

ECE 5314: Power System Operation & Control

Lecture 8: Network-constrained Economic Dispatch

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- R2 A. Gomez-Exposito, A. J. Conejo, C. Canizares, *Electric Energy Systems: Analysis and Operation*, Chapters 6.4 & 6.6.
- R1 A. J. Wood, B. F. Wollenberg, and G. B. Sheble, *Power Generation, Operation, and Control*, Wiley, 2014, Chapter 8.
- R4 J. Taylor, *Convex Optimization of Power Systems*, Cambridge University Press, 2015, Chapter 3.

Transmission congestion example

G1: 0-500 MW @ 5\$/MWh; **G2:** 0-500 MW @ 6 \$/MWh; **Load:** 400 MW

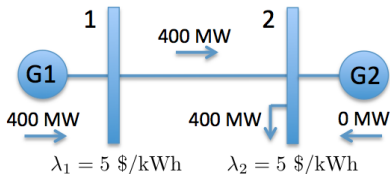


Figure: Transmission line with unlimited capacity

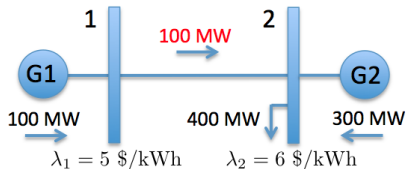
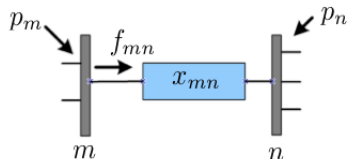


Figure: Line power flow limited to 100 MW in both directions (overheating, sagging)

Flows in DC model

- Grid with N buses and L lines $\mathcal{G} = (\mathcal{B}, \mathcal{L})$
- According to DC power flow model

$$f_\ell = f_{(m,n)} = \frac{\theta_m - \theta_n}{x_{mn}} \text{ for } \ell \in \mathcal{L}$$



- Collect all line flows in $\mathbf{f} = \mathbf{X}^{-1} \mathbf{A} \boldsymbol{\theta} \in \mathbb{R}^L$
- Diagonal matrix with reactances $\mathbf{X} = \text{diag}(\{x_{mn}\})$
- **Branch-bus incidence matrix:** captures network connectivity ($\mathbf{A} \mathbf{1} = \mathbf{0}$)

$$\mathbf{A} = \begin{bmatrix} \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ 0 & \cdots & +1 & \cdots & -1 & \cdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \end{bmatrix} \leftarrow \text{line } (m, n) \right._{L \times N}$$

source bus m dest. bus n
 ↓ ↓

Injections in DC model

- Conservation of power (lossless network)

$$p_m = \sum_{\ell:(m,n)} f_\ell - \sum_{\ell:(n,m)} f_\ell$$

- Collect active power injections in

$$\mathbf{p} = \mathbf{A}^\top \mathbf{f} = \mathbf{B}\boldsymbol{\theta}$$

where $\mathbf{B} = \mathbf{A}^\top \mathbf{X}^{-1} \mathbf{A}$ from DC power flow [recall $\mathbf{B} \succeq \mathbf{0}$ and $\mathbf{B}\mathbf{1} = \mathbf{0}$]

- **Reduced bus reactance matrix:** $\mathbf{B}_r \in \mathbb{S}_{++}^{N-1}$ invertible for connected grids

$$\mathbf{B} = \begin{bmatrix} B_{11} & \mathbf{b}_1^\top \\ \mathbf{b}_1 & \mathbf{B}_r \end{bmatrix}$$

- **Reduced branch-bus incidence matrix:**

$$\mathbf{A} = [\mathbf{a}_1 \ \mathbf{A}_r] \quad \text{with} \quad \mathbf{B}_r = \mathbf{A}_r^\top \mathbf{X}^{-1} \mathbf{A}_r$$

Network-constrained economic dispatch or DC-OPF

Minimize generation cost subject to

$$\min_{\boldsymbol{\theta}, \mathbf{p}} \sum_{m=1}^N C_m(p_m) \quad (\text{P1})$$

$$\text{s.to } \underline{\mathbf{p}} \leq \mathbf{p} \leq \bar{\mathbf{p}} \quad (\text{P1a})$$

$$\mathbf{p} = \mathbf{B}\boldsymbol{\theta} \quad (\text{P1b})$$

$$-\bar{\mathbf{f}} \leq \mathbf{X}^{-1}\mathbf{A}\boldsymbol{\theta} \leq \bar{\mathbf{f}} \quad (\text{P1c})$$

