

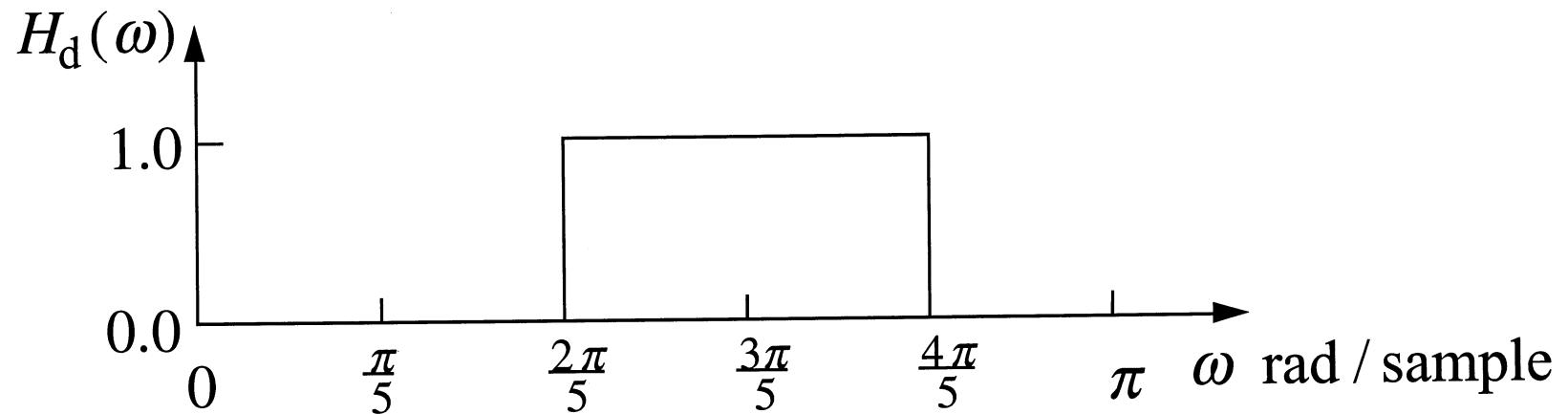
Digital Filter Design

Synopsis

- Overview of filter design problem
- Finite impulse response filter design
- Infinite impulse response filter design

Ideal Impulse Response

- Consider same ideal frequency response as before



- Inverse DTFT

$$h[n] = \frac{1}{2\pi} \int_{-\pi}^{\pi} H(\omega) e^{j\omega n} d\omega$$

Ideal Impulse Response (cont.)

$$h[n] = \frac{1}{2\pi} \left\{ \int_{-4\pi/5}^{-2\pi/5} e^{j\omega n} d\omega + \int_{2\pi/5}^{4\pi/5} e^{j\omega n} d\omega \right\}$$

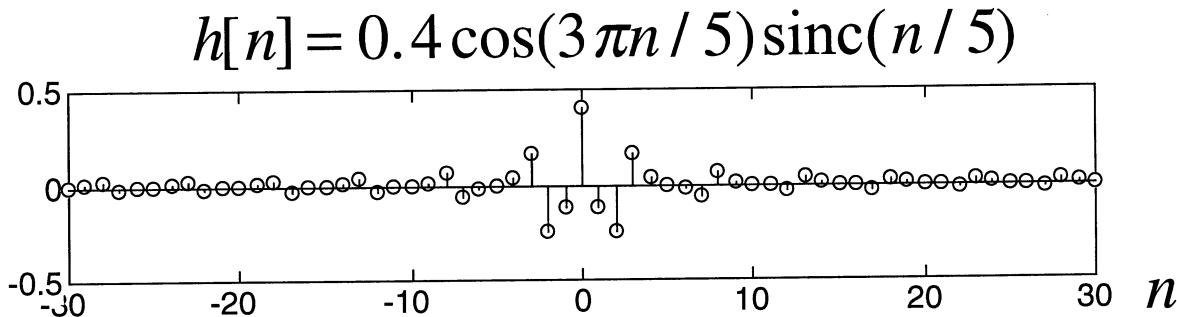
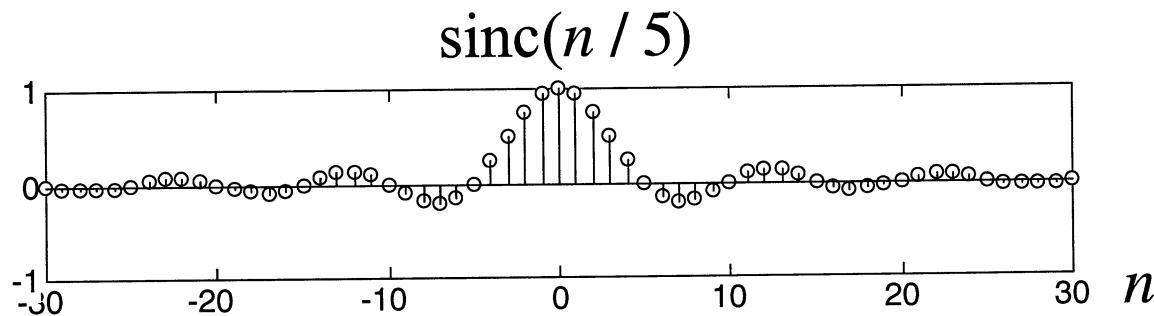
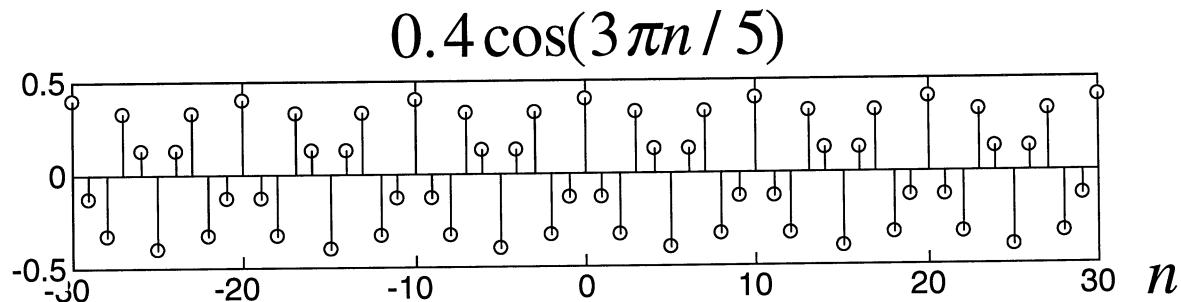
$$h[n] = \frac{1}{j2\pi n} \left\{ \left[e^{-j2\pi n/5} - e^{-j4\pi n/5} \right] + \left[e^{j4\pi n/5} - e^{-j2\pi n/5} \right] \right\}$$

$$h[n] = \frac{1}{j2\pi n} \left\{ e^{-j3\pi n/5} \left[e^{j\pi n/5} - e^{-j\pi n/5} \right] + e^{j3\pi n/5} \left[e^{j\pi n/5} - e^{-j\pi n/5} \right] \right\}$$

$$h[n] = \left\{ e^{-j3\pi n/5} \frac{1}{5} \text{sinc}\left(\frac{n}{5}\right) + e^{j3\pi n/5} \frac{1}{5} \text{sinc}\left(\frac{n}{5}\right) \right\}$$

Ideal Impulse Response (cont.)

