Determination STALL SPEED and Cmax experiment #1 Data Card

- 1. Observe the characteristics at the stall at different c.g. positions, configurations, and power settings.
 - Determine the warning speeds and stall speeds as above.
 - Observe flow sepalation patterns.

Instrumentation

- .. Airspeed and altimeter calibrated for instrument and position errors.
- Angle of attack (a) meter. < From GIST Shatton
 - Wing buffs.

Flight Test Techniques

The aircraft is stabilized at approximately 1.5 times the stalling speed in the configuration to be tested. All forces are trimmed out. Then, using pitch alone, the aircraft speed is reduced at 1 kt/sec until the aircraft reaches the stall. The planned configurations are:

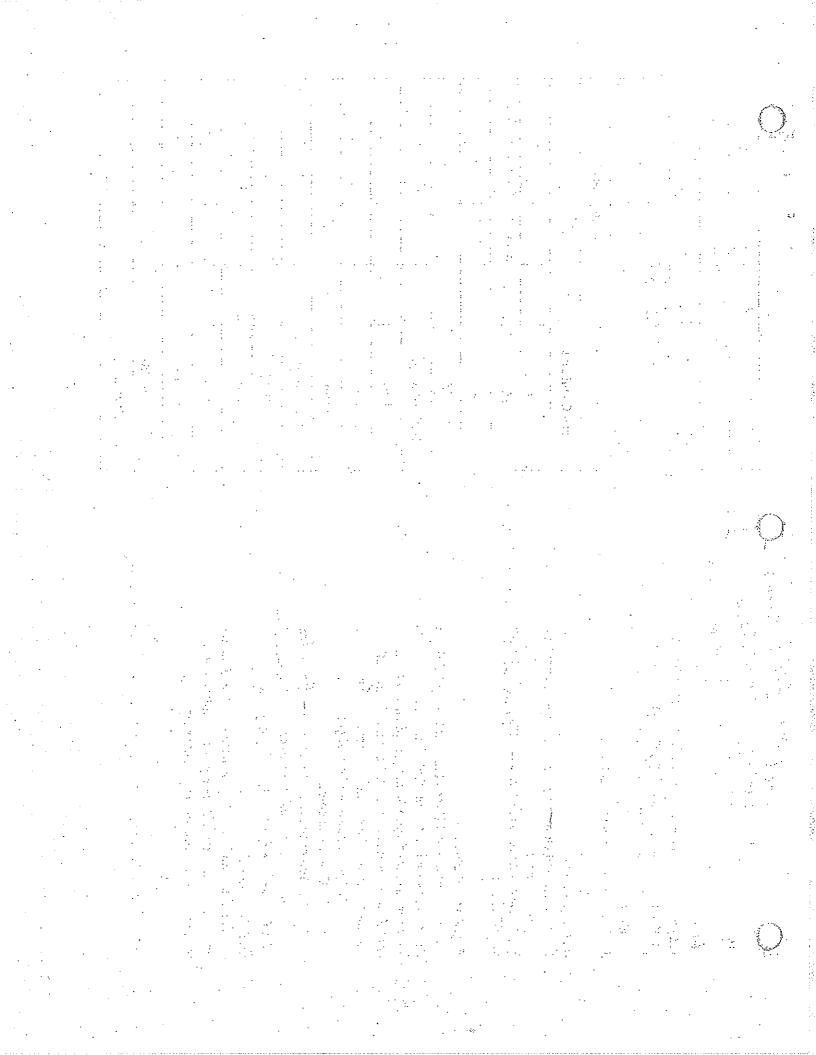
- 1. Clean, power for level flight.
 - 2. Clean, idle power.
- 3. Approach flaps, idle power. 1/2 Flaps
- 4. Landing flaps, idle power. FULL FL 29.92 in Hg. set altimeter

Flow Visualization

configuration will be done for data. Then each stall will be repeated to allow students stall over the wing. to see the propagation of the The first stall in each

