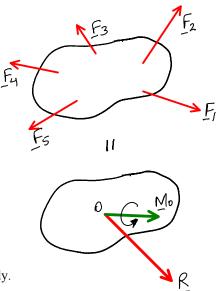
Chapter 4: Equilibrium of Rigid Bodies

A (rigid) body is said to in equilibrium if the vector sum of <u>ALL forces</u> and all their <u>moments</u> taken about <u>any (and all) points</u> is <u>zero</u>.

$$\begin{split} &\sum \vec{F} = 0 \\ &\sum \vec{M}_o = \sum \left(\vec{r} \times \vec{F} \right) = 0 \end{split}$$

In x, y, z components:

$$\begin{split} & \sum F_x = 0 \qquad \sum F_y = 0 \qquad \sum F_z = 0 \\ & \sum M_x = 0 \qquad \sum M_y = 0 \qquad \sum M_z = 0 \end{split}$$



These equations give 6 independent equations in 3D space for each (rigid) body.

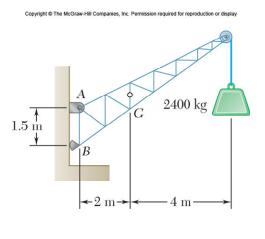
4.2 Free Body Diagrams

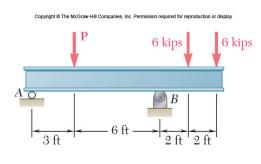
The free body diagram is a depiction of an object or a body along with <u>all</u> the external forces acting on it.

Steps in drawing a FBD of a body:

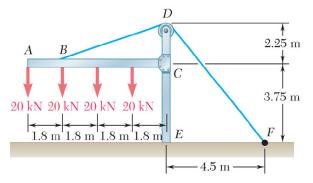
- Choose and draw the body (with dimensions). Carefully define its boundaries.
- Imagine the body in its current state and how it interacts with its surroundings.
- Draw <u>ALL</u> the <u>external</u> forces acting <u>on</u> the body (including self-weight).
- Any <u>unknown</u> forces acting on the body (required to keep it in equilibrium) must also be drawn.











4.3 REACTIONS coming from the supports

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Usually a body is constrained against motion using supports.

The forces from these supports, acting on the body are <u>external</u> to the body and must be included in the FBD.

The magnitude of these support forces are usually unknown and are obtained by solving the equilibrium equations.

Some examples of these support reactions are:

Courtesy National Information Service for Earthquake Engineering, University of California, Berkeley

Number of Support or Connection Reaction Unknowns 1 Force with known Frictionless Rocker Rollers line of action surface 1 Short cable Short link Force with known line of action 1 Collar on Force with known Frictionless pin in slot frictionless rod line of action 2 Frictionless pin Rough surface Force of unknown or hinge direction 3 Fixed support Force and couple

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It is very important to correctly estimate the **<u>number</u>** and **<u>type</u>** of reactions that a support can provide.

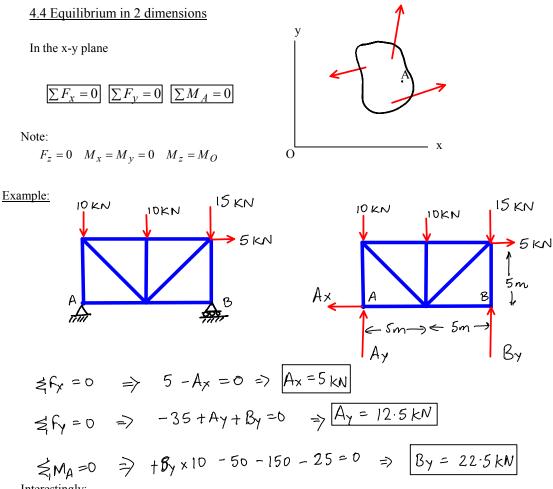
One way to determine that is:

- Imagine yourself in the position of the body ().
- Now ask the question:
 "If I wanted to move in the x or y or z direction, would the support be able to stop my movement in that direction?"
- If the answer is "yes" then there <u>will</u> be an unknown reaction <u>force</u> from the support acting on the body in that direction.