$$h[n] = 0.4 \cos(3\pi n / 5) \operatorname{sinc}(n / 5)$$



Approximation of Desired Filter Impulse Response by Truncation

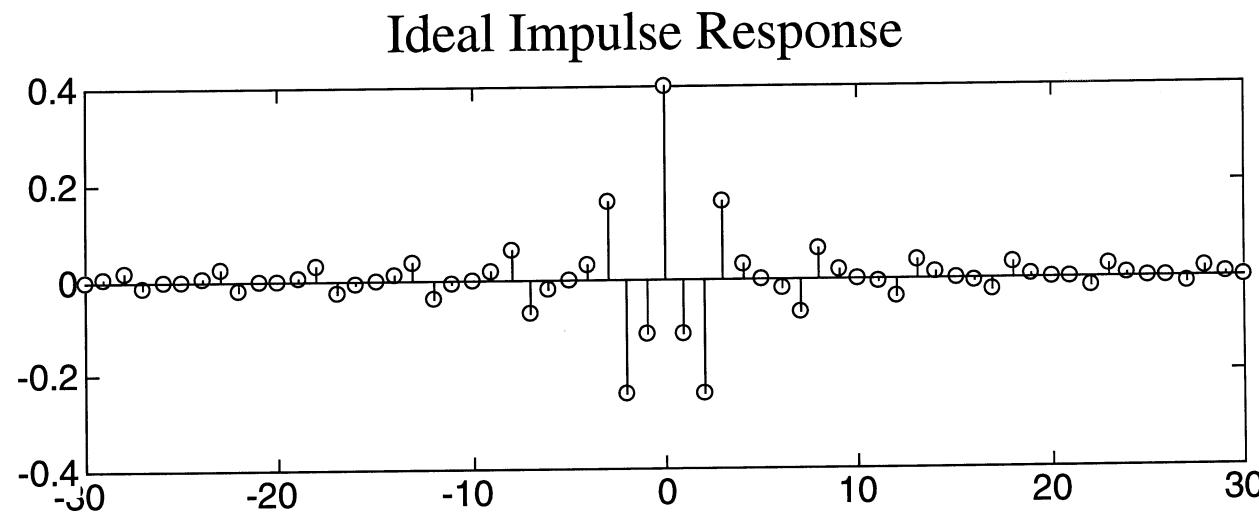
- FIR filter equation

$$y[n] = \sum_{m=0}^{M-1} a_m x[n-m]$$

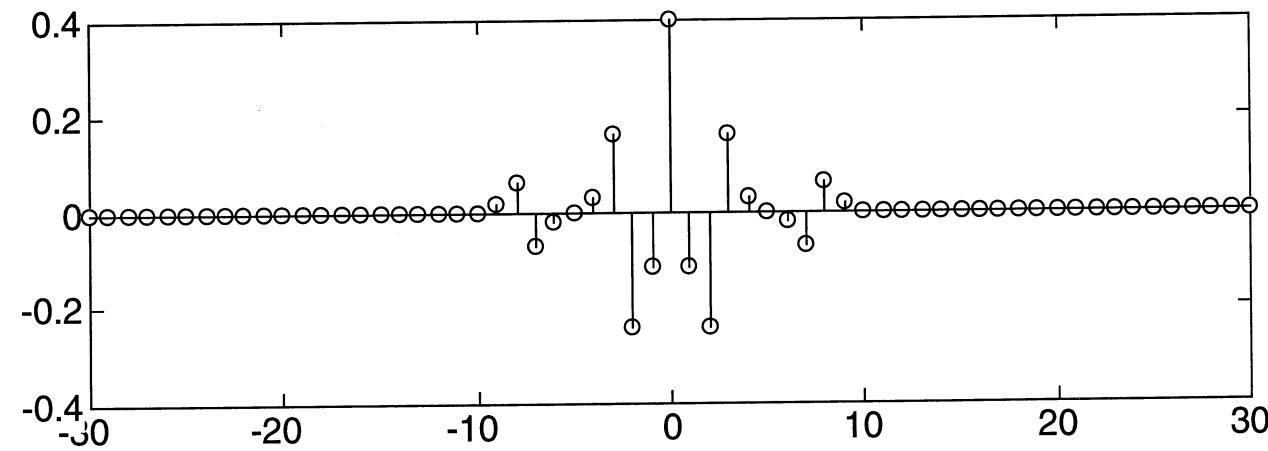
- Filter coefficients (assuming M is odd)

$$a_m = h_{\text{ideal}}[m - (M-1)/2], \quad m = 0, \dots, M-1$$

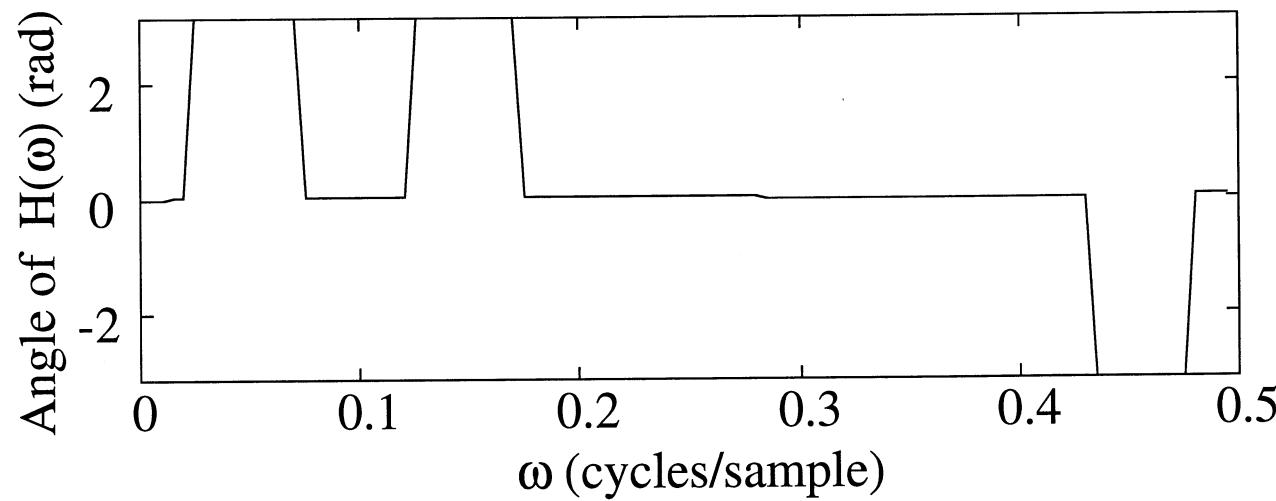
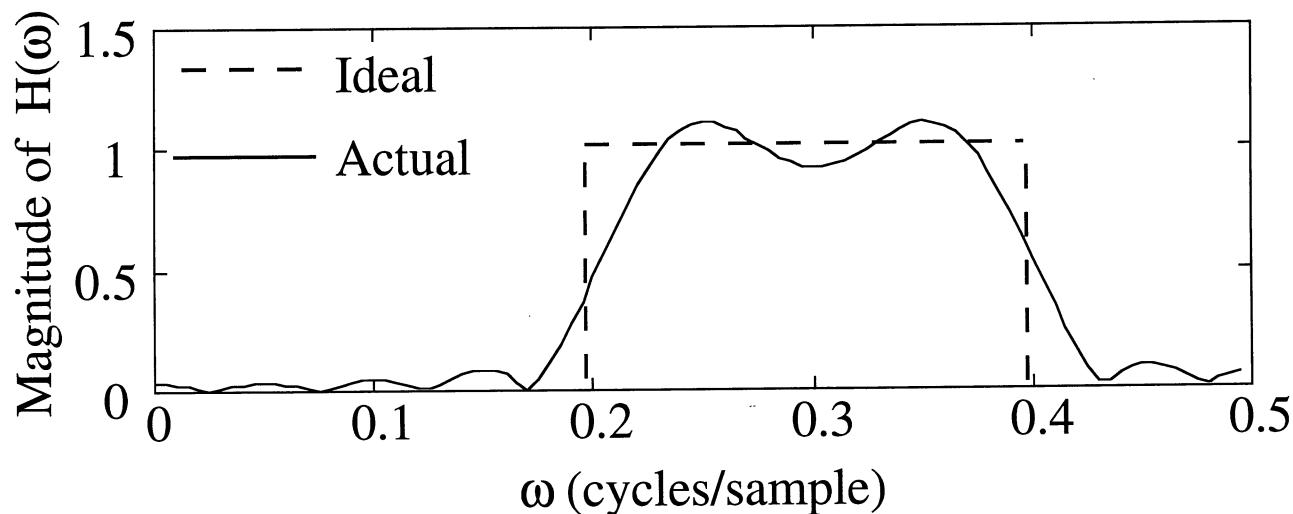
Truncation of Impulse Response (cont.)



