

DESIGN AND CONTROL OF FORMATIONS NEAR THE LIBRATION POINTS OF THE SUN-EARTH/MOON EPHEMERIS SYSTEM

K.C. Howell and B.G. Marchand Purdue University





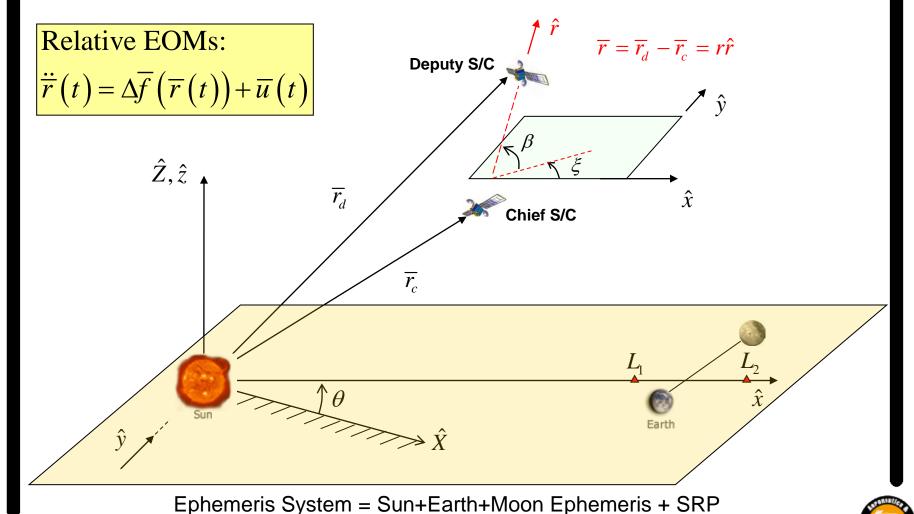
Reference Motions

- Natural Formations
 - String of Pearls
 - Others: Identify via Floquet controller (CR3BP)
 - Quasi-Periodic Relative Orbits (2D-Torus)
 - Nearly Periodic Relative Orbits
 - Slowly Expanding Nearly Vertical Orbits
- + Stable Manifolds

- Non-Natural Formations
 - Fixed Relative Distance and Orientation { RLP | Inertial
 - Fixed Relative Distance, Free Orientation
 - Fixed Relative Distance & Rotation Rate
 - Aspherical Configurations (Position & Rates)



2-S/C Formation Model in the Sun-Earth-Moon System



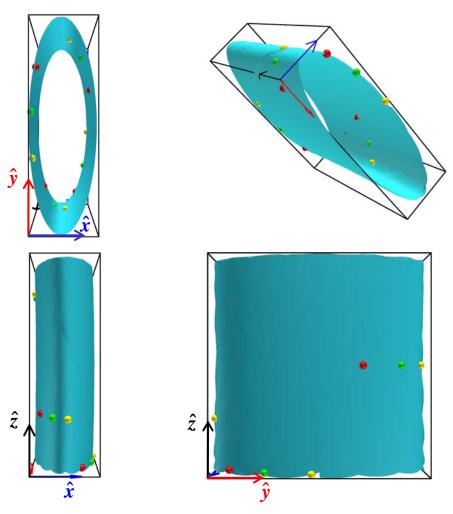


Natural Formations



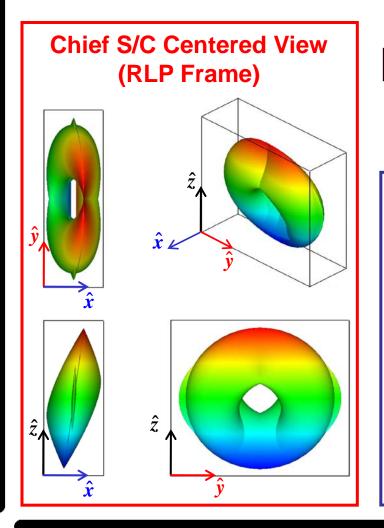


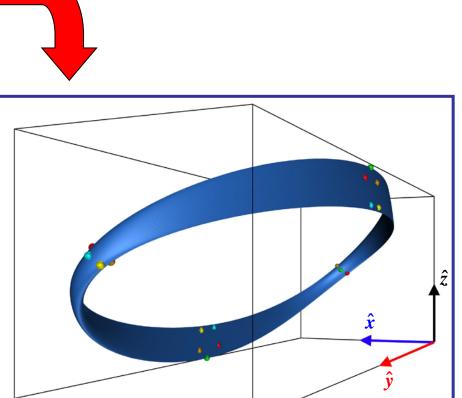
Natural Formations: String of Pearls





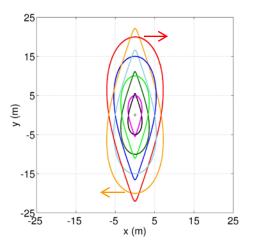
Natural Formations: Quasi-Periodic Relative Orbits → 2-D Torus