- (P1a): generation constraints; it captures (in)elastic loads too
- (P1b): physical model (approx. DC power flow model)
 $\boldsymbol{\theta}$ in radians and \mathbf{B} in pu
- (P1c): limits on line power flows [why two-sided?]
line overheating; limits $\bar{\mathbf{f}}$ depend on weather conditions

Eliminating voltage angles

- Focus on constraints:
$$\mathbf{p} = \mathbf{B}\boldsymbol{\theta} \quad (\text{P1b})$$
$$-\bar{\mathbf{f}} \leq \mathbf{X}^{-1}\mathbf{A}\boldsymbol{\theta} \leq \bar{\mathbf{f}} \quad (\text{P1c})$$

- Eliminate bus voltage angles by setting $\theta_1 = 0$ in (P1b)

$$\mathbf{p} = \begin{bmatrix} p_1 \\ \mathbf{p}_r \end{bmatrix} = \begin{bmatrix} B_{11} & \mathbf{b}_1^\top \\ \mathbf{b}_1 & \mathbf{B}_r \end{bmatrix} \begin{bmatrix} \theta_1 \\ \boldsymbol{\theta}_r \end{bmatrix} = \begin{bmatrix} \mathbf{b}_1^\top \boldsymbol{\theta}_r \\ \mathbf{B}_r \boldsymbol{\theta}_r \end{bmatrix}$$

- Constraint (P1b) equivalent to $\mathbf{1}^\top \mathbf{p} = 0$ and $\boldsymbol{\theta}_r = \mathbf{B}_r^{-1} \mathbf{p}_r$
- Flow vector in (P1c) can be expressed as $\mathbf{f} = \mathbf{X}^{-1} \mathbf{A} \boldsymbol{\theta} = \mathbf{S} \mathbf{p}$
- Power-transfer distribution factor (PTDF) matrix:**

$$\mathbf{S} := [\mathbf{0} \quad \mathbf{X}^{-1} \mathbf{A}_r \mathbf{B}_r^{-1}]_{L \times N}$$

DC-OPF simplified

$$\min_{\mathbf{p}} \sum_{m=1}^N C_m(p_m) \quad (\text{P2})$$

$$\text{s.to } \underline{\mathbf{p}} \leq \mathbf{p} \leq \bar{\mathbf{p}} \quad (\text{kept implicit}) \quad (\text{P2a})$$

$$\mathbf{1}^\top \mathbf{p} = 0 \quad \leftarrow \lambda \quad (\text{P2b})$$

$$-\bar{\mathbf{f}} \leq \mathbf{S}\mathbf{p} \leq \bar{\mathbf{f}} \quad \leftarrow (\underline{\boldsymbol{\mu}}, \bar{\boldsymbol{\mu}}) \quad (\text{P2c})$$

How to solve this problem?

$$\text{Lagrangian fun.: } L = \sum_{m=1}^N C_m(p_m) - \lambda \mathbf{1}^\top \mathbf{p} + \underline{\boldsymbol{\mu}}^\top (-\bar{\mathbf{f}} - \mathbf{S}\mathbf{p}) + \bar{\boldsymbol{\mu}}^\top (\mathbf{S}\mathbf{p} - \bar{\mathbf{f}})$$

After re-arranging:

$$L = \sum_{m=1}^N C_m(p_m) - \left[\lambda \mathbf{1} - \mathbf{S}^\top (\bar{\boldsymbol{\mu}} - \underline{\boldsymbol{\mu}}) \right]^\top \mathbf{p} - (\bar{\boldsymbol{\mu}} + \underline{\boldsymbol{\mu}})^\top \bar{\mathbf{f}}$$