Do two configurations

Data Card Aircraft: Councilination Zero fuel weight: 3 7 7 2 β ξ c.g: Pitot-static system: Councinguration Trim Conditions 1 2 3 4 P, Councinguration M.P. or torque 1 2 3 4 M.P. or torque 1 2 5 <th></th> <th>Stall Flight</th> <th>light</th> <th></th> <th></th>		Stall Flight	light		
### Date: 3772 bf Console: Configuration Configuration		Data (ard		
3772 bf cg: Console: Configuration tions	Aircraft:		-	Date;	
Configuration tions 1 2 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	10	7	£	:8 :8	
Configuration 5000 5000 5000	Pitot-static system:		-	Console:	
2000 5000 5000			Config	uration	
coos coos	Trim Conditions	1	2	8	4
0005 0005	V_i				
	H_{l}	0005	2000	5,000	5000
	W				
	RPM				
	M.P. or torque				
	flaps		·		
Data V_i (warning) V_i (stall) α (stall) $\Delta \phi$ (bank) $\Delta \psi$ (heading) H_i (recovery)	gear				
V_i (warning) V_i (stall) H_i (stall) α (stall) α (stall) $\Delta \phi$ (bank) $\Delta \psi$ (heading) $A\psi$ (heading)	Data				
P_i (stall) A_i (stall) A_j (stall) A_j (bank) A_j (heading) A_j (recovery)	V, (warning)				
H_i (stall) α (stall) $\Delta \phi$ (bank) $\Delta \psi$ (heading) H_i (recovery)	V, (stall)				
α (stall) $\Delta \phi$ (bank) $\Delta \psi$ (heading) H_i (recovery)	H_i (stall)				
$\Delta \phi$ (bank) $\Delta \psi$ (heading) H_i (recovery)	α (stall)				
$\Delta \psi$ (heading) H_i (recovery)	Δφ (bank)				
H, (recovery)	Δψ (heading)				
	H_i (recovery)				



			Stall Flight	light	
			Data Reduction	duction	
	H, (ft)				
7	V, (kts)				
ε.	ΔV_{tc} (kts)				
4	ΔV_{po} (kts)				
5.	ΔV_{c} (kts)				
9	V, (kts)				·
7	W, (lbs)				
∞.	$C_{L,max}$,
6	$V_{\rm S1}$ (kts)				
10	V, (kts)				
11	ΔV_{lc} (kts)				
12	ΔV_{pc} (kts)				-
13	ΔV_c (kts)				
14	V. (kts)				
15	V_{wam} (kts)	· /			
16	ΔV (kts)				
17	α (μΑ)				
18	α (degree)				

See Experiment #1 handout for a MATLAB script that implements thus data reduction,

Stall Flight Data Reduction

- H_{ℓ} (ft) Indicated pressure altitude.
- V_i (kts) Indicated stall airspeed.
- ΔV_{ie} (kts) Airspeed instrument error correction.
- ΔV_{pc} (kts) Airspeed position error correction.
- ΔV_c (kts) Scale altitude error correction (approximately 0 below 250 kts, below 10,000 ft)
- V_c (kts) Equivalent airspeed: [2] + [3] + [4] + [5].
- W_i (lbs) Test weight = zero fuel weight + fuel weight
- Stall lift coefficient = $\frac{2W}{\rho_0 V_e^2 S} = \frac{2[7]}{.002377([6] \times 1.689)^2 S}$ where S is the wing area.
- 9. V_{S1} (kts) Stall speed corrected for weight = $V_e \sqrt{\frac{W_S}{W_t}} = [6] \sqrt{\frac{W_S}{[7]}}$
- 10. V_i (kts) Indicated stall warning airspeed (buffet, horn, light)

where W_s is the standard weight

- 11. ΔV_{ic} (kts) Airspeed instrument error correction.
- 12. $\Delta V_{\rho\sigma}$ (kts) Airspeed position error correction.
- 13. ΔV_c (kts) Scale altitude error correction (approximately 0 below 250 kts, below 10,000 ft)
- 14. V_e (kts) Equivalent airspeed: [10] + [11] + [12] + [13].
- 15. V_{worm} (kts) Warning speed corrected for weight = $V_e \sqrt{\frac{W_s}{W_t}} = [14] \sqrt{\frac{W_s}{[7]}}$ where W_s is the standard weight
- 16. ΔV (kts) Stall warning = $V_{mem} V_{S1} = [15] [9]$
- 7. α (μA) Indicated α at stall
- α (deg) Stall α converted to degrees (use aircraft calibration book)