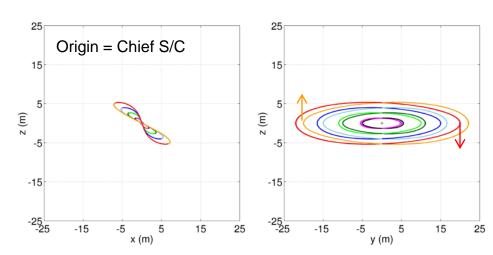




Natural Formations: Nearly Periodic Relative Motion



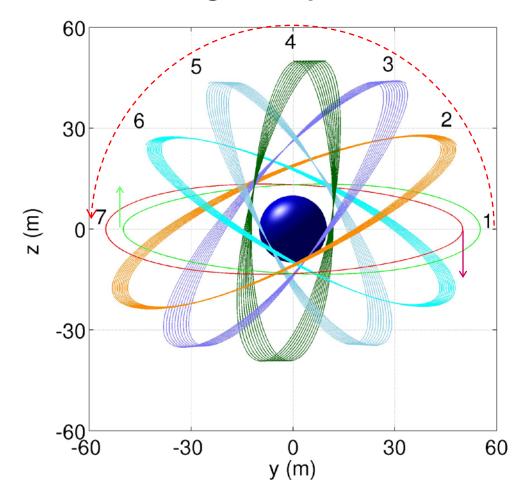
10 Revolutions = 1,800 days







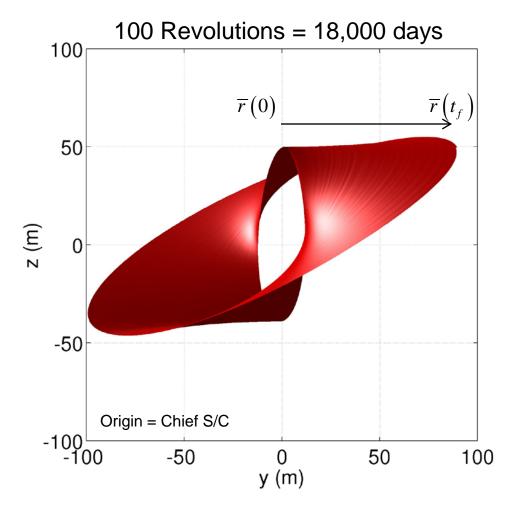
Evolution of Nearly Vertical Orbits Along the *yz*-Plane







Natural Formations: Slowly Expanding Vertical Orbits





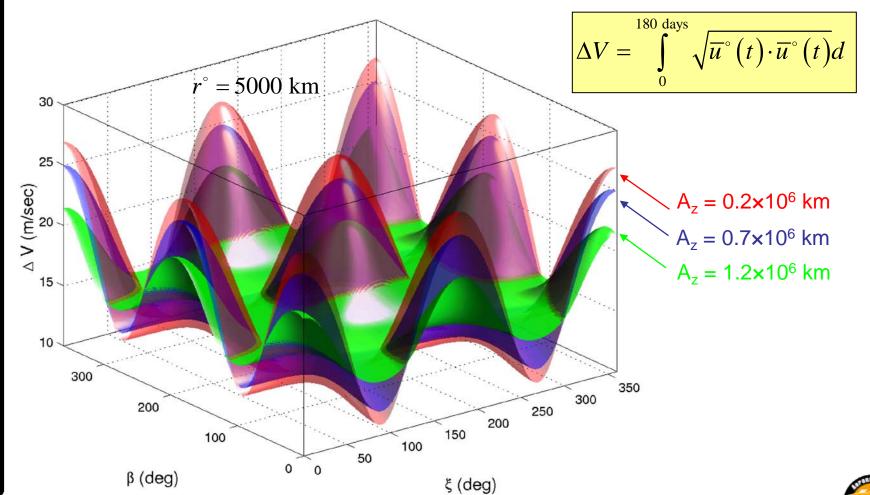


Non-Natural Formations



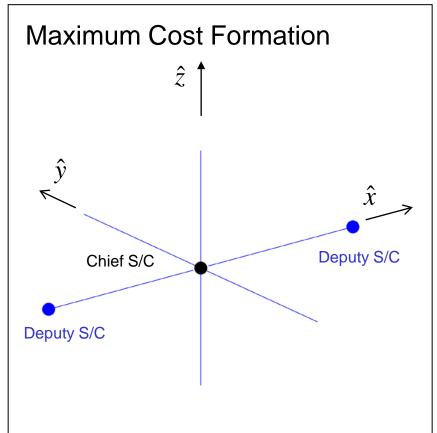


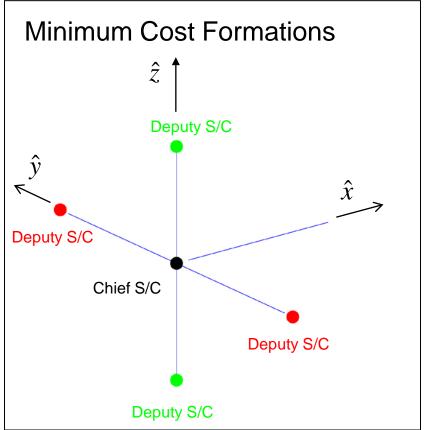
Nominal Formation Keeping Cost (Configurations Fixed in the RLP Frame)