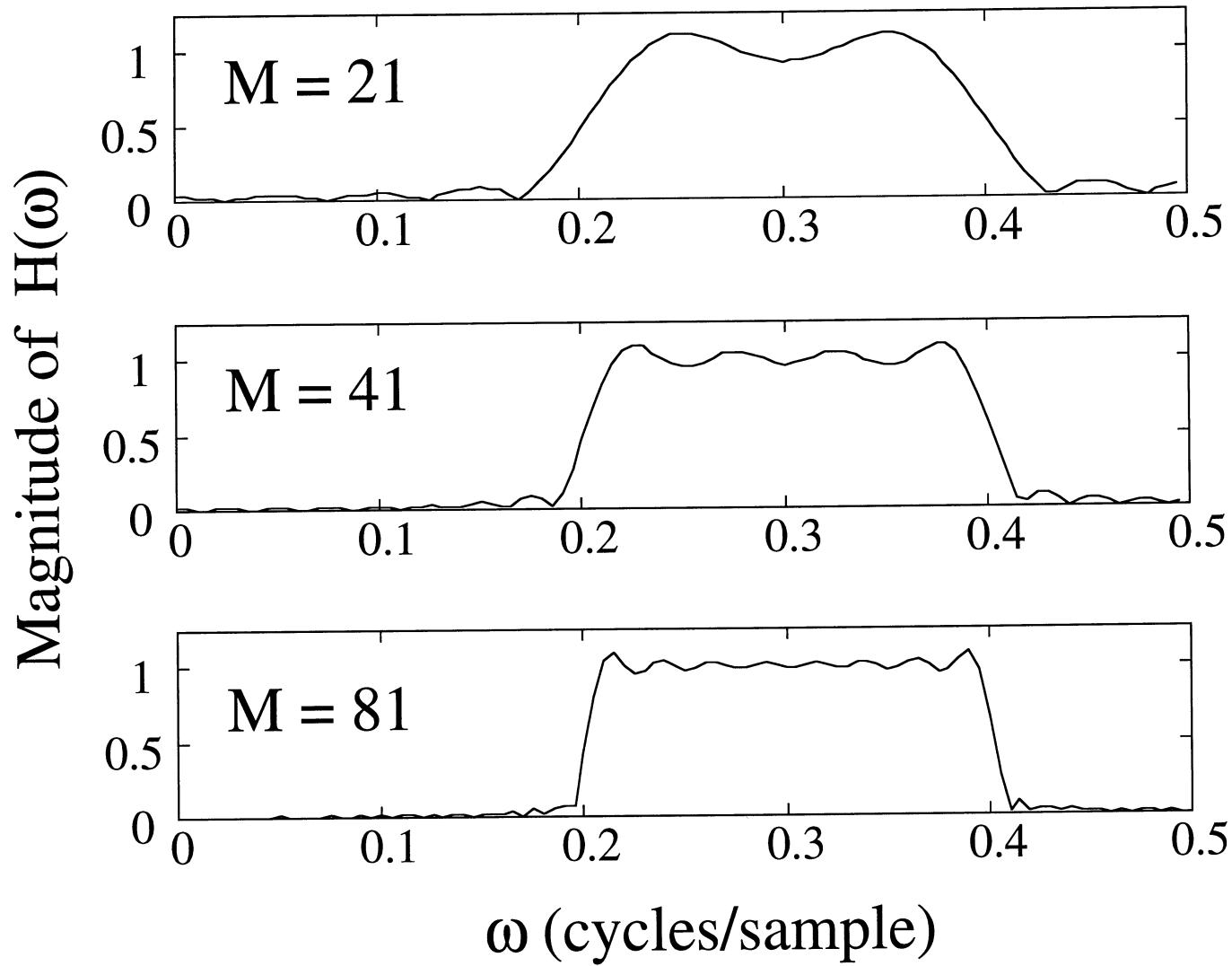
Truncated Impulse Response ($M = 21$)



Frequency Response of Truncated Filter



Effect of Filter Length



Analysis of Truncation

- **Ideal infinite impulse response** - $h_{\text{ideal}}[n]$
- **Actual, finite impulse response** - $h_{\text{actual}}[n]$
- **Window sequence** - $w[n]$

$$w[n] = \begin{cases} 1, & |n| \leq (M-1)/2 \\ 0, & \text{else} \end{cases}$$

- **Relation between ideal and actual impulse responses**

$$h_{\text{actual}}[n] = h_{\text{ideal}}[n]w[n]$$

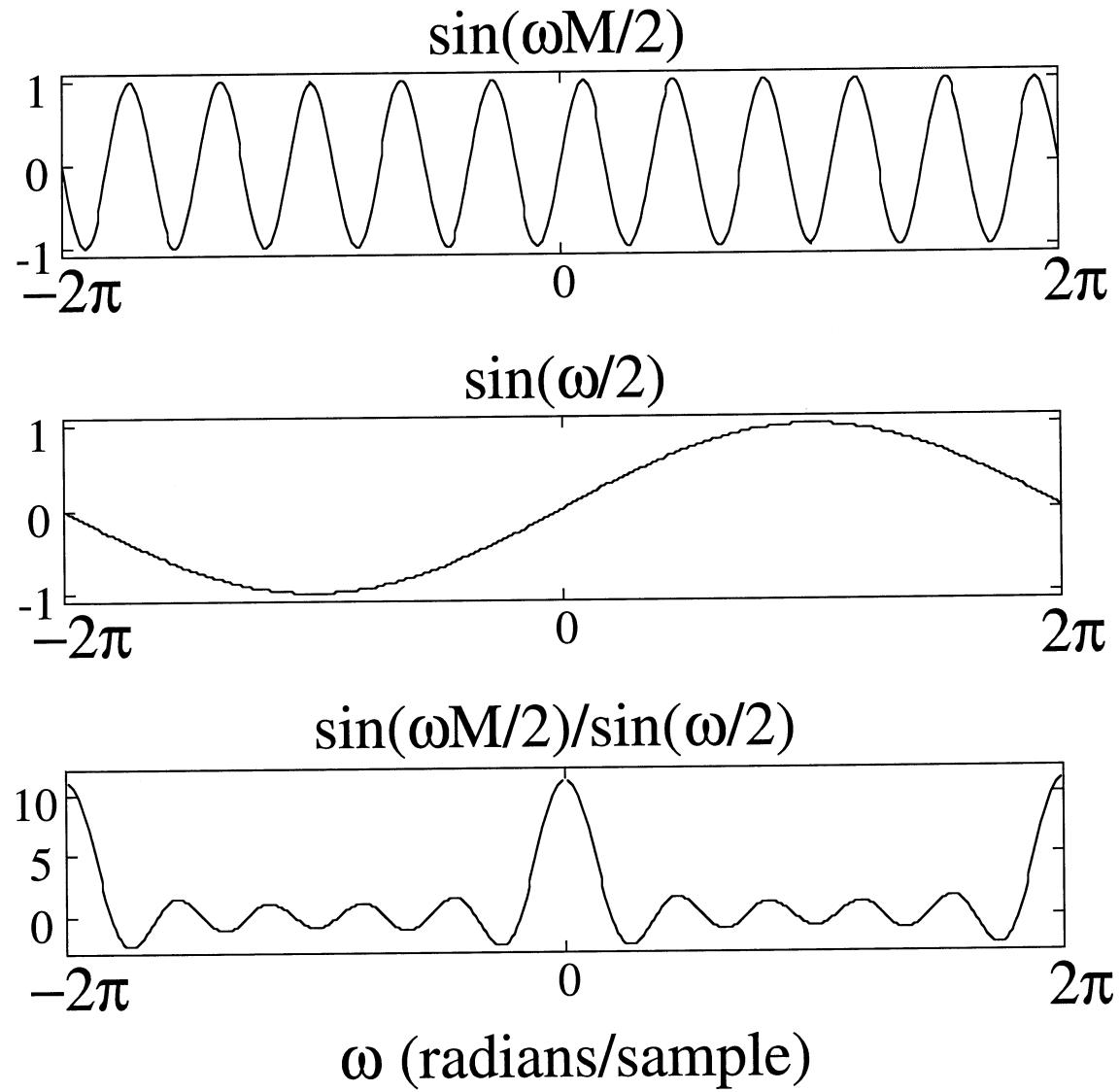
$$H_{\text{actual}}(\omega) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_{\text{ideal}}(\lambda)W(\omega - \lambda)d\lambda$$