Stall Flight

Data Analysis

- 1. Does aircraft have adequate stall warning for each configuration?
- Are stall speed warning results repeatable or do you require. more data to obtain statistical confidence?
- How does stall a change with configuration?
- baseline value, how does $C_{L_{\max}}$ change with configuration? Using $C_{L_{\max}}$ in the clean/idle power configuration as the
 - Does aircraft meet FARs for heading change in a stall?
 - Does aircraft meet FARs for bank change in a stall?
 - 7. Does aircraft lose more than 100 feet in a stall?
- Are above results dependent of pilot technique?

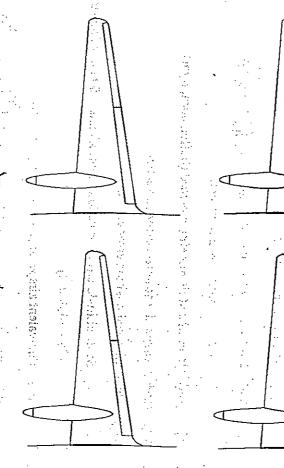
Airflow Separation Analysis



How does power effect the pattern?

Which appears to be most benign? Most adverse? . How does the flap setting effect the pattern?

Is separation sudden? How does it correlate to buffer





Experiment #1 Continued Error Analysis

You are to perform the error analysis for the computation of CLmax. To do this you need to use the provided error analysis software (see course web site) and to write a MATLAB function that returns a scalar CLmax.

Error analysis software has been provided to you at the course web site.

http://roger.ecn.purdue.edu/~andrisan/Courses/AAE490A_S2003/Index.html

Note that CLmax is computed in this experiment from only 5 input quantities, Hi, Vi, Wt, flap and wing area. So we can build a vector of inputs x as follows:

x(1)=Hi(j)	Indicated altitude, feet
x(2)=Vi(j	Indicated airspeed at stall, knots
x(3)=Wt(j)	Weight, pounds
x(4)=flap(j)	Flap setting flap=0 for no flap %flap=0.5
	for half flap %flap=1 for full flap
x(5)=S	Wing area, ft ² .

You will need to compute the error analysis for j=1 to the length of Hi. If your flight experiment involved flying three cases, then Hi, Vi, Ht and flap will be vectors of length three (j=1,2,3).

Unfortunately, the measured values of the first four of there these quantities are all slightly in error. These errors mean that the computed values for maximum lift coefficient will also be in error.

You need to write a MATLAB script to study the relationship between the errors in the five inputs (Hi, Vi, Wt, flap, and S) and the error in the output (CLmax).

First you need to define the array of errors

```
error=[100, 1, 100, .0001, .00001]
```

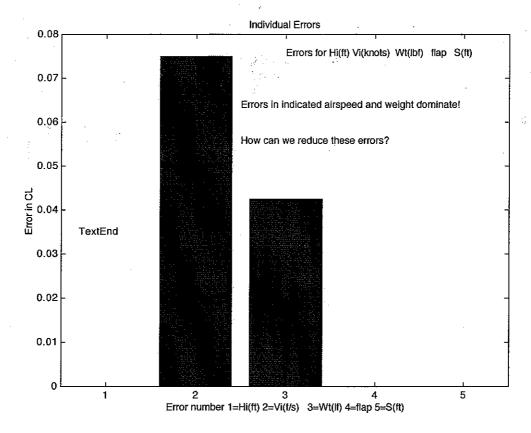
These are the assumed errors in Hi, Vi, Wt, flap, and S. Units are feet, knots, pounds, non-dimensional, square feet. Note that the errors in flap and S are deliberately quite small since we actually know them quite well.

If your flight experiment had three different cases, then you will need to generate a table of error analysis results of the following form.