PURDUE

Max./Min. Cost Formations (Configurations Fixed in the RLP Frame)



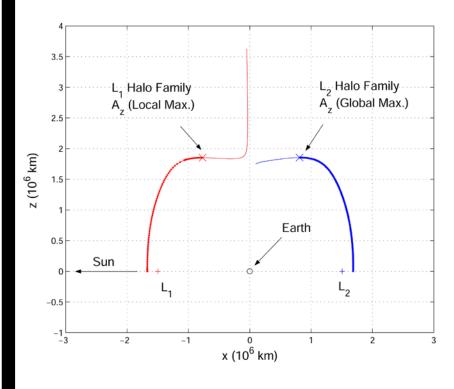


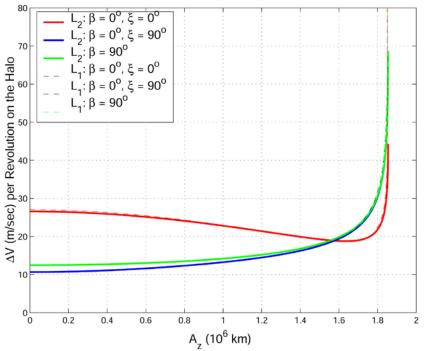
Nominal Relative Dynamics in the Synodic Rotating Frame





Formation Keeping Cost Variation Along the SEM L₁ and L₂ Halo Families (Configurations Fixed in the RLP Frame)







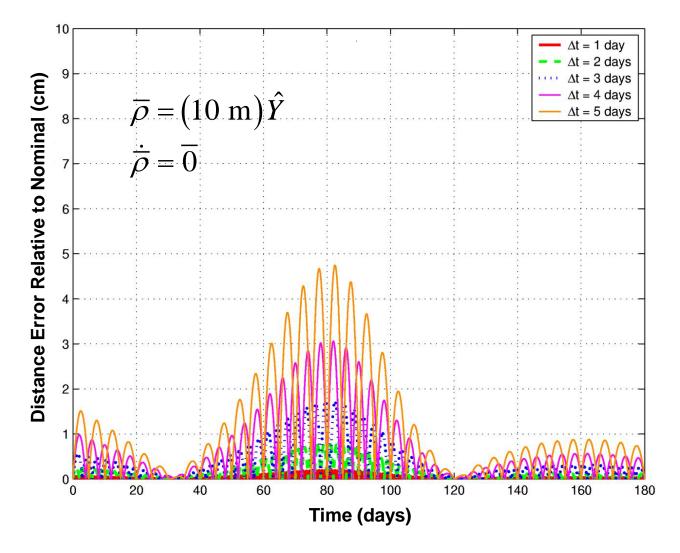


Discrete vs. Continuous Control





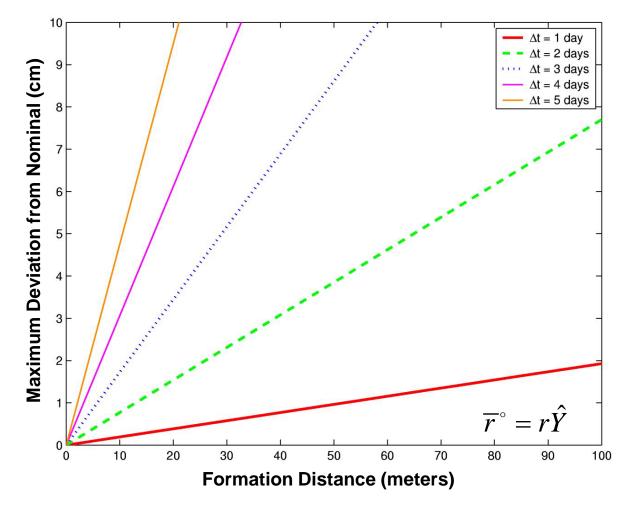
Discrete Control: Linear Targeter







Achievable Accuracy via Targeter Scheme





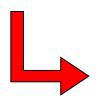


Continuous Control: LQR vs. Input Feedback Linearization

LQR for <u>Time-Varying</u> Nominal Motions

$$\dot{\overline{x}}(t) = \left[\dot{\overline{r}} \quad \ddot{\overline{r}}\right]^{T} = \overline{f}(t, \overline{x}(t), \overline{u}(t)) \qquad \to \overline{x}(0) = \overline{x}_{0}$$

$$\dot{P} = -A^{T}(t)P(t) - P(t)A(t) + P(t)B(t)R^{-1}B^{T}(t)P(t) - Q \to P(t_{f}) = 0$$