DTFT of Rectangular Window

$$\begin{aligned} W(\omega) &= \sum_{n=-(M-1)/2}^{n=(M-1)/2} e^{-j\omega n} \\ &= \sum_{m=0}^{M-1} e^{-j\omega[m-(M-1)/2]} \\ &= e^{j\omega(M-1)/2} \frac{1 - e^{j\omega M}}{1 - e^{j\omega}} \\ &= \frac{\sin(\omega M / 2)}{\sin(\omega / 2)} \end{aligned}$$

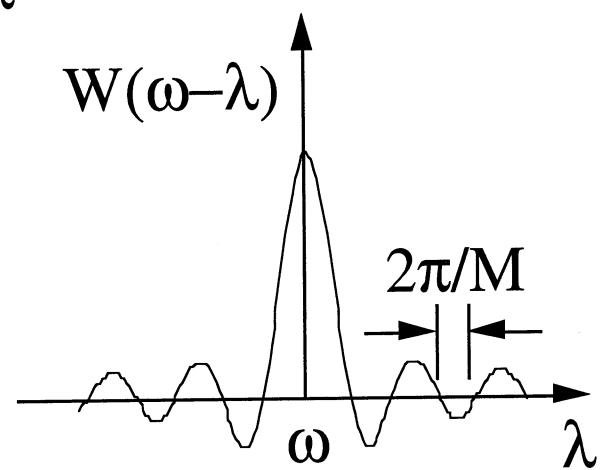
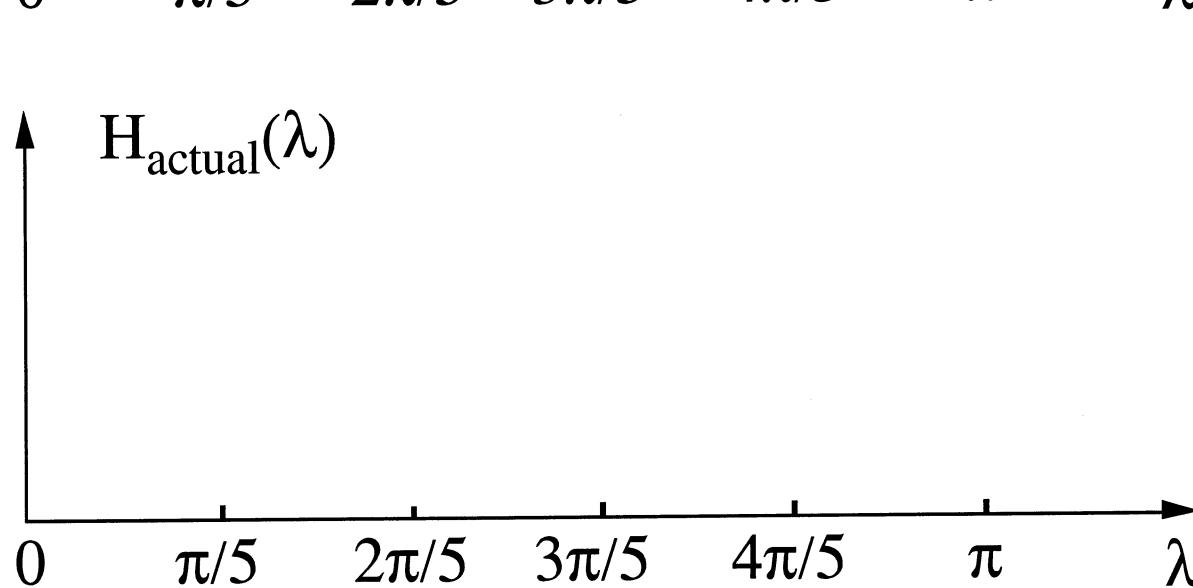
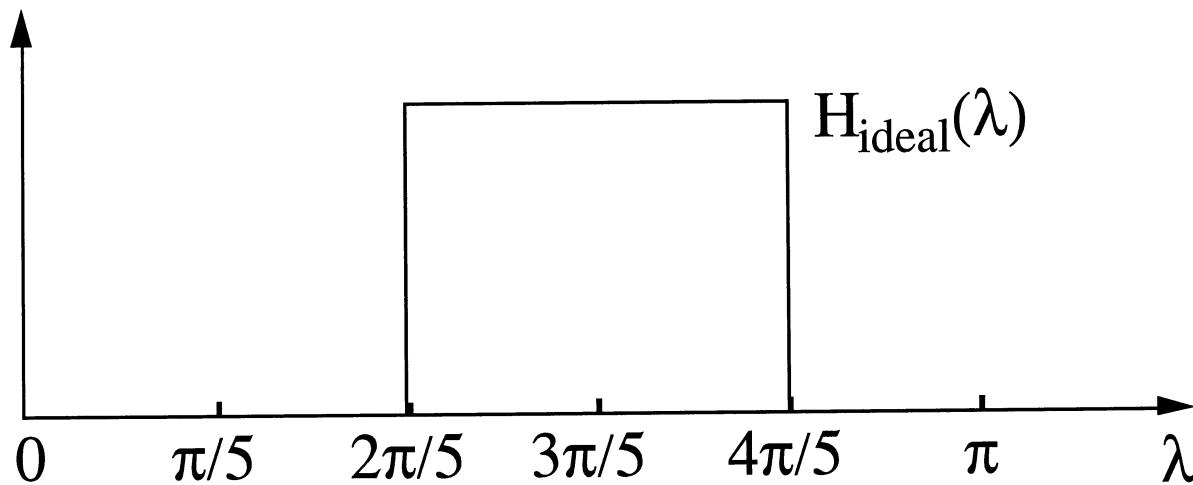
let $m = n + (M-1)/2$

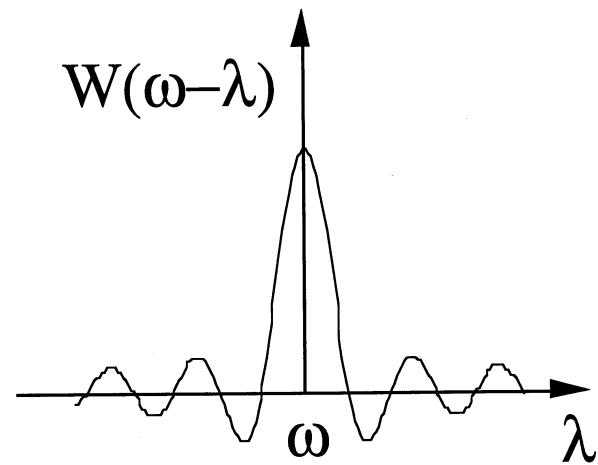
DTFT of Rectangular Window (Cont.)