Conversely if the support cannot stop my motion in some direction, then there will <u>not</u> be a reaction force in that direction.

- Same thing holds true for <u>rotations</u>. "If I wanted to <u>rotate</u> in the x or y or z direction, would the support be able to stop my rotation in that direction?"
- If the answer is "yes" then there <u>will</u> be an unknown reaction <u>moment</u> acting on the body in that direction. Conversely if the support cannot stop my rotation in some direction, then there will <u>not</u> be a reaction moment in that direction.

Monday, September 21, 2009 12:22 PM



Interestingly:

• The 3 equilibrium equations above can also be <u>replaced</u> with the following equivalent equations: (only for 2 dimensions)

(A)
$$\sum F_x = 0 \sum M_A = 0 \sum M_B = 0$$

(where the line AB is not perpendicular to the x-axis)

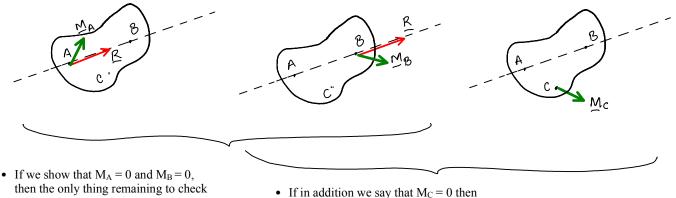
OR

 $\sum M_A = 0 \quad \sum M_B = 0 \quad \sum M_C = 0$ (B) (where A, B and C are not all along the same line)

Reason is:

would be $\Sigma F = 0$ along AB.

Consider the equivalent force & moments at points A, B and C:

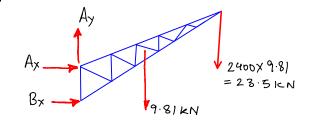


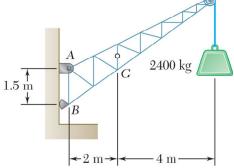
that possibility is ruled out as well.

A fixed crane has a mass of 1000 kg and is used to lift a 2400 kg crate. It is held in place by a pin at A and a rocker at B. The center of gravity of the crane is located at G.

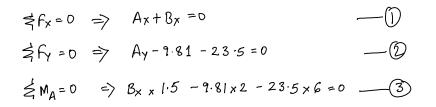
Determine the components of the reactions at A and B.

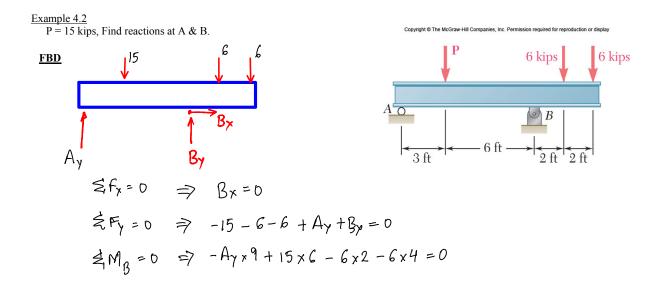
FBD





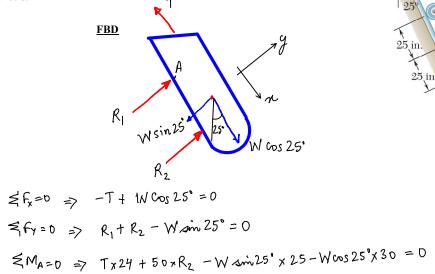
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A loading car is at rest on an inclined track. The gross weight of the car and its load is 5500 lb, and it is applied at at *G*. The cart is held in position by the cable.

Determine the tension in the cable and the reaction at each pair of wheels.



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G

2.25 m

3.75 m

F

30 in.

24 in.