Optimal Control Law:

Nominal Control Input
$$\overline{u}(t) = \overline{u}^{\circ}(t) + \left\{ -R^{-1}B^{T}P(t)(\overline{x}(t) - \overline{x}^{\circ}(t)) \right\}$$
Optimal Control, Relative to Nominal, from LQR

Input Feedback Linearization (IFL)

$$\ddot{\overline{r}}(t) = \overline{F}(\overline{r}(t)) + \overline{u}(t)$$

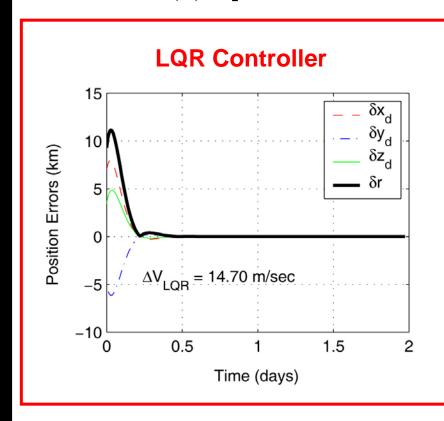


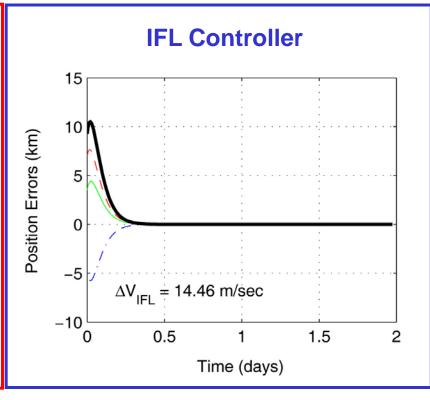


Dynamic Response to Injection Error

$$\rho = 5000 \text{ km}, \ \xi = 90^{\circ}, \ \beta = 0^{\circ}$$

$$\delta \overline{x}(0) = \begin{bmatrix} 7 \text{ km} & -5 \text{ km} & 3.5 \text{ km} & 1 \text{ mps} & -1 \text{ mps} \end{bmatrix}^T$$





Dynamic Response Modeled in the CR3BP Nominal State Fixed in the Rotating Frame





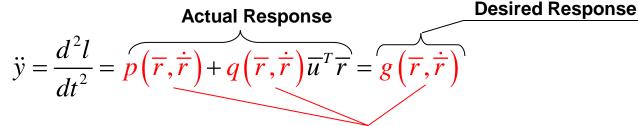
Output Feedback Linearization (Radial Distance Control)

Formation Dynamics

$$\ddot{r} = \Delta \overline{f}(\overline{r}) + \overline{u}(t) \longrightarrow \text{Generalized Relative EOMs}$$

$$y = l(\overline{r}) \longrightarrow \text{Measured Output}$$

Measured Output Response (Radial Distance)



Scalar Nonlinear Functions of \overline{r} and $\dot{\overline{r}}$

Scalar Nonlinear Constraint on Control Inputs

$$h(\overline{r}(t), \dot{\overline{r}}(t)) - \overline{u}(t)^{T} \overline{r}(t) = 0$$





Output Feedback Linearization (OFL)

(Radial Distance Control in the Ephemeris Model)

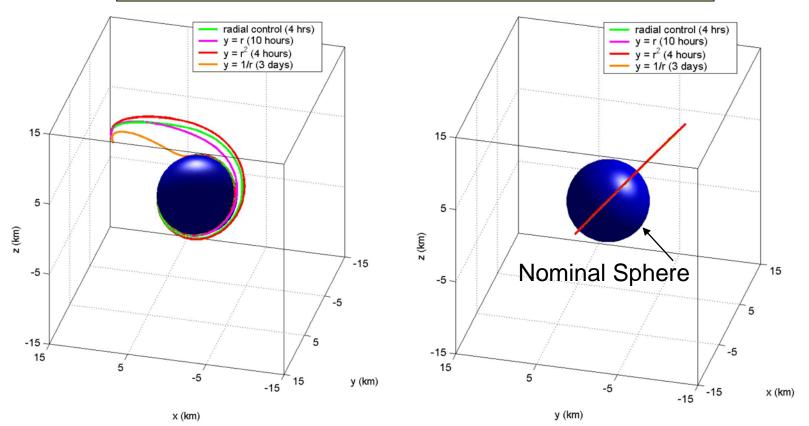
$y = l\left(\overline{r}, \dot{\overline{r}}\right)$	Control Law
r	$\overline{u}(t) = \frac{h(\overline{r}, \dot{\overline{r}})}{r} \hat{r}$ Geometric Approach: Radial inputs only
r	$\overline{u}(t) = \left\{ \frac{g(\overline{r}, \dot{\overline{r}})}{r} - \frac{\dot{\overline{r}}^T \dot{\overline{r}}}{r^2} \right\} \overline{r} + \left(\frac{\dot{r}}{r}\right) \dot{\overline{r}} - \Delta \overline{f}(\overline{r})$
r^2	$\overline{u}(t) = \left\{ \frac{1}{2} \frac{g(\overline{r}, \dot{\overline{r}})}{r^2} - \frac{\dot{\overline{r}}^T \dot{\overline{r}}}{r^2} \right\} \overline{r} - \Delta \overline{f}(\overline{r})$
1/r	$\overline{u}(t) = \left\{ -rg(\overline{r}, \dot{\overline{r}}) - \frac{\dot{\overline{r}}^T \dot{\overline{r}}}{r^2} \right\} \overline{r} + 3\left(\frac{\dot{r}}{r}\right) \dot{\overline{r}} - \Delta \overline{f}(\overline{r})$