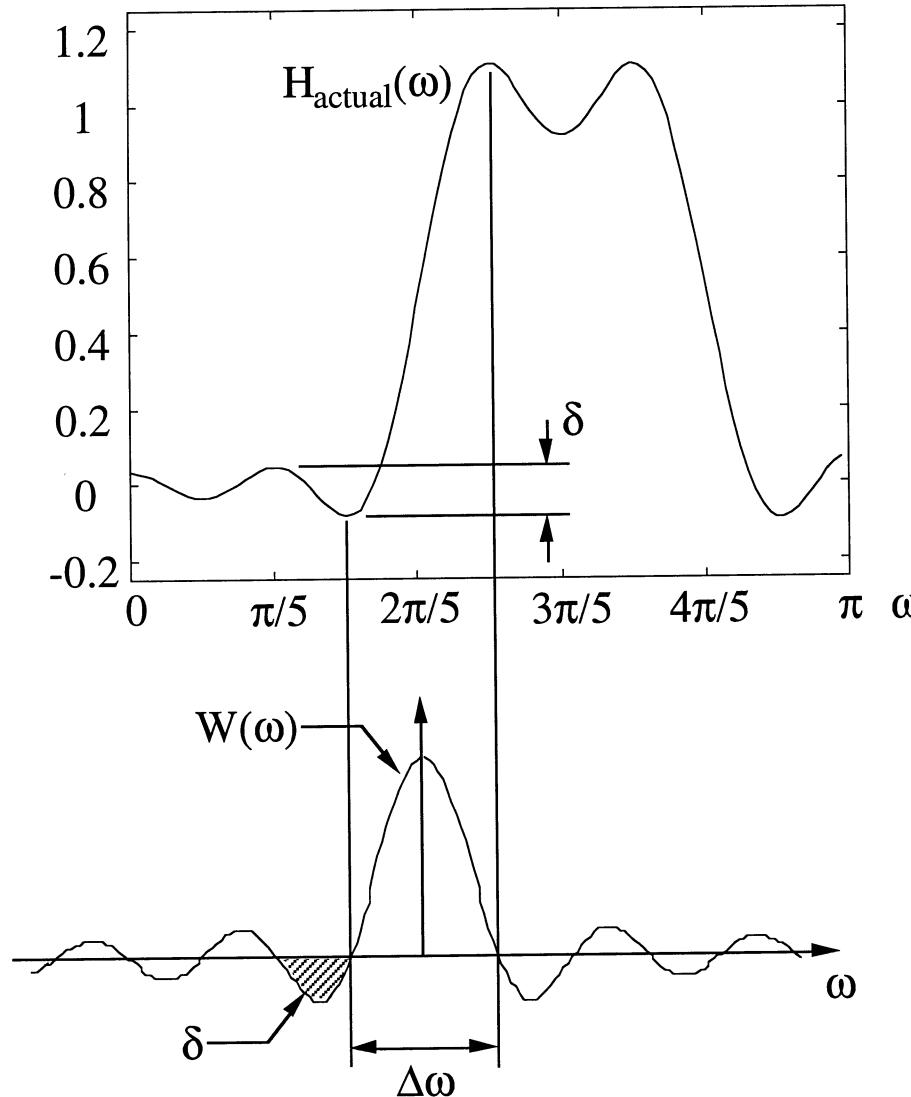
Graphical View of Convolution

$$H_{\text{actual}}(\omega) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_{\text{ideal}}(\lambda) W(\omega - \lambda) d\lambda$$





Relation between Window Attributes and Filter Frequency Response



Parameter	$W(\omega)$	$H_{actual}(\omega)$
$\Delta\omega$	Mainlobe width	Transition bandwidth
δ	Area of first sidelobe	Passband and stopband ripple

Design of FIR Filters by Windowing

- Relation between ideal and actual impulse responses

$$h_{\text{actual}}[n] = h_{\text{ideal}}[n]w[n]$$

- Choose window sequence $w[n]$ for which DTFT has
 - minimum mainlobe width
 - minimum sidelobe area
- Kaiser window is best choice
 - based on optimal prolate spheroidal wavefunctions
 - contains a parameter that permits tradeoff between mainlobe width and sidelobe area

Kaiser Window

$$w[n] = \begin{cases} \frac{I_0[\beta(1 - [(n - \alpha) / \alpha]^2)^{1/2}]}{I_0(\beta)}, & 0 \leq n \leq M-1 \\ 0, & \text{else} \end{cases}$$