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C

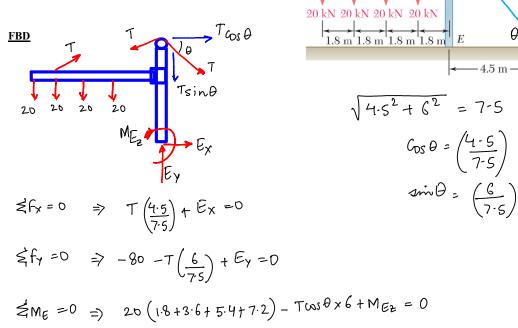
В

A

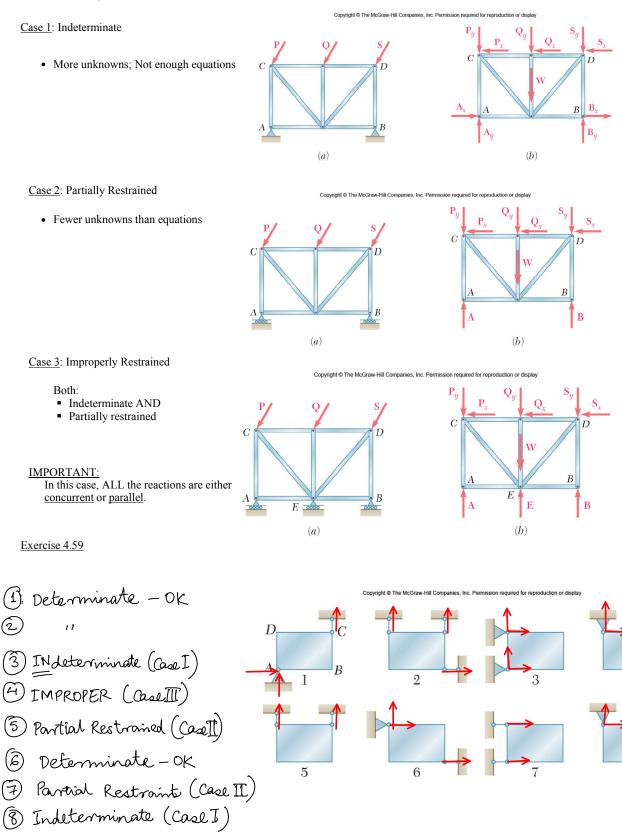
Example 4.4

The frame supports part of the roof of a small building. The tension in the cable is 150 kN.

Determine the reaction at the fixed end *E*.