Optimality conditions

1. Primal feasibility: \mathbf{p}^* satisfies (P2b) and (P2c)
2. Dual feasibility: $\bar{\boldsymbol{\mu}}^*, \underline{\boldsymbol{\mu}}^* \geq \mathbf{0}$
3. Lagrangian optimality:

$$\mathbf{p}^* \in \arg \min_{\underline{\mathbf{p}} \leq \mathbf{p} \leq \bar{\mathbf{p}}} \sum_{m=1}^N C_m(p_m) - \left[\lambda^* \mathbf{1} - \mathbf{S}^\top (\bar{\boldsymbol{\mu}}^* - \underline{\boldsymbol{\mu}}^*) \right]^\top \mathbf{p}$$

4. Complementary slackness: $(-\bar{\mathbf{f}} - \mathbf{S}\mathbf{p}^*) \odot \underline{\boldsymbol{\mu}}^* = \mathbf{0}$ and $(\mathbf{S}\mathbf{p}^* - \bar{\mathbf{f}}) \odot \bar{\boldsymbol{\mu}}^* = \mathbf{0}$

Economic interpretation: If $\boldsymbol{\pi} = \lambda^* \mathbf{1} - \mathbf{S}^\top (\bar{\boldsymbol{\mu}}^* - \underline{\boldsymbol{\mu}}^*) \in \mathbb{R}^N$ is used as a vector of prices, it maximizes the social welfare while adhering to network limits and power balance constraints!

$$p_m^* \in \arg \min_{\underline{p}_m \leq p_m \leq \bar{p}_m} C_m(p_m) - \pi_m p_m$$

Locational Marginal Prices (LMPs)

- **Locational marginal prices:** widely used in energy markets

$$\boldsymbol{\pi} := \lambda^* \mathbf{1} - \mathbf{S}^\top (\overline{\boldsymbol{\mu}}^* - \underline{\boldsymbol{\mu}}^*)$$

- vector $\boldsymbol{\pi}$ shown to be equal to the vector of Lagrange multipliers for (P1b)
- **perturbation interpretation:** π_m is the cost of supplying the next demand increment at location m
- market practice: location can be a bus or a cluster of buses
- price at the reference bus is $\pi_1 = \lambda^*$ [the first column of \mathbf{S} is zero]

LMP components

- **Locational marginal prices:** $\boldsymbol{\pi} := \lambda^* \mathbf{1} - \mathbf{S}^\top (\overline{\boldsymbol{\mu}}^* - \underline{\boldsymbol{\mu}}^*)$
- If **no congestion** (line flows strictly within limits)

$$\underline{\boldsymbol{\mu}}^* = \overline{\boldsymbol{\mu}}^* = \mathbf{0} \implies \boldsymbol{\pi} = \lambda^* \mathbf{1}$$

- **Marginal energy component (MEC):** $\lambda^* \mathbf{1}$
- **Marginal congestion component (MCC):** $-\mathbf{S}^\top (\overline{\boldsymbol{\mu}}^* - \underline{\boldsymbol{\mu}}^*)$
vector of **shadow prices** $(\overline{\boldsymbol{\mu}}^* - \underline{\boldsymbol{\mu}}^*) \in \mathbb{R}^L$

- **Marginal loss component (MLC):** LMPs are heuristically adjusted by MLC to account for losses; e.g., $\text{MLC} = \lambda^* \nabla_{\mathbf{p}} P_{\text{loss}}(\mathbf{p})$ (typically small)
- In practice, $\text{LMP} = \text{MEC} + \text{MCC} + \text{MLC}$

Reference and slack buses

- So far, reference and slack bus coincided; they don't have to
- *Reference bus* r : the bus for which we select $\theta_r = 0$
 - it determines which column of \mathbf{B} is dropped to form \mathbf{B}_r
- *Slack bus* s : the bus s for which we select $p_s = -\sum_{n \neq s} p_n$
 - it determines which row of \mathbf{B} is dropped to form \mathbf{B}_r
 - the s -th column of $\mathbf{S}_{s,r}$ is zero
- When changing reference and/or slack buses:
 - shadow prices $(\underline{\mu}, \underline{\mu})$ do not change
 - $\text{MEC} = \pi_s$ and $\text{MCC} = -\mathbf{S}_{s,r}^\top (\underline{\mu} - \underline{\mu})$ change
 - however, vector $\boldsymbol{\pi} = \text{MEC} + \text{MCC}$ remains the same!
 - MLC components change ...