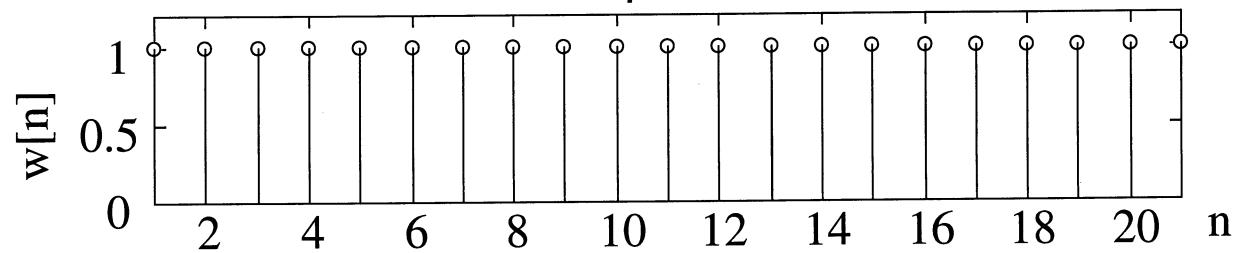
$$\alpha = (M-1)/2$$

$I_0(\cdot)$ zeroth-order modified Bessel function
of the first kind

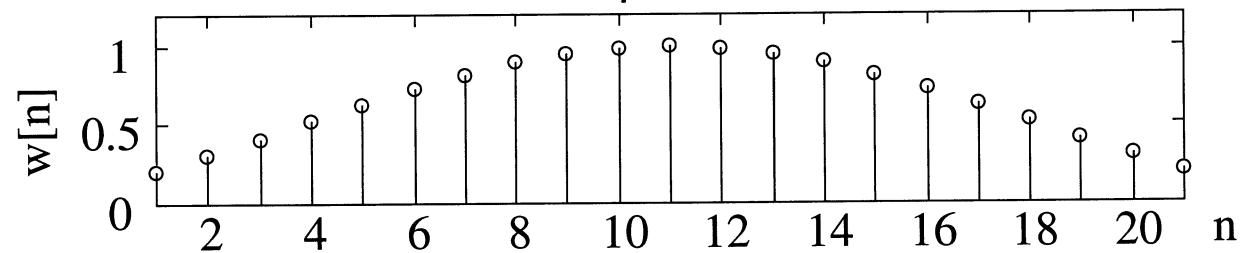
Effect of Parameter β

$M=21$

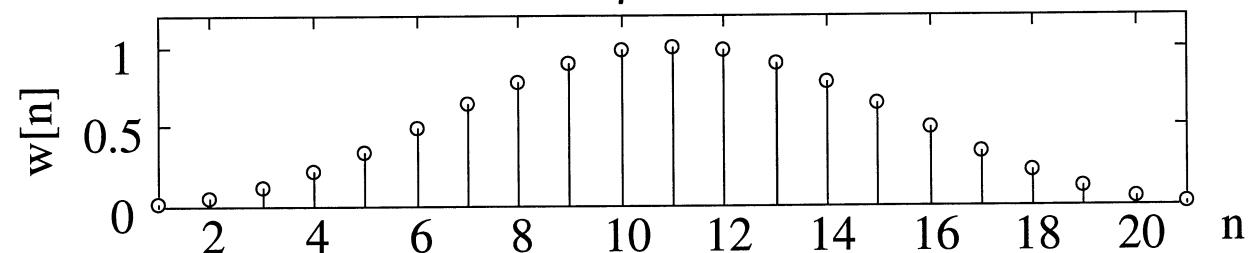
$\beta = 0$



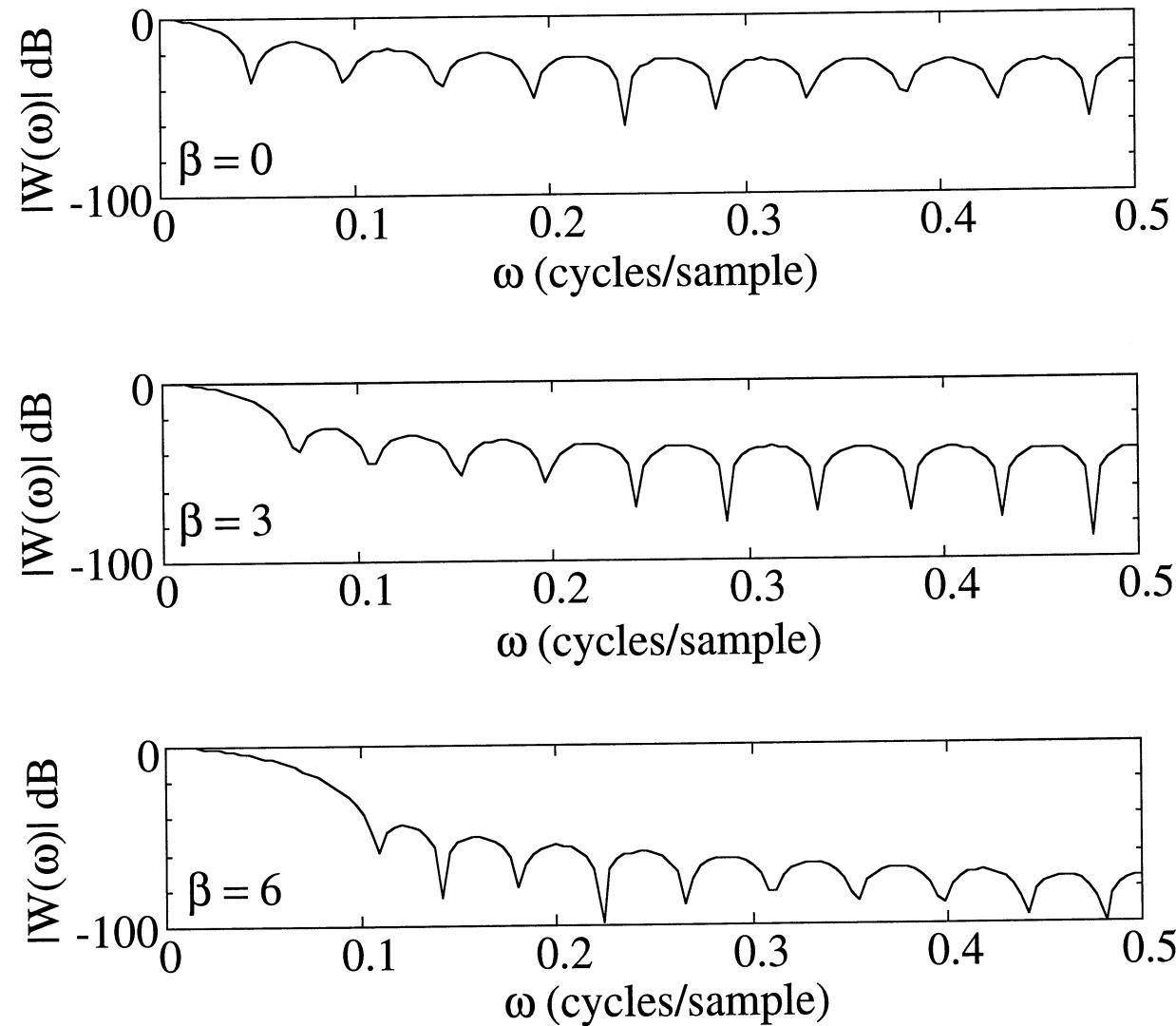
$\beta = 3$



$\beta = 6$

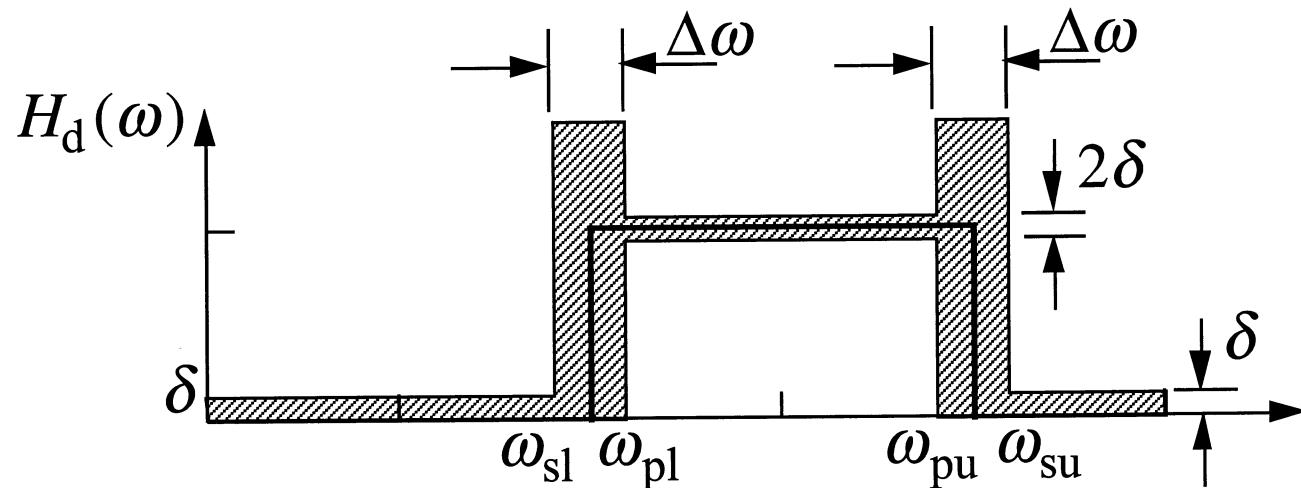


Effect of Parameter β (cont.)



Filter Design Procedure for Kaiser Window

1. Choose stopband and passband ripple and transition bandwidth



2. Determine parameter β

$$A = -20 \log_{10} \delta$$

$$\beta = \begin{cases} 0.112(A - 8.7), & A > 50, \\ 0.5842(A - 21)^{0.4} + 0.07886(A - 21), & 21 \leq A \leq 50, \\ 0.0, & A < 21. \end{cases}$$

Filter Design Procedure for Kaiser Window (cont.)

3. Determine filter length M

$$M = \frac{A - 8}{2.285\Delta\omega} + 1$$

- Example

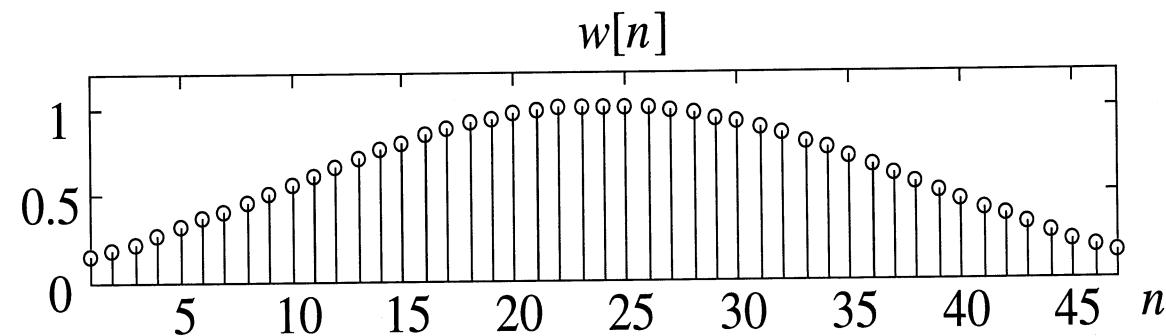
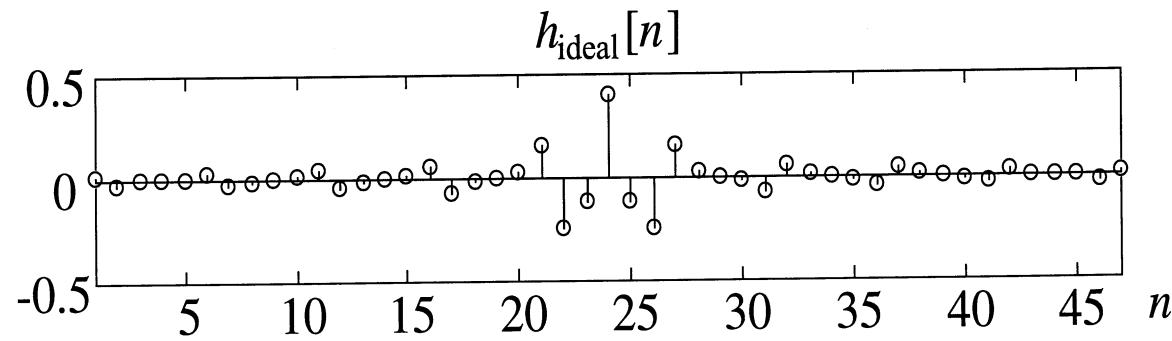
$$\begin{aligned}\Delta\omega &= 0.1\pi \text{ radians / sample} \\ &= 0.05 \text{ cycles / sample}\end{aligned}$$