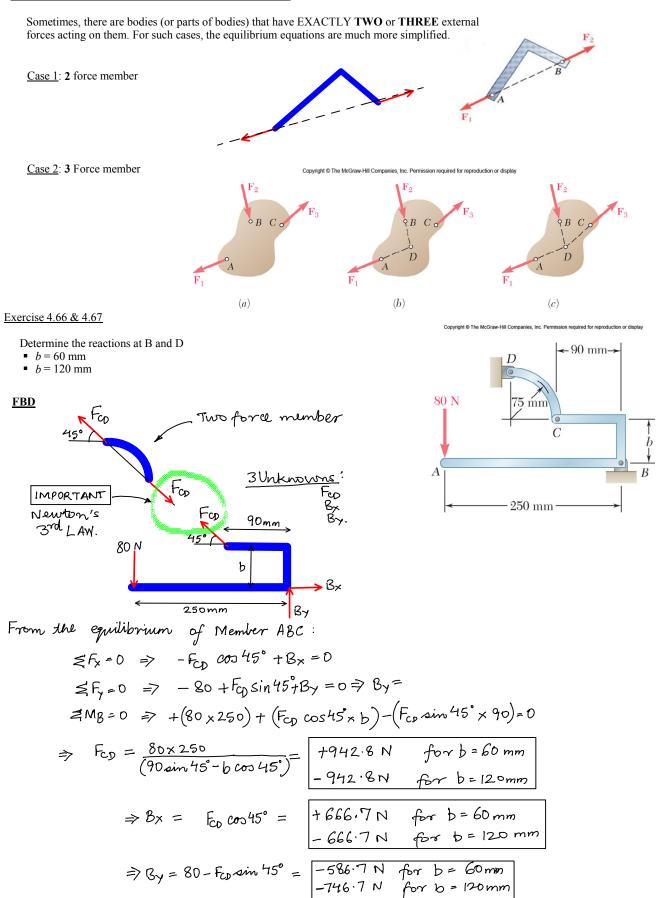
4.5 Statically INDETERMINATE Reactions



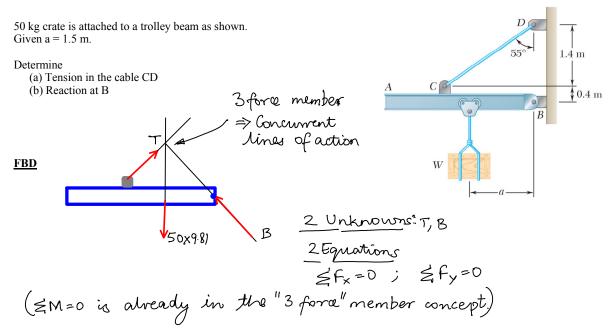
4

8

4.6 - 4.7 Two Force members & Three Force members

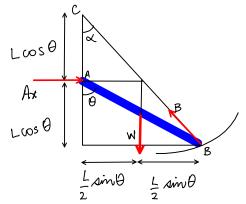


CE297-FA09-Ch4 Page 7





Find an equation in R, L and θ that governs Equilibrium.



At this point θ can be found simply from geometry.

 Vertical distance: Horizontal distance:

R

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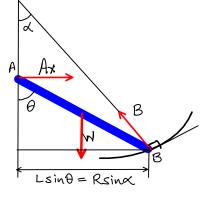
 $2L\cos\theta = R\cos\alpha$ $L\sin\theta = R\sin\alpha$ Eliminate " α " to get an equation $in \theta, R, L$.

Alternatively:

Without using the fact that this is a 3-force member:

Geometry:

$$\begin{bmatrix} \text{Lsim}\,\theta = R \, \text{sin} \propto \end{bmatrix} (\text{gives } \alpha \text{ in terms of } \theta) \\
+ \\ \begin{bmatrix} \Xi \, f_X = 0 \\ \Xi \, f_Y = 0 \\ \Xi \, K_Y = 0 \\ \Xi \, M_B = 0 \end{bmatrix} \xrightarrow{\text{3 unknowns}} (A_X, B_, \theta)$$



4.8 - 4.9 Equilibrium of Bodies in 3D space

- Draw the **<u>FBD</u>**
- Equations of equilibrium are given by:

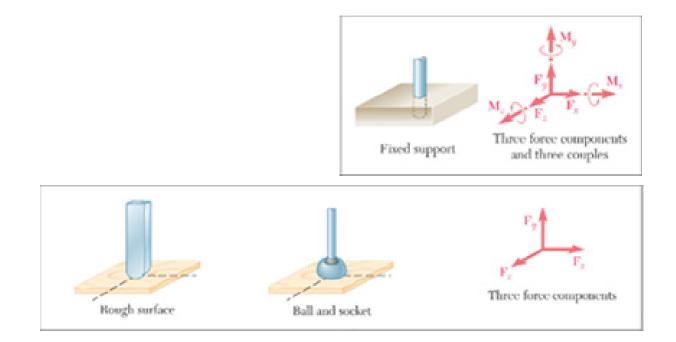
$$\sum \vec{F} = 0$$
$$\sum \vec{M}_{O} = \sum \left(\vec{r} \times \vec{F} \right) = 0$$

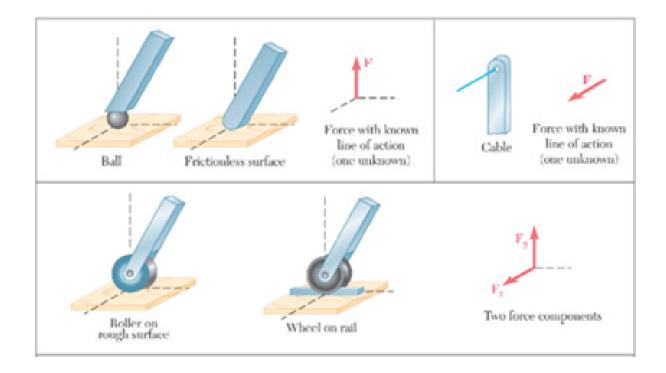
• <u>6 scalar equations</u> are required to express the conditions for the equilibrium of a rigid body in the general three dimensional case.