Transmission congestion surplus

How much money does the ISO collect?

$$\begin{aligned} s &= -\boldsymbol{\pi}^\top \mathbf{p}^* \\ &= -\lambda^* \mathbf{1}^\top \mathbf{p}^* + (\bar{\boldsymbol{\mu}}^* - \underline{\boldsymbol{\mu}}^*)^\top \mathbf{S} \mathbf{p}^* \\ &= 0 + (\bar{\boldsymbol{\mu}}^* - \underline{\boldsymbol{\mu}}^*)^\top \mathbf{f}^* \end{aligned}$$

The optimal line flows $\mathbf{f}^* = \mathbf{S} \mathbf{p}^*$ satisfy:

$$(-\bar{\mathbf{f}} - \mathbf{f}^*)^\top \underline{\boldsymbol{\mu}}^* = 0 \quad \text{and} \quad (\mathbf{f}^* - \bar{\mathbf{f}})^\top \bar{\boldsymbol{\mu}}^* = 0$$

which yields a positive transmission congestion surplus

$$s = (\bar{\boldsymbol{\mu}}^* + \underline{\boldsymbol{\mu}}^*)^\top \bar{\mathbf{f}} \geq 0$$

Surplus is distributed via auctions of **financial transmission rights** (FTR)

AC optimal power flow (AC-OPF)

DC-OPF cannot handle constraints on reactive power and voltage magnitudes

$$\min_{\mathbf{p}, \mathbf{q}, \mathbf{v}} \sum_{m=1}^N C_m(p_m) \quad (\text{P3})$$

$$\text{s.to } \mathbf{p} + j\mathbf{q} = \text{diag}(\mathbf{v})(\mathbf{Y}\mathbf{v})^* \quad (\text{physical system}) \quad (\text{P3a})$$

$$|P_{mn}| \leq P_{mn}^{\max} \quad \text{and/or} \quad |S_{mn}| \leq S_{mn}^{\max} \quad (\text{P3b})$$

$$V_m^{\min} \leq |V_m| \leq V_m^{\max} \quad (\text{P3c})$$

$$\mathbf{p}_{\min} \leq \mathbf{p} \leq \mathbf{p}_{\max}; \quad \mathbf{q}_{\min} \leq \mathbf{q} \leq \mathbf{q}_{\max} \quad (\text{P3d})$$

- (P3): generation or any other meaningful cost
- (P3b): limits on line flows
- (P3c): limits on voltage magnitudes
- (P3d): generation and demand limits

Fundamental tool in power system operations

- eliminate variables (\mathbf{p}, \mathbf{q}) using (P3a)

$$\min_{\mathbf{v}} \sum_{m=1}^N C_m(\mathbf{v}) \quad (\text{P4})$$

$$\text{s.to } |P_{mn}(\mathbf{v})| \leq f_{mn}^{\max} \quad \text{and/or} \quad |S_{mn}(\mathbf{v})| \leq S_{mn}^{\max} \quad (\text{P4b})$$

$$V_m^{\min} \leq |V_m(\mathbf{v})| \leq V_m^{\max} \quad (\text{P4c})$$

$$\mathbf{p}_{\min} \leq \mathbf{p}(\mathbf{v}) \leq \mathbf{p}_{\max}; \quad \mathbf{q}_{\min} \leq \mathbf{q}(\mathbf{v}) \leq \mathbf{q}_{\max} \quad (\text{P4d})$$

- voltages \mathbf{v} in polar or rectangular coordinates
- comparison to power flow problem
- other variables: transformer tap ratios, phase shifters, shunt capacitors

Solving the OPF

- AC-OPF [Carpentier 1960] is a challenging problem (NP-hard)
- Several approaches have been developed:
 1. Augmented Lagrangian methods
 2. Primal-dual interior point methods
 3. Successive linear or quadratic approximations
 4. Semidefinite program (SDP) relaxation
- Under assumptions, convergence to optimum guaranteed by approach 4

