

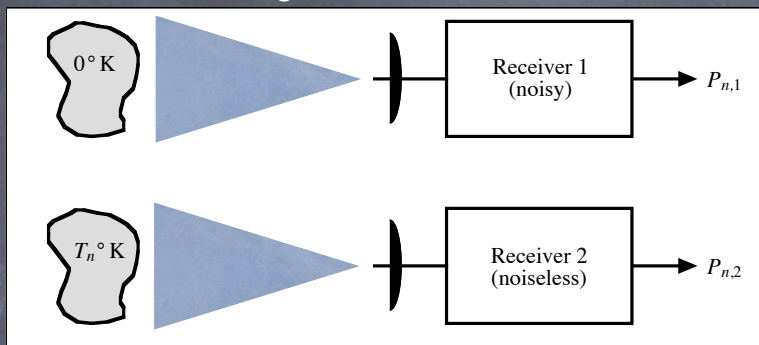
Session 10

Recall ...

Noise Temperature

10.1

(Characterizing Microwave System Noise)



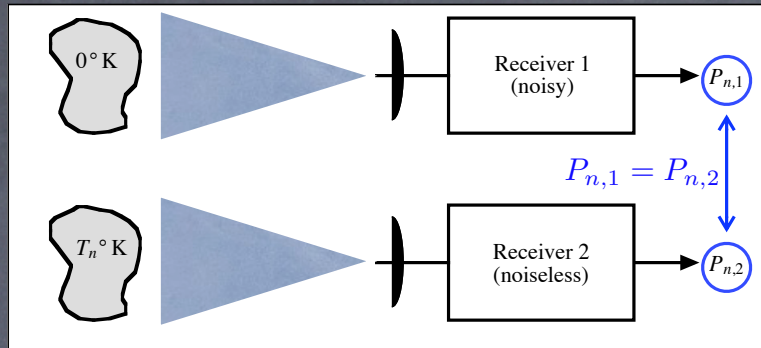
Receiver 1 is an *actual* noisy receiver. Its antenna pointed at a black body of temperature $T = 0^\circ\text{K}$.

Receiver 2 is a *hypothetical* noiseless receiver. Its antenna is pointing at a black body of temperature T_n .

Assume we can adjust T_n in second scenario until

$$P_{n,1} = P_{n,2}$$

We call the T_n achieving this the noise temperature of Receiver 1.



- When we quote a noise temperature for a real receiver, we are referring internal receiver noise to a hypothetical external noise source.
- This is a convenient accounting trick, as it allows us to look at all noise contributions at the same location—the input to the *receiver*.

Noise Figure or Noise Factor

The noise figure or noise factor NF of a receiver is

$$\text{NF} = \frac{T_n}{290^\circ \text{ K}} + 1$$

It is often expressed in dB:

$$\text{NF}_{\text{dB}} = 10 \log_{10} \left(\frac{T_n}{290 \text{ K}} + 1 \right) \quad (\text{dB})$$

Typical Noise Figures

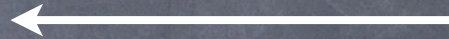
- ⑥ Noise figures for typical microwave receivers used in satellite communications are in the range of 2–5 (3–7 dB).
- ⑥ Radar systems are typically higher, because they are clutter—not thermal noise—limited.
- ⑥ NASA DSN Stations have an overall system noise temperature of about 20°K. $NF=1.069$

Big Antennas, "Cool" Receivers

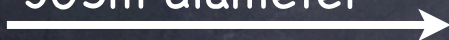
70-Meter Antenna
Goldstone Deep Space Communications Complex
Goldstone, California, U.S.A.