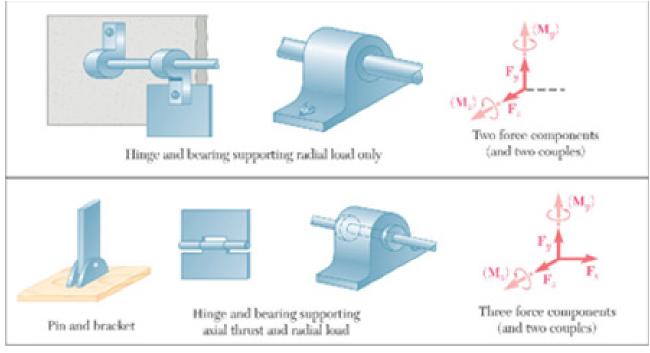
$$\begin{split} & \sum F_x = 0 \qquad \sum F_y = 0 \qquad \sum F_z = 0 \\ & \sum M_x = 0 \qquad \sum M_y = 0 \qquad \sum M_z = 0 \end{split}$$

• <u>6 unknown reactions</u> can be solved for.

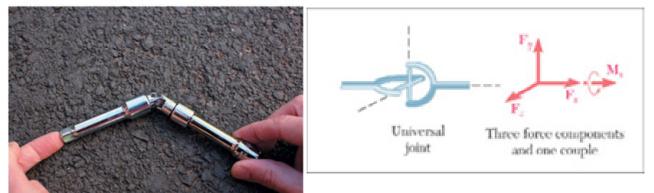
Some unknown reactions in 3D:







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Friday, October 02, 2009 10:45 AM

Examples 4.7

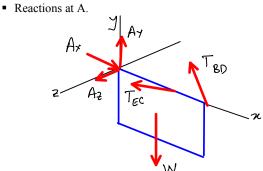
Copyright @ The McGraw-Hill Compa sion required for reproduction or dis es, Inc. Permis CGiven W = Ladder + Person= 100 x 9.81 = 981 N The wheels at A & B are flanged while the wheel at C is unflanged. 3 m Determine reactions at A, B and C 0.6 m Cz 0.6 m В 0.3 m 0.9 m 7 = 0.91 - 0.6K W= 981N Note: unrestrained in "x". Az 5 unknowns 5 equations x Bz \$F=0 $\Rightarrow 0 \underline{i} + (A_{y} + B_{y} - W) \underline{j} + (A_{z} + B_{z} + C_{z}) \underline{k} = \underline{0}] 2 \text{ equations}$ ZM=Z7×F=0 $\Rightarrow \leq \vec{M}_{A} = (\vec{r}_{AB} \times \vec{F}_{B}) + (\vec{r}_{AC} \times \vec{F}_{C}) + (\vec{r}_{AW} \times \vec{W})$ $(\text{about } A)^{n} = \left[1 \cdot 2 \cdot \underline{i} \times (B_{y} \cdot \underline{j} + B_{z} \cdot \underline{k})\right] + \left[(0 \cdot 6 \cdot \underline{i} + 3 \cdot \underline{j} - 1 \cdot 2 \cdot \underline{k}) \times C_{z} \cdot \underline{k}\right]$ 3equations + [(09i-0.6k)×(-wj)]

Example 4.8

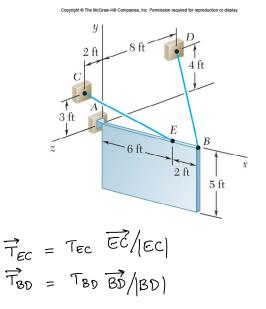
Given W = 270 lbs

Determine

• Tensions in AE and BD.