	Error Anal	ysis		
	Data Reduc	tion		
1	Error in Hi(ft)	100.0	100.0	100.0
2	Error in Vi(kts)	1.0	1.0	1.0
3	Error in Wt(lbf)	100.0	100.0	100.0
4	Abs Err in CLmax	0.11	0.11	0.12
5	Rss Err in CLmax	0.08	0.08	0.09

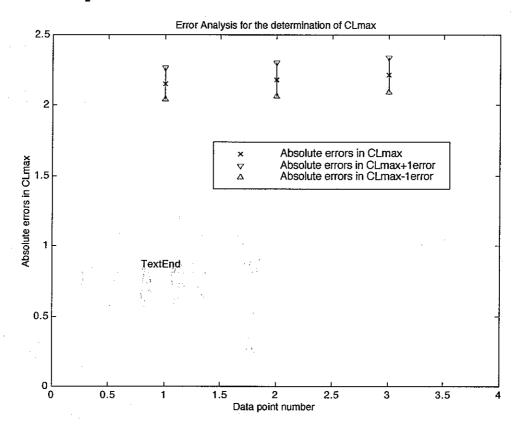
This table shows the results of using the provided software to compute the absolute and rss errors in the computation of CLmax.

Using the provided software, you need to generate a bar chart showing the individual errors from the five input quantities (Hi, Vi, Wt, flap, and S). An example is shown below.

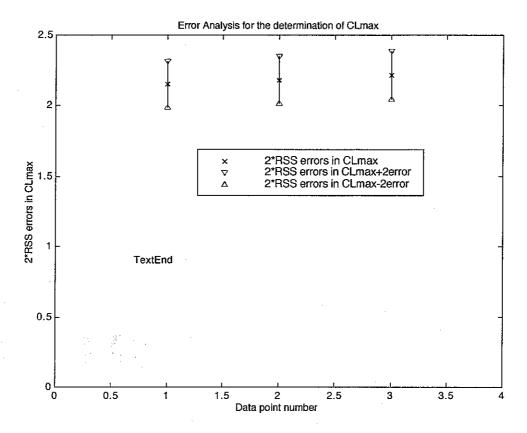


Please interpret these results. Do errors in altitude affect the accuracy of our determination of CLmax? What factors most affect the accuracy of our determination of CLmax?

You need also to plot CLmax that you determined for each of the cases you flew and plot them as shown below. Put the error bounds on the figure to indicate graphically how accurately you have computed CLmax. Do this under the assumption that the errors specified above are to be interpreted as absolute errors and again if the errors are to be interpreted as rss errors.



Shown below are the computed values of CLmax under the assumption that the errors are rss errors. The error bars reflect +- 2 times the rss errors.



In your opinion which error model is the most appropriate to use, the absolute error model or the rss error model? Why?

MATLAB SCRIPT TO PERRFORM THE FIRST PART OF THE EXPERIMENT DATA ANALYSIS (not including the error analysis)

The following script and the script MakeOutputTable can be found at the course web site.