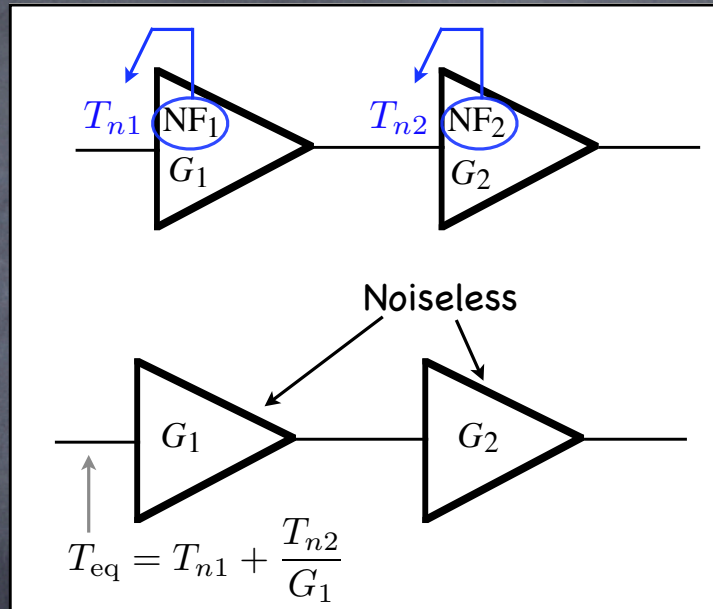
NASA DSN Antenna
70m diameter



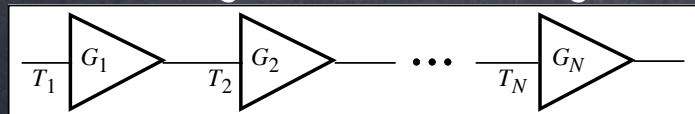
Arecibo (PR) Radio/Radar
Telescope Antenna
305m diameter



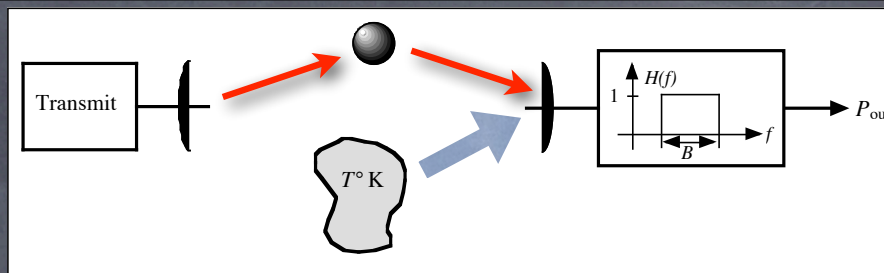
Noise Temperature/Figure of a Cascade 10.6



This can be generalized to N stages...



©2004 by Mark R. Bell, mrb@ecn.purdue.edu



10.7

We transmit a pulse of bandwidth B at frequency f_0 .

The received signal power is

$$P_r = \frac{P_t A^2 \sigma}{4\pi \lambda^2 R^4} \quad (\text{Radar Equation})$$

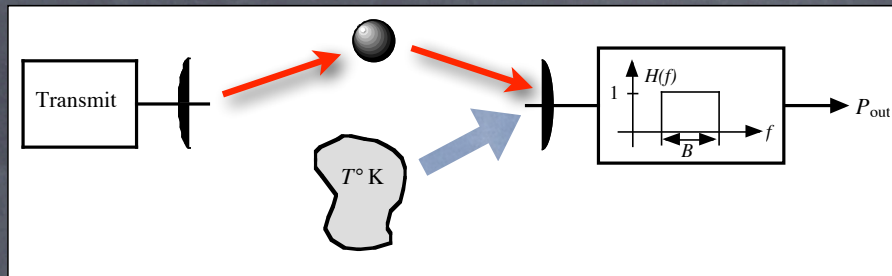
Assume ideal bandpass filter $H(f)$ does not effect the signal

(*n.b.* We must carefully interpret P_t and P_r :
 “Peak Power”, “Average Power”?—more on this later.)