- Critically damped output response achieved in all cases
- Total ΔV can vary significantly for these four controllers



OFL Control of Spherical Formations in the Ephemeris Model

$$\overline{r}(0) = \begin{bmatrix} 12 & -5 & 3 \end{bmatrix}$$
 km $\dot{\overline{r}}(0) = \begin{bmatrix} 1 & -1 & 1 \end{bmatrix}$ m/sec



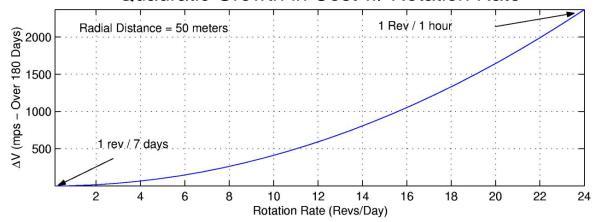
Relative Dynamics as Observed in the Inertial Frame



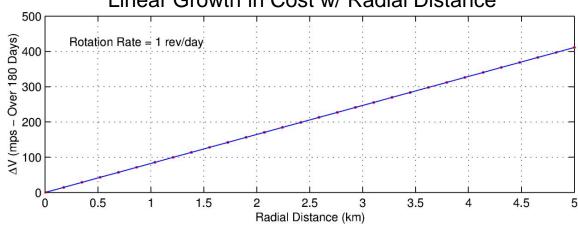


OFL Control of Spherical Formations Radial Dist. + Rotation Rate





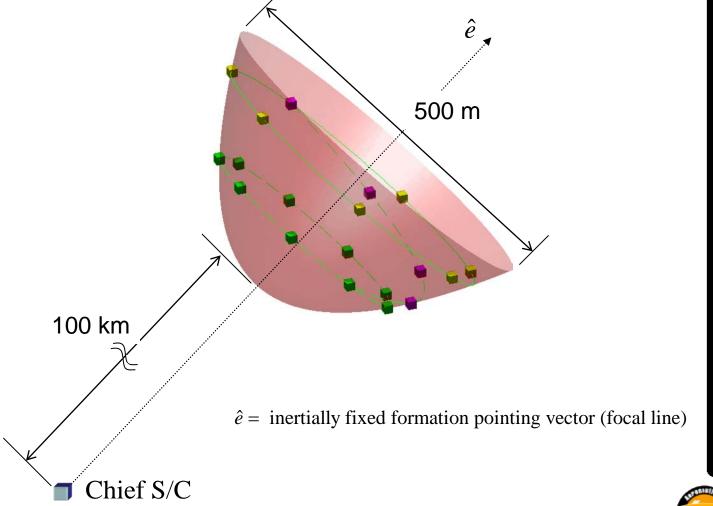
Linear Growth in Cost w/ Radial Distance







Inertially Fixed Formations in the Ephemeris Model





Conclusions

- Continuous Control in the Ephemeris Model:
 - Non-Natural Formations
 - LQR/IFL → essentially identical responses & control inputs
 - IFL appears to have some advantages over LQR in this case
 - OFL → spherical configurations + unnatural rates
 - Low acceleration levels → Implementation Issues
- Discrete Control of Non-Natural Formations
 - Targeter Approach
 - Small relative separations → Good accuracy
 - Large relative separations → Require nearly continuous control
 - Extremely Small ΔV's (10⁻⁵ m/sec)
- Natural Formations
 - Nearly periodic & quasi-periodic formations in the RLP frame
 - Floquet controller: numerically ID solutions + stable manifolds