$$\delta = 0.01$$

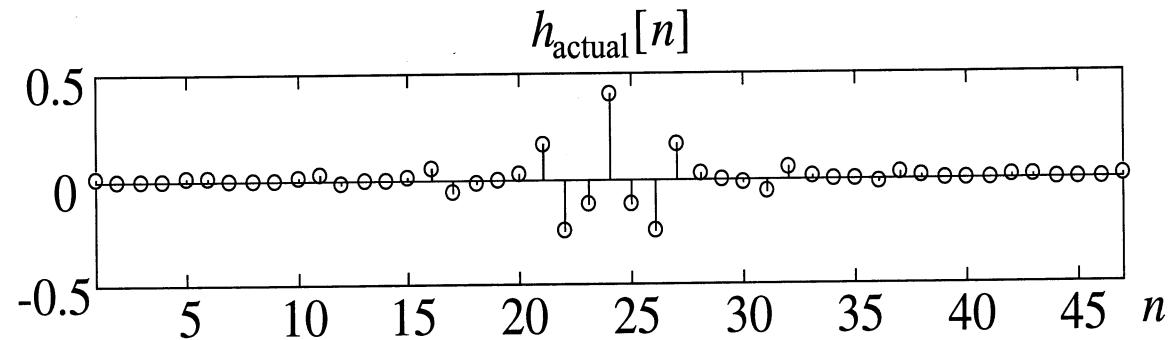
$$\beta = 3.4$$

$$M = 45.6$$

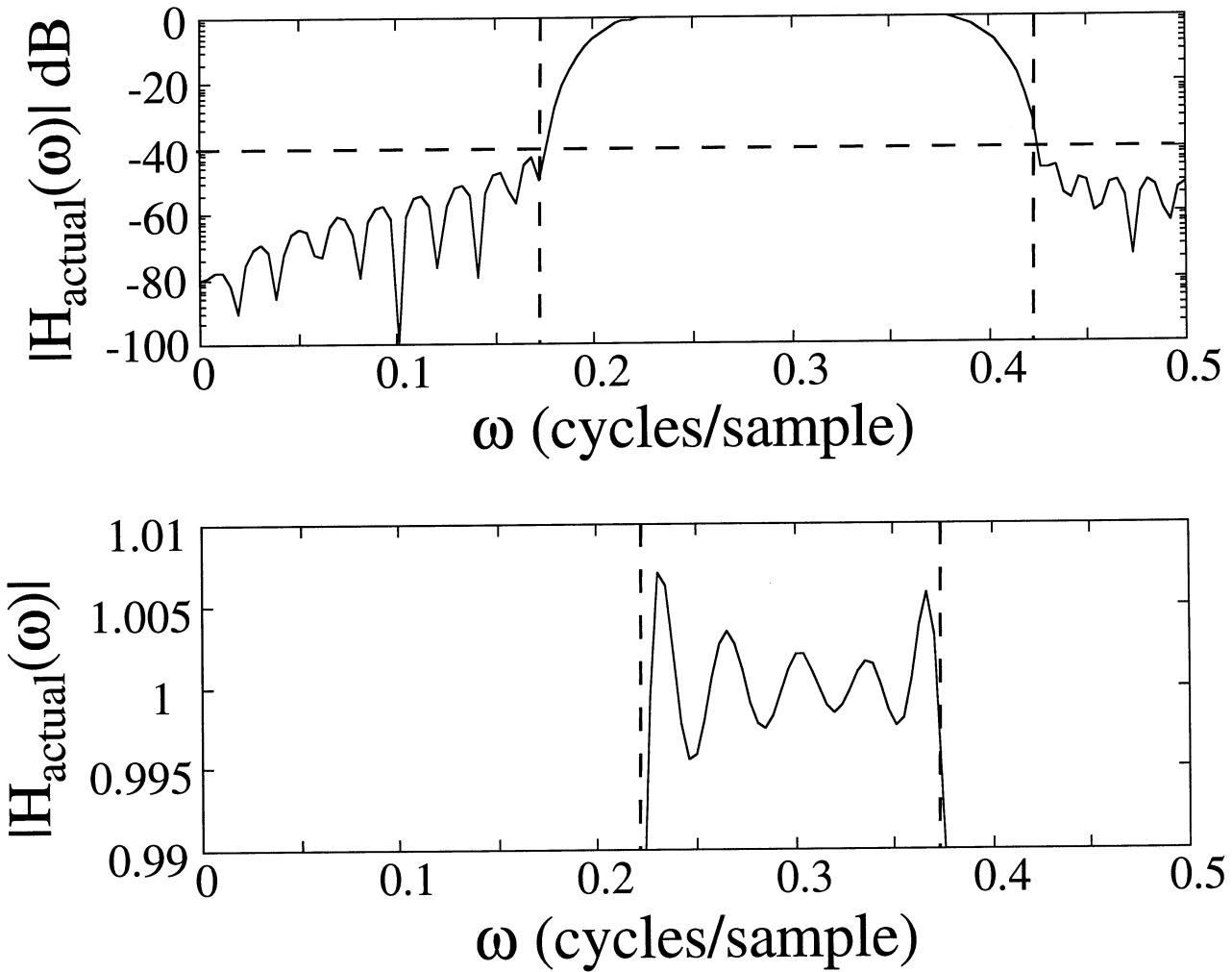
Filter Designed with Kaiser Window



$$M = 47$$
$$\beta = 3.4$$



Kaiser Filter Frequency Response



$$\begin{aligned}M &= 47 \\ \beta &= 3.4 \\ \delta &= 0.01 \\ &= -40 \text{ dB}\end{aligned}$$

$$\begin{aligned}\Delta\omega &= 0.05 \\ \omega_{\text{sl}} &= 0.175 \\ \omega_{\text{pl}} &= 0.225 \\ \omega_{\text{pu}} &= 0.375 \\ \omega_{\text{su}} &= 0.425\end{aligned}$$

Optimal FIR Filter Design

- Although the Kaiser window has certain optimal properties, filters designed using it are not optimal in any sense.
- Consider the design of filters to minimize integral mean-squared frequency error
- Problem:
 - Choose $h_{\text{actual}}[n], n = -(M-1)/2, \dots, (M-1)/2$ to minimize

$$E = \frac{1}{2\pi} \int_{-\pi}^{\pi} |H_{\text{actual}}(\omega) - H_{\text{ideal}}(\omega)|^2 d\omega$$

Minimum Mean-Squared Error Design

- Using Parseval's relation, we obtain a direct solution to this problem

$$E = \frac{1}{2\pi} \int_{-\pi}^{\pi} |H_{\text{actual}}(\omega) - H_{\text{ideal}}(\omega)|^2 d\omega$$

$$= \sum_{n=-\infty}^{\infty} |h_{\text{actual}}[n] - h_{\text{ideal}}[n]|^2$$

$$= \sum_{n=-(M-1)/2}^{(M-1)/2} |h_{\text{actual}}[n] - h_{\text{ideal}}[n]|^2 +$$

$$\sum_{n=-\infty}^{-(M+1)/2} |h_{\text{ideal}}[n]|^2 + \sum_{n=(M+1)/2}^{\infty} |h_{\text{ideal}}[n]|^2$$

Minimum Mean-Squared Error Design (cont.)