The received noise power is

$$P_n = kT_e B$$

©2004 by Mark R. Bell, mrb@ecn.purdue.edu



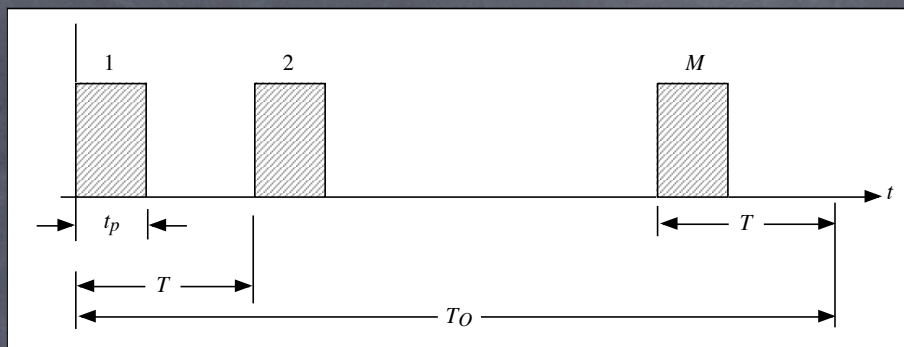
The signal-to-noise ratio is

$$\text{SNR} = \frac{P_r}{P_n} = \frac{P_t A^2 \sigma}{4\pi \lambda^2 R^4 k T_e B} \quad \leftarrow \text{Effective Aperture}$$

$$= \frac{P_t \lambda^2 G^2 \sigma}{(4\pi)^3 R^4 k T_e B} \quad \leftarrow \text{Antenna Gain}$$

We can think of this as the SNR for a single pulse when the pulse is "on", but many radars transmit a sequence of pulses.

©2004 by Mark R. Bell, mrb@ecn.purdue.edu



t_p = Pulse Width

T = Pulse Period (PRI ~ Pulse Repetition Interval)

T_O = Observation Time = MT

Similarly, we can define bandwidths/frequencies

$B = 1/t_p$ = Pulse Bandwidth (unmodulated)

$f_R = 1/T$ = Pulse Repetition Frequency (PRF)

$\Delta B_{\text{Dop}} = 1/T_O$ = Doppler Resolution of Radar

©2004 by Mark R. Bell, mrb@ecn.purdue.edu

If the source is not transmitting all of the time, we must be careful to note whether we are talking about Peak Power or Average Power.

P_T

P_{AVE}

If P_T is the peak power (power when transmitter is on)

$$P_{ave} = \frac{P_T t_p}{T}$$

If a coherent detector and matched filter are used to process returns, the voltage received from each pulse adds coherently:

Signal power increases as M^2

Noise power increases as M

Thus we have

$$\text{SNR}_M = M \cdot \text{SNR}_1 = \frac{M P_T A^2 \sigma}{4\pi \lambda^2 R^4 k T_e B}$$

Because P_T is the peak power when the transmitter is “on” and the signal bandwidth $B \approx 1/t_p$, we have

$$\begin{aligned} \text{SNR}_M &= \frac{M P_{ave} \frac{T}{t_p} A^2 \sigma}{4\pi \lambda^2 R^4 k T_e B} = \frac{P_{ave} \frac{B}{\Delta B_{Dop}} A^2 \sigma}{4\pi \lambda^2 R^4 k T_e B} \\ &= \frac{P_{ave} A^2 \sigma}{4\pi \lambda^2 R^4 k T_e \Delta B_{Dop}} \end{aligned}$$

Typically, $\Delta B_{Dop} \ll B$ and it can be that $P_{ave} \ll P_T$.

So, “who wins?”

$$\text{SNR}_M = \frac{P_{\text{ave}} A^2 \sigma}{4\pi \lambda^2 R^4 k T_e \Delta B_{Dop}}$$

Typically P_{ave} is constant.

Bounded from above
by hardware limitations

Noise bandwidth varies as $1/M$

Thus, SNR_M is proportional to M .

ΔB_{Dop} becomes the effective noise bandwidth.
(We will see this later.)