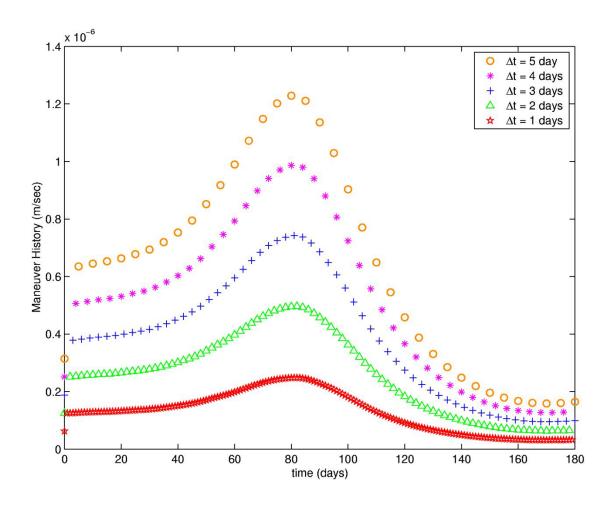


Backups





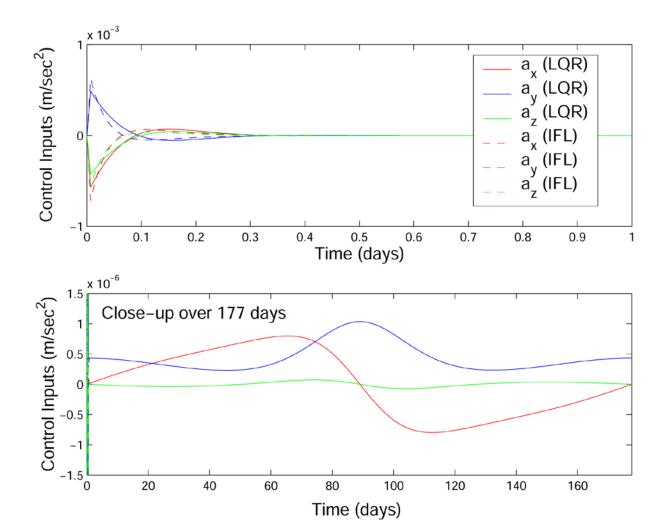
Targeter Maneuver Schedule







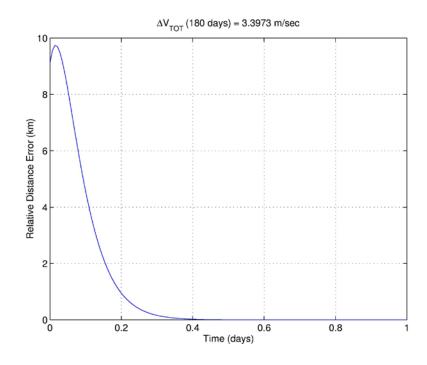
LQR vs. IFL (CR3BP) Control Accelerations