http://roger.ecn.purdue.edu/%7Eandrisan/Courses/AAE490A_S2006/Buffer/Exp1/

```
% Experiment #1 Stall Speed and CLmax Determination
% Ref: NTPS, pages D24-D26.
% This MATLAB script computes stall airspeed and CLmax
% given Vindicated, flap setting, indicated geopotential pressure
altitude.
% It assumes standard outside air temperature for the calibrated
pressure altitude.
disp(' ')
disp('Start here')
disp('Experiment 1') %Example 1
disp(' ')
clear all
echo on
% List all inputs: Data Inputs
Hi=[4500,4100,4400] % Item 1 of the Table of Outputs: indicated
geopotential feet at stall. Put your data in this vector.
Vi= [61,60,59]
                          % Item 2: stall speed knots. Put your data in .:
this vector and the one below.
flap=[ 0, 0, 0]
                          % Flap setting %flap=0 for no flap %flap=0.5
for half flap %flap=1 for full flap
FuelWeight=[900,800,700] % Pounds (lbf).
Viwarn=[64,66,63]
                          % Item 10, indicated stall warning speed
knots.
                          % Pounds <<< Check this number. Use the
ZeroFuelWeight=4500
number Cèline gives you.
Ws=5500
                          % Pounds (lbf), standard weight is maximum
takeoff weight (Baron 58 manual p. 1-12)
S=199.2:
                          % Wing area, ft squared
% When you do your experiment you will replace this data with your
% All three vectors above must be of the same length.
% Compute stall speed and Clmax and build a Table of Outputs
% as called for in the Data Reduction section of the experiment.
% Item 1 in the Table of Outputs is indicated pressure altitude
% for the flight experiment and has been given above.
% Item 2 in the Table of Outputs is indicated stall airspeed
% for the flight experiment and has been given above.
% The following step is not listed in the NTPS Data Reduction
procedure,
% but we will do this in this and other experiments.
% We will use the function ALTBaron58 which performs two useful
% data corrections at once. It computes calibrated pressure altitude
% from indicated pressure altitude, indicated airspeed and flap
setting.
% In the process it determines the instrument corrections and
```

```
% static position error corrections. Unfortunately it does not
% return these two errors individually as is required for the Table of
Outputs,
% so we will have to do a few awkward steps to get data in the required
format
% for the Table of Outputs
help ALTBaron58
% Correct indicated altitude for instrument and position errors.
Hcalibrated=ALTBaron58(Hi, Vi, flap) % Altitude units are feet.
% Notice that we are using array operations to compute Hcalibrated,
% Hi and Vi are arrays and returned variable Hcalibrated is an array.
% For most computations done below we will use array operations.
% Items 3 and 4 are the individual corrections applied to
% airspeed measurements,
% dVic is the speed increment to add to indicated airspeed to
% correct for instrument error.
          Vic=Vi+dVic
% dVpc is the increment to add to airspeed to correct for
% static position error.
          Vcalibrated=Vic+dVpc
                     =Vi+dVic+dVpc
% Item 3 in the Table of Outputs: airspeed instrument correction (dVic)
% The Baron manual assumes that Vinstrumentcorrected (Vic) = Vindicated
(Vi)
% so dVic = 0
dVic=zeros(size(Vi)); % for Item 3
Vic=Vi+dVic; % sort of trivial since we assumed dVic=0
% Airspeed units are KNOTS.
% Item 4 in the Table of Outputs: airspeed position correction (dVpc)
% To do this we will use a function called AS1Baron58. This
% function corrects indicated airspeed for instrument error
% and static position error. Unfortunately it does not
% return these two errors individually, as is required for the Table of
% so we will have to do a few awkward steps to get data in the required
format.
help AS1Baron58
Vcalibrated=AS1Baron58(Vi,flap) % Airspeed units are KNOTS.
dVpc=Vcalibrated-Vic; % for Item 4. This is the awkward step.
% Airspeed units are KNOTS.
% Items 5 and 6 Compute dVc and equivalent airspeed
% dVc is the Scale Altitude Correction a.k.a. "Compressibility
Correction".
% Item 6a Get standard pressure (p, lbf/ft^2) for calibrated pressure
GeometricFlag=0 %Hvector is Geopotential altitude
```

[temp,p,rho,Hgeopvector]=atmosphere4(Hcalibrated,GeometricFlag);

```
p
% Item 6b Get equivalent airspeed (Vequivalent)
% To do this we will use the function AS2 to compute
```

% equivalent velocity from calibrated velocity and static pressure at the test

% condition. Unfortunately, this function does not return dVc, so we % will have to perform an awkward step to compute it.

help AS2

[Vequivalent,qcOverp0,qcOverp]=AS2(Vcalibrated,p); % for line 6, Knots dVc=Vequivalent-Vcalibrated; % for Item 5. This is the awkward step. Vequivalent % Airspeed units are KNOTS.

% Item 7 Compute test weights.
Wt=ZeroFuelWeight+FuelWeight % for Item 7 of the Table of Outputs

% Compute Item 8: CLmax

% To do this we will use two different methods.

% Item 8 done using equivalent airspeed (Vequivalent, knots)
rho0=0.00237691267925741; % Sea level density, slugs per cubic foot
Vefps=1.687808*Vequivalent % convert knots to ft/sec
Clmax=2*Wt./(rho0*Vefps.*Vefps*S) % for Item 9 of the Table of Outputs

- % Item 8 of the Table of Outputs done using true airspeed (Vtrue, knots)
- $\mbox{\ensuremath{\$}}$ In this calculation we assume standard temperature for the calibrated pressure altitude.
- % It would be better if we had measured outside air temperature, but we did not in this experiment.

temp %degree Rankine

- $\mbox{\ensuremath{\$}}$ To do this we use the function AS3. This function computes true airspeed
- $\ensuremath{\$}$ from equivalent airspeed, outside air temperature and calibrated altitude.

help AS3

[Vtrue,M,aknots,rho,sigma]=AS3(Vequivalent,temp,Hcalibrated); % knots Vtfps=1.687808*Vtrue % convert knots to ft/sec Clmax2=2*Wt./(rho.*Vtfps.*Vtfps*S) % Note that this is dene with array operations.