Note: Unrestrained in rotation about x. Unknowns: Ax, Ay, Az, TEC, TBD



CE297-FA09-Ch4 Page 11

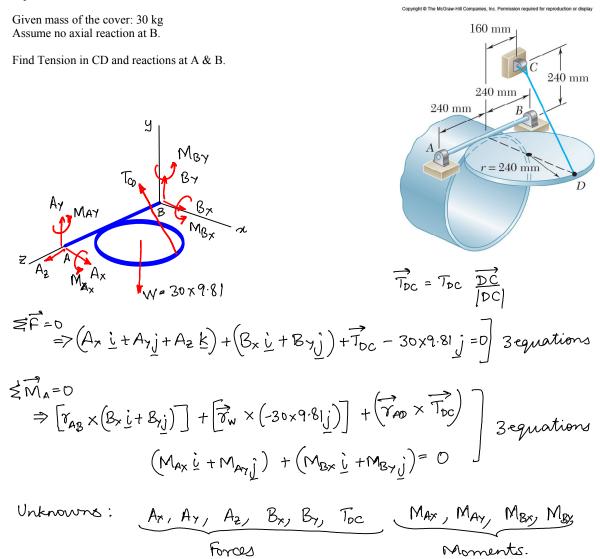
$$\vec{z}\vec{F} = 0$$

$$\vec{z} \neq A_{x}\vec{i} + A_{y}\vec{j} + A_{z}\vec{k} + \vec{T}ec + \vec{T}BD - 270\vec{j} = 0] \quad 3equations$$

$$\vec{z}\vec{M} = 0$$

$$\vec{z}_{AE} \times \vec{T}Ec + \vec{T}BD + \vec{z}_{AB} \times \vec{T}BD + \vec{z}_{AE} \times (-270\vec{j}) = 0] \quad 2equations$$

$$\vec{z} = \vec{z}_{AE} \times \vec{T}Ec + \vec{z}_{AB} \times \vec{T}BD + \vec{z}_{AB} \times (-270\vec{j}) = 0] \quad 2equations$$

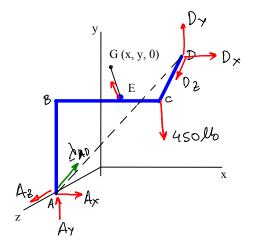


<u>Note</u>: The book assumes that $M_{A_X} = M_{A_Y} = M_{B_X} = M_{B_Y} = 0$. This is <u>not</u> a good assumption.

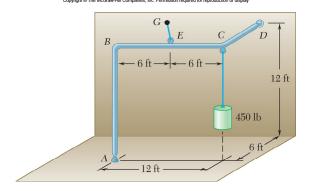
Given W = 450 lb.

Find

- Location of G so that the tension EG is minimum
- This minimum value of tension



Moment about AD:



$$\overrightarrow{AD} = 12 \underline{i} + 12 \underline{j} - 6 \underline{k}$$

$$\overrightarrow{\lambda}_{AD} = 27_3 \underline{i} + 2_3 \underline{j} - \frac{1}{3} \underline{k}$$

$$\overrightarrow{EG} = (\alpha - 6) \underline{i} + (y - 12) \underline{j}^* - 6 \underline{k}$$

$$\overrightarrow{TEG} = T \quad \overrightarrow{\lambda}EG = T \quad \overrightarrow{EG}$$