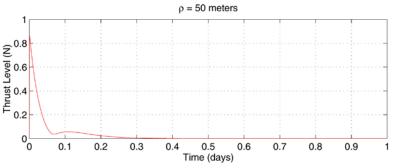


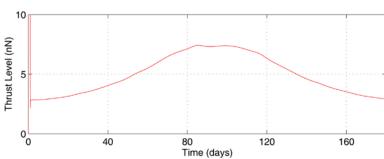




IFL Response in the Ephemeris Model



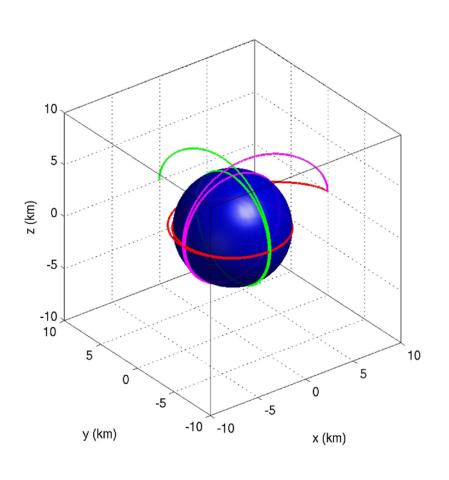


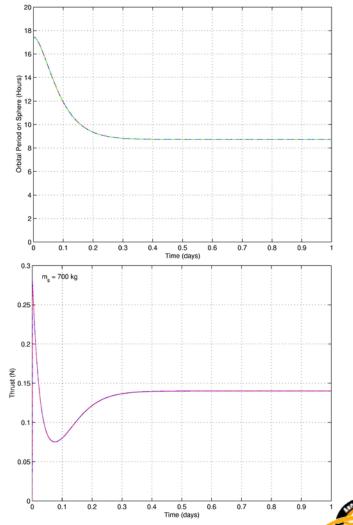






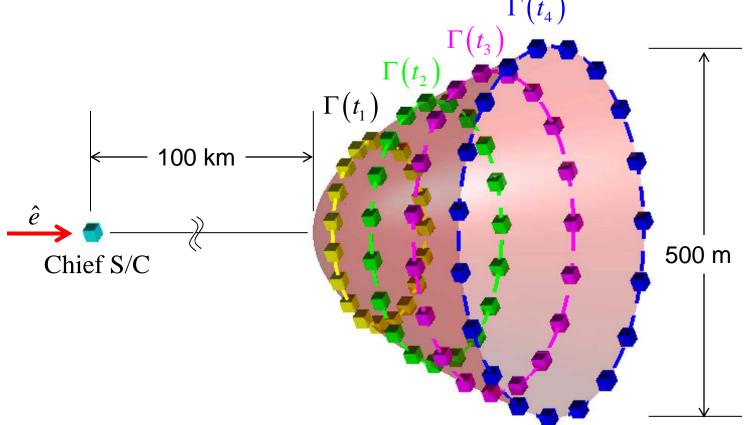
OFL Control in the Ephemeris Model







Inertially Fixed Formations in the Ephemeris Model



 $\Gamma(t_j)$ = Nominal configuration of deputies (20 s/c) at time t_j

 \hat{e} = inertially fixed formation pointing vector (focal line)



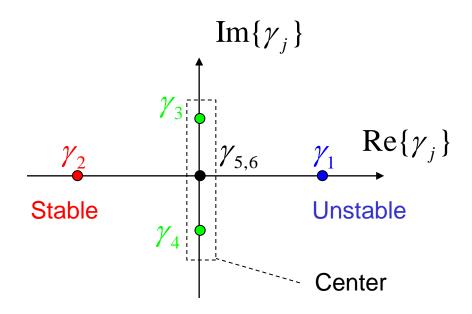


Stability of *T*-Periodic Orbits

Linear Variational Equation:

$$\delta \overline{x}(t) = \Phi(t,0) \delta \overline{x}(0)$$

 $\delta \overline{x}(t) \rightarrow$ measured relative to periodic orbit

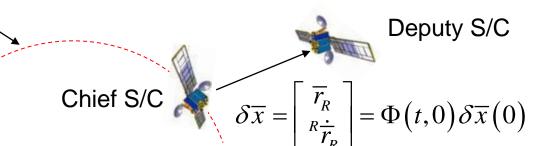






Eigenstructure Near Halo Orbit

Reference Halo Orbit



Floquet Decomposition of $\Phi(t,0)$:

$$\Phi(t,0) = \left\{ P(t)S \right\} e^{Jt} \left\{ P(0)S \right\}^{-1}$$

Floquet Modal Matrix:

$$E(t) = P(t)S = \Phi(t,0)E(0)e^{-Jt}$$

Solution to Variational Eqn. in terms of Floquet Modes:

$$\delta \overline{x}(t) = \sum_{j=1}^{6} \delta \overline{x}_{j}(t) = \sum_{j=1}^{6} c_{j}(t) \overline{e}_{j}(t) = E(t) \overline{c}$$





Floquet Controller

(Remove Unstable + 2 Center Modes)

Find $\Delta \overline{v}$ that removes undesired response modes:

$$\sum_{j=1}^{6} \delta \overline{x}_{j} + \begin{bmatrix} 0_{3} \\ I_{3} \end{bmatrix} \Delta \overline{v} = \sum_{\substack{j=2,3,4 \\ \text{or} \\ j=2,5,6}} (1 + \alpha_{j}) \delta \overline{x}_{j}$$

Remove Modes 1, 3, and 4:

$$\begin{bmatrix} \overline{\alpha} \\ \Delta \overline{v} \end{bmatrix} = \begin{bmatrix} \delta \overline{x}_{2\overline{r}} & \delta \overline{x}_{5\overline{r}} & \delta \overline{x}_{6\overline{r}} & 0_{3} \\ \delta \overline{x}_{2\overline{v}} & \delta \overline{x}_{5\overline{v}} & \delta \overline{x}_{6\overline{v}} & -I_{3} \end{bmatrix}^{-1} \left(\delta \overline{x}_{1} + \delta \overline{x}_{3} + \delta \overline{x}_{4} \right)$$

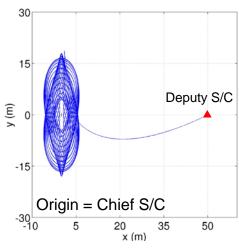
Remove Modes 1, 5, and 6:

$$\begin{bmatrix} \overline{\alpha} \\ \Delta \overline{v} \end{bmatrix} = \begin{bmatrix} \delta \overline{x}_{2\overline{r}} & \delta \overline{x}_{3\overline{r}} & \delta \overline{x}_{4\overline{r}} & 0_{3} \\ \delta \overline{x}_{2\overline{v}} & \delta \overline{x}_{3\overline{v}} & \delta \overline{x}_{4\overline{v}} & -I_{3} \end{bmatrix}^{-1} \left(\delta \overline{x}_{1} + \delta \overline{x}_{5} + \delta \overline{x}_{6} \right)$$