% Item 9 of the Table of Outputs: Stall speed corrected to the standard weight

Vs1=Vequivalent.*sqrt(Ws./Wt) % for Item 9 of the Table of Outputs,
knots

- 8 *****
- % Compute warning speed. To do this we reepeat all the airspeed calibration steps.
- % Item 10 Indicated airspeed at stall warning.
- % This was input above in the Data Inputs section of this script.
- % The following step is not listed in the NTPS Data Reduction

```
procedure,
% but we will do this in this and other experiments.
% Correct indicated altitude for instrument and position errors.
Hcalibratedwarn=ALTBaron58(Hi, Viwarn, flap)
% The Baron manual assumes that Vinstrumentcorrected (Vic) = Vindicated
(Vi)
% so dVic = 0
dVicwarn=zeros(size(Viwarn)); % forItem 11
Vicwarn=Viwarn+dVicwarn;
% Items 11 and 12 Correct for indicated airspeed for instrument,
position errors.
Vcalibratedwarn=AS1Baron58(Viwarn, flap) % Airspeed units are KNOTS.
dVpcwarn=Vcalibratedwarn-Vicwarn; % for Item 12
% Items 13 and 14 Compute equivalent airspeed
% Item 14a Get standard pressure (p, lbf/ft^2) for calibrated pressure.
altitude.
GeometricFlag=0 %Hcalibratedwarn is Geopotential altitude
[temp,pwarn,rho,Hgeopvector] = atmosphere4(Hcalibratedwarn,GeometricFlag)
pwarn
% Item 14b Get equivalent airspeed (Vequivalent)
[Vequivalentwarn,qcOverp0,qcOverp]=AS2(Vcalibratedwarn,pwarn); %Knots
Veguivalentwarn % for Item 14
dVcwarn=Veguivalentwarn-Vcalibratedwarn; % for Item 13
% Item 15 Warning speed corrected for weight
Vwarn=Vequivalentwarn.*sqrt(Ws./Wt) %for Item 15, knots
% Item 16 Stall warning
StallWarning=Vwarn-Vs1 % for Item 16, knots
% Now let's call a script that writes a formatted table
%to the command window in a pretty format. We use a script here simply
% cut down on the size of this main script (which is already too long).
echo off
MakeOutputTable
```

Results of running the script Expl.m

Start here Experiment 1

% List all inputs: Data Inputs

Hi=[4500,4100,4400] % Item 1 of the Table of Outputs: indicated geopotential feet at stall. Put your data in this vector.

Hi =

4500

4100

4400

Vi= [61,60,59] % Item 2: stall speed knots. Put your data in this vector and the one below.

Vi =

61 60 59

flap=[0, 0, 0] % Flap setting %flap=0 for no flap %flap=0.5 for half flap %flap=1 for full flap

flap =

0 0 0

FuelWeight=[900,800,700] % Pounds (lbf).

FuelWeight =

900 800 700

Viwarn=[64,66,63] % Item 10, indicated stall warning speed
knots.

Viwarn =

64 66 63

ZeroFuelWeight=4500 % Pounds <<< Check this number. Use the number Cvline gives you.

ZeroFuelWeight =

4500

Ws=5500 % Pounds (lbf), standard weight is maximum takeoff weight (Baron 58 manual p. 1-12)

Ws =

5500

S=199.2; % Wing area, ft squared % When you do your experiment you will replace this data with your data. % All three vectors above must be of the same length.

