2.2.2 DEVELOPMENT OF A GENERAL MODEL

Line-Continuous Flying Spot Process

$$egin{aligned} \mathbf{s}(\mathbf{t}) &= \int\limits_{-\infty}^{\infty} \int\limits_{-\infty}^{\infty} \mathbf{p_i} [\xi - \mathbf{x_s}(\mathbf{t}), \; \eta - \mathbf{y_s}(\mathbf{t})] \mathbf{p_r} [\xi - \mathbf{x_s}(\mathbf{t}), \; \eta - \mathbf{y_s}(\mathbf{t})] \ & imes \mathbf{g}(\xi, \eta) \; \mathrm{d}\xi \, \mathrm{d}\eta \end{aligned}$$

 $p_i(x,y)$ – illuminating spot profile

pr(x,y) – read spot profile

 $[x_s(t), y_s(t)] - scan trajectory$

g(x,y) — continuous-space still image

s(t) - scan signal

• Combine illuminating and read spot profiles as one function

$$p(x,y) = p_i(x,y) p_r(x,y)$$

- Separate the three processes:
 - integration over aperture
 - sampling
 - scanning (consider this later)

Integration over Aperture

$$s(t) = \int \int p[\xi - x_s(t), \eta - y_s(t)] g(\xi, \eta) d\xi d\eta$$

define

$$\begin{split} \tilde{\mathbf{g}}(\mathbf{x}, \mathbf{y}) &= \int \int \mathbf{p}[\xi - \mathbf{x}, \ \eta - \mathbf{y}] \ \mathbf{g}(\xi, \eta) \ \mathrm{d}\xi \ \mathrm{d}\eta \\ &= \int \int \mathbf{p}[-(\mathbf{x} - \xi), \ -(\mathbf{y} - \eta)] \ \mathbf{g}(\xi, \eta) \ \mathrm{d}\xi \ \mathrm{d}\eta \\ &= \mathbf{p}(-\mathbf{x}, \ -\mathbf{y}) \ ** \ \mathbf{g}(\mathbf{x}, \mathbf{y}) \end{split}$$

then

$$s(t) = \tilde{g} [x_s(t), y_s(t)]$$

Sampling

define

$$m q(x,y) = \int\limits_{-\infty}^{\infty} \delta[x-x_s(t), \ y-y_s(t)] \ dt$$

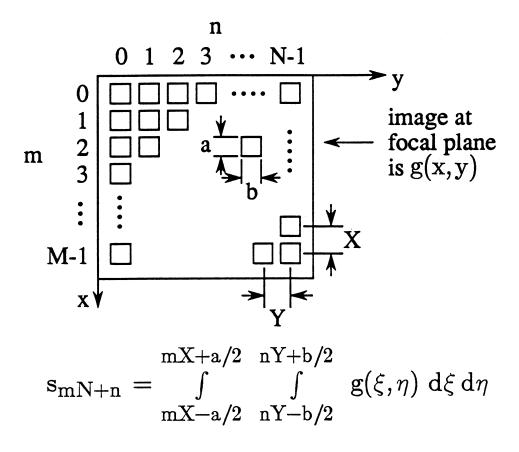
then let

$$\tilde{g}_s(x,y) = q(x,y) \; \tilde{g}(x,y)$$

This signal embodies all the effects due to the fact that we only see $\tilde{g}(x,y)$ along the locus of points $[x_s(t), y_s(t)], -\infty < t < \infty$.

With regard to these sampling effects, it is unimportant how we map the signal information into a 1-D function of time.

Focal Plane Array Scan Process



Integration over Aperture

$$s_{mN+n} = \int\limits_{-\infty}^{\infty} \int\limits_{-\infty}^{\infty} rect \left(\frac{\xi - mX}{a}, \ \frac{\eta - nY}{b} \right) g(\xi, \eta) d\xi \ d\eta$$

let

$$p(x,y) = rect(\frac{x}{a}, \frac{y}{b})$$

define

$$\tilde{\mathbf{g}}(\mathbf{x}, \mathbf{y}) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \mathbf{p}(\xi - \mathbf{x}, \eta - \mathbf{y}) \ \mathbf{g}(\xi, \eta) d\xi d\eta$$
$$= \mathbf{p}(-\mathbf{x}, -\mathbf{y}) ** \mathbf{g}(\mathbf{x}, \mathbf{y})$$

then

$$s_{mN+n} = \tilde{g}(mX, nY)$$

Sampling

define

$$q(x,y) = \sum_{m} \sum_{n} \delta(x-mX, y-nY)$$

then let

$$\tilde{g}_{\scriptscriptstyle S}(x,y) = q(x,y) \; \tilde{g}(x,y)$$

Again, this signal embodies all the effects due to the fact that we observe g(x,y) only at locations (mX,nY)

General Model for Scanning and Sampling

Aperture effects

$$\tilde{g}(x,y) = p(-x, -y) ** g(x,y)$$

$$\tilde{G}(u,v) = P(-u, -v) G(u,v)$$

- Aperture acts as a filter
- As p(x,y) spreads out, P(u,v) contracts resulting in attenuation of the higher frequency components of the image g(x,y).

Sampling effects

$$\tilde{g}_{s}(x,y) = q(x,y) \ \tilde{g}(x,y)$$

$$\tilde{G}_{S}(u,v) = Q(u,v) ** \tilde{G}(u,v)$$

- Since q(x,y) generally contains periodic structures, Q(u,v) will consist of an array of impulses.
- Convolution of Q(u,v) with $\tilde{G}(u,v)$ will result in replications of $\tilde{G}(u,v)$ located at the coordinates of each impulse in Q(u,v).