- Solution

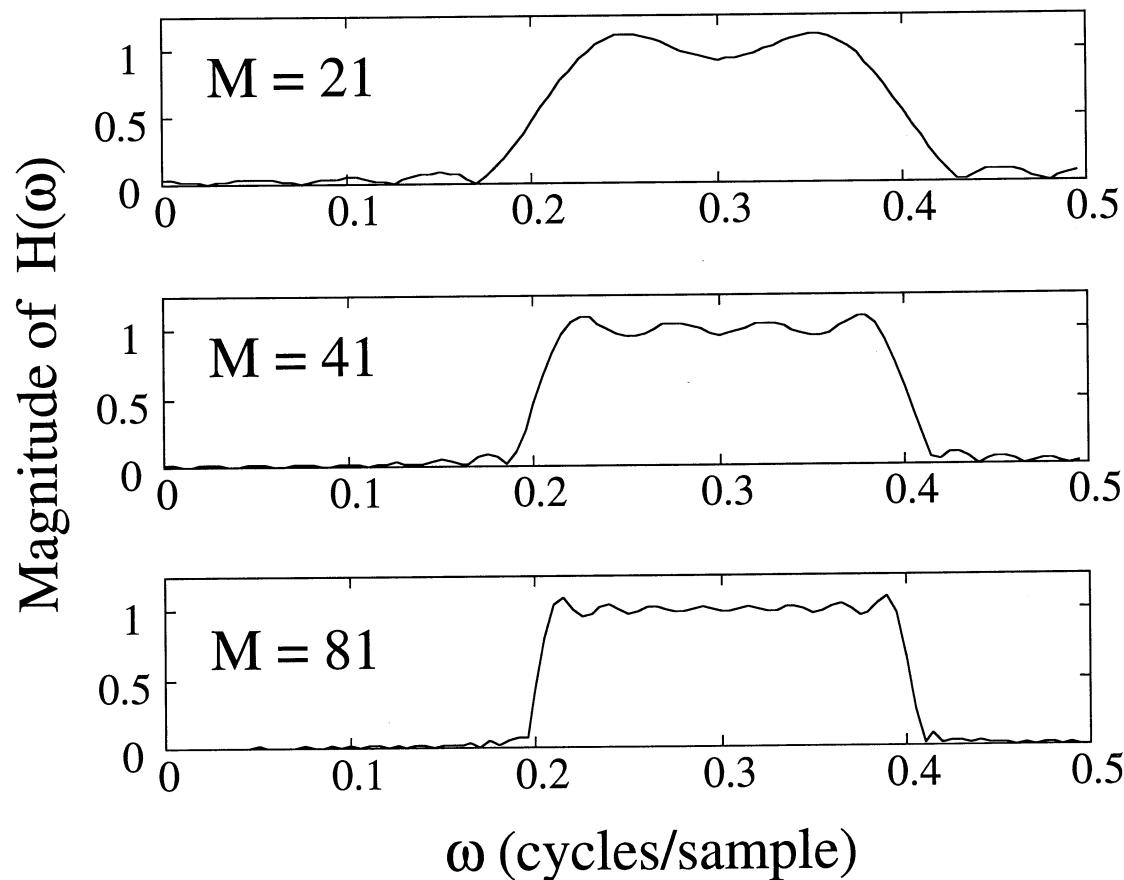
set $h_{\text{actual}}[n] = h_{\text{ideal}}[n]$, $n = -(M-1)/2, \dots, (M-1)/2$
minimum error is given by

$$E = \sum_{n=-\infty}^{-(M+1)/2} |h_{\text{ideal}}[n]|^2 + \sum_{n=(M+1)/2}^{\infty} |h_{\text{ideal}}[n]|^2$$

- But this is nothing more than truncation of the ideal impulse response
- Conclude that original criteria of minimizing mean-squared error was not a good choice

Minimum Mean-Squared Error Design (cont.)

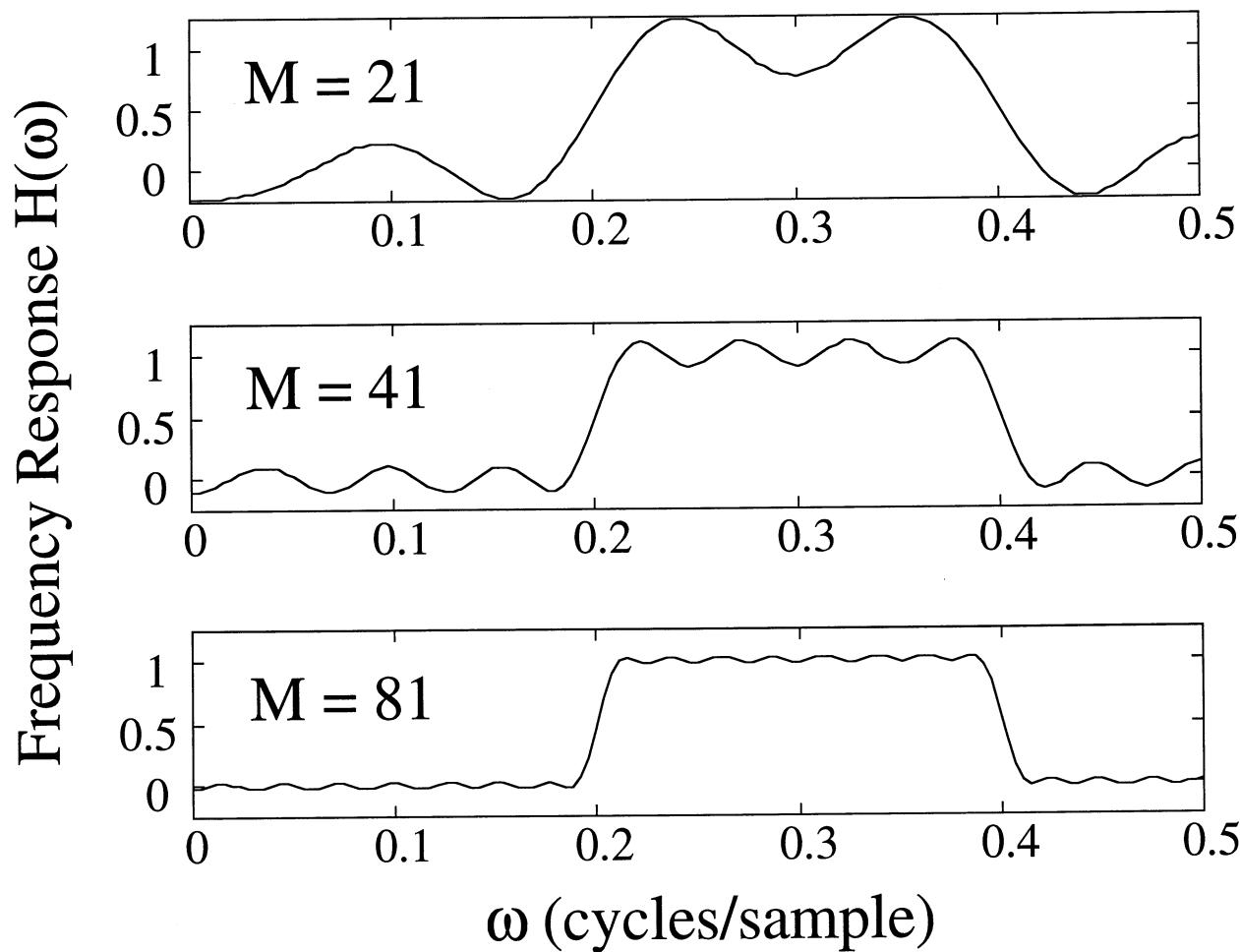
- What was the problem with truncating the ideal impulse response?



Minimax (Equi-ripple) Filter Design

- No matter how large we pick M for the truncated impulse response, we cannot reduce the peak ripple
- Also, the ripple is concentrated near the band edges
- Rather than focusing on the integral of the error, let's consider the maximum error
- Parks and McClellan developed a method for design of FIR filters based on minimizing the maximum of the weighted frequency domain error

Effect of Filter Length: Parks-McClellan Equiripple Filters



Comparison: Kaiser Window-Based and Parks-McClellan Filters