Successive linearization

1. Start from the current operating point \mathbf{v}^0
2. Linearize all functions involved around current \mathbf{v}^t
3. Solve linearized OPF with respect to constrained increment $\delta\mathbf{v}^{t+1}$
4. Evaluate system conditions at $\mathbf{v}^{t+1} = \mathbf{v}^t + \delta\mathbf{v}^{t+1}$ via power flow
5. Return to Step 2 until convergence

Convergence, feasibility, or optimality are not guaranteed

Electric quantities as quadratic functions of voltages

Similar to the power flow problem:

- (re)active power injections
- (re)active line power flows
- squared current magnitudes
- squared voltage magnitudes

are all quadratic functions of \mathbf{v} in rectangular coordinates

Constraints can be expressed as non-convex quadratic inequalities

$$\underline{p}_m \leq p_m(\mathbf{v}) \leq \bar{p}_m \iff \underline{p}_m \leq \mathbf{v}^H \mathbf{M}_{P_m} \mathbf{v} \leq \bar{p}_m$$

Semidefinite program relaxation

- Introduce $\mathbf{V} = \mathbf{v}\mathbf{v}^H$ and express optimal power flow as:

$$\begin{aligned} \min_{\mathbf{v} \succeq \mathbf{0}, \text{rank}(\mathbf{V})=1} \quad & \sum_{n=1}^N c_n \text{Tr}(\mathbf{M}_{P_n} \mathbf{V}) \\ \text{s.to} \quad & \underline{s}_k \leq \text{Tr}(\mathbf{M}_k \mathbf{V}) \leq \bar{s}_k, \quad \forall k \end{aligned}$$

- Drop rank constraint to express OPF as an SDP
- Relaxation is exact under different operating assumptions
- Counterexamples with minimizers having rank higher than one do exist
- Problem simplifies to an SOCP for radial grids

X. Bai, H. Wei, K. Fujisawa, and Y. Wang, "Semidefinite programming for optimal power flow problems" *Int. J. Elect. Power Energy Syst.*, Vol. 30, No. 67, pp. 383-392, 2008.

J. Lavaei and S. Low, "Zero duality gap in optimal power flow problem," *IEEE Trans. on Power Systems*, Vol. 27, No. 1, Feb. 2012, pp. 92-107.

Generation planning

Operation vs. planning problems

Problem statement: where should we build new generation units?

$$\begin{aligned} \min_{\mathbf{p}, \mathbf{u}} \quad & \sum_{m=1}^N c_m u_m \\ \text{s.t.} \quad & u_m \underline{p}_m \leq p_m \leq u_m \bar{p}_m \\ & \mathbf{1}^\top \mathbf{p} = 0; \quad -\bar{\mathbf{f}} \leq \mathbf{S}\mathbf{p} \leq \bar{\mathbf{f}} \\ & u_m \in \{0, 1\} \end{aligned}$$

- integer or continuous u_m for placement and sizing tasks
- solved as MILP for hundreds of variables
- $\mathbf{u}^* = \mathbf{0}$ if system already feasible

Transmission planning or switching

Braess' paradox: opening a new road may increase average traffic delays!

Problem statements: Where should we build new transmission lines? Which existing lines should be active?

$$\begin{aligned} \min_{\mathbf{p}, \boldsymbol{\theta}, \mathbf{f}, \mathbf{u}} \quad & \sum_{\ell=1}^L c_{\ell} u_{\ell} \quad \text{or} \quad \sum_{m=1}^N C_m(p_m) \\ \text{s.to} \quad & \mathbf{p} = \mathbf{A}^{\top} \mathbf{f}; \quad \underline{\mathbf{p}} \leq \mathbf{p} \leq \bar{\mathbf{p}} \\ & \left| f_{\ell} - \frac{\mathbf{a}_{\ell}^{\top} \boldsymbol{\theta}}{x_{\ell}} \right| \leq M(1 - u_{\ell}) \\ & |f_{\ell}| \leq u_{\ell} \bar{f}_{\ell}, \quad u_{\ell} \in \{0, 1\} \end{aligned}$$

- **Big M trick:** satisfy one of two constraints: $f_1(\mathbf{p}) \leq Mu$ and $f_2(\mathbf{p}) \leq M(1 - u)$ for $u \in \{0, 1\}$ and for large M
- AC versions to incorporate reactive power and voltage stability issues