$$[EG]$$

 $= M_{ab} = \overline{\lambda}_{ab} \cdot \left[\left(\overline{\gamma}_{AE} \times \overline{T}_{EQ} \right) + \left(\overline{\gamma}_{AC} \times \overline{W} \right) \right] = 0$ $= \overline{\lambda}_{ab} \cdot \left(\overline{\gamma}_{AE} \times \overline{T}_{EQ} \right) + \frac{\overline{AD}}{|AD|} \cdot \left[\left(12 \underline{i} + 12 \underline{j} \right) \times (-450 \underline{j}) \right] = 0$ $= \overline{\lambda}_{ab} \cdot \left(\overline{\gamma}_{AE} \times \overline{T}_{EQ} \right) + \left(\frac{2}{3} \underline{i} + \frac{2}{3} \underline{j} - \underline{j} \underline{k} \right) \cdot \left(-5400 \underline{k} \right) = 0$ $= \lambda_{ab} \cdot \left(\overline{\gamma}_{AE} \times \overline{T}_{EQ} + 1800 \right) = 0$ $= \lambda_{ab} \cdot \left(\overline{\gamma}_{AE} \times \overline{T}_{EQ} + 1800 \right) = 0$ $= \overline{\lambda}_{ab} \cdot \left(\overline{\gamma}_{AE} \times \overline{T}_{EQ} + 1800 \right) = 0$ $= \overline{\lambda}_{ab} \cdot \left(\overline{\gamma}_{AE} \times \overline{T}_{EQ} + 1800 \right) = 0$ $= \overline{\lambda}_{ab} \cdot \left(\overline{\gamma}_{AE} \times \overline{T}_{EQ} + 1800 \right) = 0$ $= \overline{\lambda}_{ab} \cdot \left(\overline{\gamma}_{AE} \times \overline{T}_{EQ} + 1800 \right) = 0$ $= \overline{\lambda}_{ab} \cdot \left(\overline{\gamma}_{AE} \times \overline{T}_{EQ} + 1800 \right) = -1800$ $T \overline{\lambda}_{EQ} \cdot \left(\frac{2}{3} \underline{i} + \frac{2}{3} \underline{j} - \frac{1}{3} \underline{k} \right) \times \left(6 \underline{i} \pm 12 \underline{j} \right) = -1800$ $T \overline{\lambda}_{EQ} \cdot \left(\frac{1}{2} \underline{j} - \frac{1}{3} \underline{k} \right) \times \left(6 \underline{i} \pm 12 \underline{j} \right) = -1800$ $T \overline{\lambda}_{EQ} \cdot \left(\frac{1}{2} \underline{j} - \frac{1}{3} \underline{k} \right) = -1800$ $T \overline{\lambda}_{EQ} \cdot \left(\frac{4}{2} \underline{i} - 2 \underline{j} + 4 \underline{k} \right) = -1800$ $= \overline{\lambda}_{AD} \cdot \left(\frac{4}{2} \underline{i} - 2 \underline{j} + 4 \underline{k} \right) = -1800$ $= \overline{\lambda}_{AD} \cdot \left(\frac{4}{2} \underline{i} - 2 \underline{j} + 4 \underline{k} \right) = -1800$ $= \overline{\lambda}_{AD} \cdot \left(\frac{4}{2} \underline{i} - 2 \underline{j} + 4 \underline{k} \right) = -1800$ $= \overline{\lambda}_{AD} \cdot \left(\frac{4}{2} \underline{i} - 2 \underline{j} + 4 \underline{k} \right) = -1800$ $= \overline{\lambda}_{AD} \cdot \left(\frac{4}{2} \underline{i} - 2 \underline{j} + 4 \underline{k} \right) = -1800$ $= \overline{\lambda}_{AD} \cdot \left(\frac{4}{2} \underline{i} - 2 \underline{j} + 4 \underline{k} \right) = -1800$

CE297-FA09-Ch4 Page 13

i.e. we can express

$$\overrightarrow{EG} = C\left(4\underline{i} - 2\underline{j} + 4\underline{k}\right) \qquad \begin{cases} \text{for some} \\ \text{inknown } C \end{cases}$$

$$\Rightarrow (\pi - 6) \underline{i} + (y - 12)\underline{j}^{-6} \underline{k} = C\left(4\underline{i} - 2\underline{j} + 4\underline{k}\right)$$
Equating 'k'' components : $-6 = C4 \Rightarrow C = -3/2$.

$$\Rightarrow \pi - 6 = (-3/2) 4 \Rightarrow \pi = 0$$

$$y - 12 = (-3/2)(-2) \Rightarrow y = 15 \text{ ft}$$

$$\Rightarrow \text{From}(1) \quad T\left(\frac{-6\underline{i} + 3\underline{j} - 6\underline{k}}{\sqrt{81}}\right) \cdot \left(4\underline{i} - 2\underline{j} + 4\underline{k}\right) = -1800$$

$$\Rightarrow \quad T\left(\frac{-54}{9}\right) = -1800 \Rightarrow \text{T} = 300 \text{ lb}$$