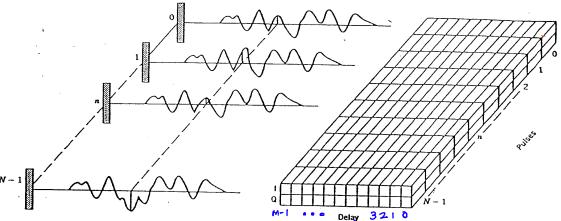


Figure 10.3 A conceptual diagram of the accumulation of 1 & Q samples at various delays, from N consecutive pulses.

(From: N. Levanon, Radar Principles, Wiley, 1987)