- % Compute stall speed and Clmax and build a Table of Outputs
- % as called for in the Data Reduction section of the experiment.
- % Item 1 in the Table of Outputs is indicated pressure altitude
- % for the flight experiment and has been given above.
- % Item 2 in the Table of Outputs is indicated stall airspeed
- % for the flight experiment and has been given above.
- % The following step is not listed in the NTPS Data Reduction procedure,
- % but we will do this in this and other experiments.
- % We will use the function ALTBaron58 which performs two useful
- % data corrections at once. It computes calibrated pressure altitude
- % from indicated pressure altitude, indicated airspeed and flap setting.
- % In the process it determines the instrument corrections and
- % static position error corrections. Unfortunately it does not
- $\mbox{\$}$ return these two errors individually as is required for the Table of Outputs,
- % so we will have to do a few awkward steps to get data in the required format
- % for the Table of Outputs

help ALTBaron58

function Hcalibrated=ALTBaron58(Hindicated, Vindicated, flap)

Correct indicated altitude for instrument error and static position error.

Data is extracted from Pilots Operating Handbook Baron 58, page 5-17 (Normal System).

It is assumed that the Beechcraft Baron 58 has zero instrument correction.

Therefore

Hinstrumentcorrected (Hic) = Hindicated (Hi)

Given below are the position error corrections to get Hcalibrated. They are a function of Hindicated, Vindicated, and flap position.

Hcalibrated=f(Hindicated, Vindicated, flap)

Hindicated is indicated pressure altitude in geopotential feet. Healibrated is calibrated pressure altitude in geopotential feet. Vindicated is indicated airspeed in knots.

flap=0 for no flap flap=0.5 for half flap flap=1 for full flap

For accuracy, Vindicated must be in the range 60-200 knots for the no flap case.

For accuracy, Vindicated must be in the range 60-130 knots for the full flap case.

For accuracy, Hindicated must be in the range 0-20000 ft for the no flap case.

For accuracy, Hindicated must be in the range 0-10000 ft for the full flap case.

Use of this function for the half flap case is somewhat questionable. This function uses the 2D table lookup function interp2.

% Correct indicated altitude for instrument and position errors. Hcalibrated=ALTBaron58(Hi,Vi,flap) % Altitude units are feet.

Hcalibrated =

4397.57666

```
% Notice that we are using array operations to compute Hcalibrated,
  % Hi and Vi are arrays and returned variable Hcalibrated is an array.
  % For most computations done below we will use array operations.
  % Items 3 and 4 are the individual corrections applied to
  % airspeed measurements,
  % dVic is the speed increment to add to indicated airspeed to
 % correct for instrument error.
            Vic=Vi+dVic
  % dVpc is the increment to add to airspeed to correct for
% static position error.
            Vcalibrated=Vic+dVpc
                       =Vi+dVic+dVpc
 % Item 3 in the Table of Outputs: airspeed instrument correction (dVic)
 % The Baron manual assumes that Vinstrumentcorrected (Vic) = Vindicated
 (Vi)
  % so dVic = 0
 dVic=zeros(size(Vi)); % for Item 3
  Vic=Vi+dVic; % sort of trivial since we assumed dVic=0
 % Airspeed units are KNOTS.
  % Item 4 in the Table of Outputs: airspeed position correction (dVpc)
 % To do this we will use a function called AS1Baron58. This
* % function corrects indicated airspeed for instrument error
  % and static position error. Unfortunately it does not
  % return these two errors individually, as is required for the Table of
  % so we will have to do a few awkward steps to get data in the required
format.
  help AS1Baron58
    function Vcalibrated=AS1Baron58(Vindicated,flap)
    Correct indicated airspeed for instrument error and static position
    Data is extracted from Pilots Operating Handbook Baron 58, page 5-16
  (Normal System).
    It is assumed that the Beechcraft Baron 58 has zero instrument
  correction.
    Therefore
                Vinstrumentcorrected (Vic) = Vindicated (Vi)
    Given below are the position error corrections to get Vcalibrated.
    They are a function of Vindicated and flap position.
                Vcalibrated=f(Vindicated,flap)
                      flap=0
                               for no flap
                      flap=0.5 for half flap
                      flap=1
                               for full flap
    Vindicated and Vcal are a row vectors.
    Half flap data is linearly interpolated between no flap and full flap
```

Vcalibrated=AS1Baron58(Vi,flap) % Airspeed units are KNOTS.