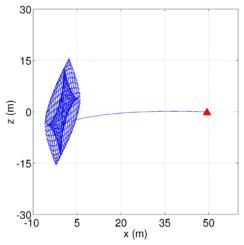


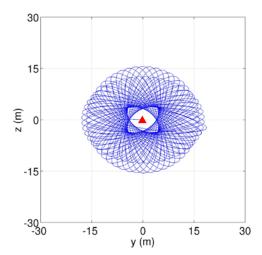


Deployment into Torus (Remove Modes 1, 5, and 6)



$$\overline{r}(0) = \begin{bmatrix} 5 & 00 & 0 \end{bmatrix}$$
 m
 $\dot{\overline{r}}(0) = \begin{bmatrix} 1 & -1 & 1 \end{bmatrix}$ m/sec

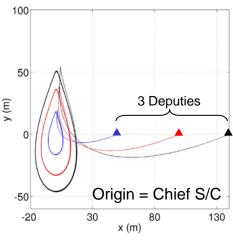






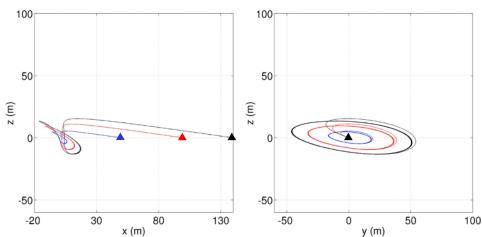


Deployment into Natural Orbits (Remove Modes 1, 3, and 4)



$$\overline{r}(0) = \begin{bmatrix} r_0 & 0 & 0 \end{bmatrix} \text{ m}$$

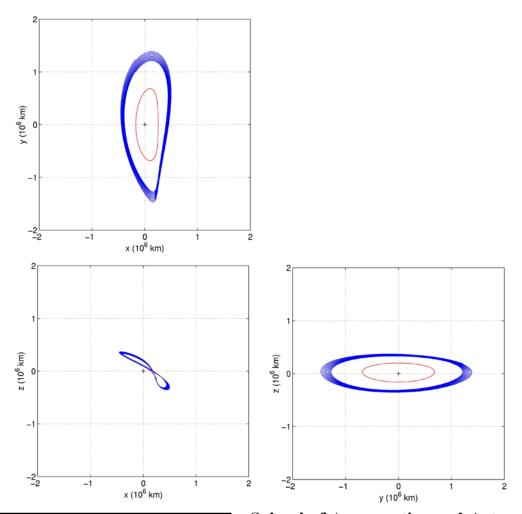
$$\dot{\overline{r}}(0) = \begin{bmatrix} 1 & -1 & 1 \end{bmatrix} \text{ m/sec}$$







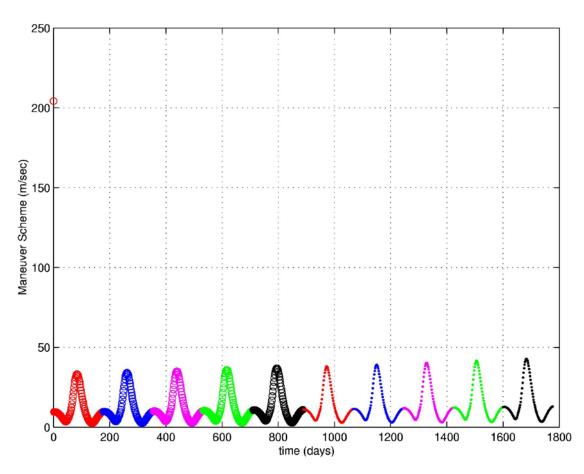
Floquet Control (Large Formations – Example 1)







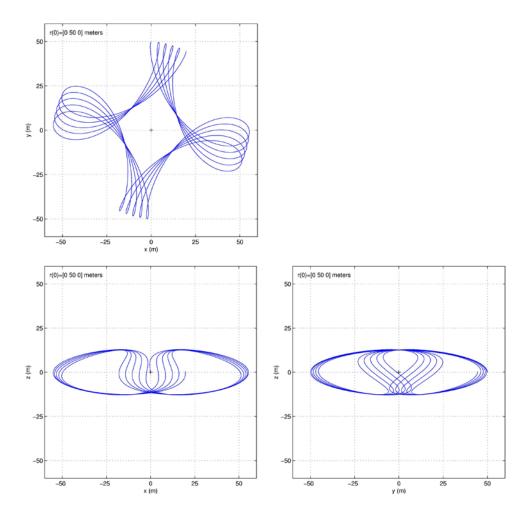
Floquet Controller Maneuver Schedule (For Example 1)







Nearly Periodic Formations (Inertial Perspective)







Nearly Vertical Formations (Inertial Perspective)