Vcalibrated =

Units are KNOTS.

dVpc=Vcalibrated-Vic; % for Item 4. This is the awkward step.
% Airspeed units are KNOTS.
% Items 5 and 6 Compute dVc and equivalent airspeed
% dVc is the Scale Altitude Correction a.k.a. "Compressibility Correction".
% Item 6a Get standard pressure (p, lbf/ft^2) for calibrated pressure altitude.
GeometricFlag=0 %Hvector is Geopotential altitude
GeometricFlag =
0

[temp,p,rho,Hgeopvector]=atmosphere4(Hcalibrated,GeometricFlag);
p

p =

1794.15802524556

1821.07726301237

1800.85576404759

- % Item 6b Get equivalent airspeed (Vequivalent)
- % To do this we will use the function AS2 to compute
- % equivalent velocity from calibrated velocity and static pressure at the test
- % condition. Unfortunately, this function does not return dVc, so we % will have to perform an awkward step to compute it. help AS2

function [Vequivalent,qcOverp0,qcOverp]=AS2(Vcalibrated,p)
Computes the Scale Altitude Correction a.k.a. "Compressibility
Correction"

Vcalibrated is calibrated velocity.

p is static pressure at which Vcalibrated is known.

Vcalibrated and p are row vectors.

Assumes Vcalibrated <=ao.

Units are knots and lbf/ft^2.

Theses equations are a slightly different version

of quantities in equation 2.15.2 in the book

"Flight Test Engineering" by Ward and Srtganac (page 13).

This function works for all different types of aircraft as long as Vcalibrated <=ao.

[Vequivalent,qcOverp0,qcOverp]=AS2(Vcalibrated,p); % for line 6, Knots dVc=Vequivalent-Vcalibrated; % for Item 5. This is the awkward step. Vequivalent % Airspeed units are KNOTS.

Vequivalent =

60.9883956985937

59.9900282280775

58.9897545503723

% Item 7 Compute test weights.
Wt=ZeroFuelWeight+FuelWeight % for Item 7 of the Table of Outputs

Wt =

5400

5300

5200

% Compute Item 8: CLmax

% To do this we will use two different methods.

% Item 8 done using equivalent airspeed (Vequivalent, knots)
rho0=0.00237691267925741; % Sea level density, slugs per cubic foot
Vefps=1.687808*Vequivalent % convert knots to ft/sec

Vefps =

102.936702167252

101.251649563575

99.5633796481548

Clmax=2*Wt./(rho0*Vefps.*Vefps*S) % for Item 9 of the Table of Outputs

Clmay =

2.15268603376695

2.18373074765527

2.2158048954023

- % Item 8 of the Table of Outputs done using true airspeed (Vtrue, knots)
- % In this calculation we assume standard temperature for the calibrated pressure altitude.
- % It would be better if we had measured outside air temperature, but we did not in this experiment. temp %degree Rankine

temp =

502.631076227417

504.057276519232

502.987538018174

- % To do this we use the function AS3. This function computes true airspeed
- % from equivalent airspeed, outside air temperature and calibrated altitude.

help AS3

function

[VtrueKnots,M,aknots,rho,sigma]=AS3(Vequivalent,TdegR,Hpcalibrated)
This function computes true arispeed from equivalent airspeed
and works for all different types of aircraft.
Hpcalibrated is calibrated pressure altitude (geopotential feet)

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TdegR is actual temperature in degR

Veguivalent is equivalent airspeed in knots.

Vtrue is true airspeed in knots.

M is mach number (nondimensional)

aknots is the speed of sound in knots

rho is actual air density (slugs/ft^3)

sigma=rho/rho0 nondimensional

[Vtrue,M,aknots,rho,sigma]=AS3(Vequivalent,temp,Hcalibrated); % knots Vtfps=1.687808*Vtrue % convert knots to ft/sec

Vtfps =

110.052373973644

107.60010827523

106.285402211383

Clmax2=2*Wt./(rho.*Vtfps.*Vtfps*S) % Note that this is dene with array
operations.

Clmax2 =

2.15268603376695

2.18373074765527

2.2158048954023

% Item 9 of the Table of Outputs: Stall speed corrected to the standard weight Vs1=Vequivalent.*sqrt(Ws./Wt) % for Item 9 of the Table of Outputs,

Vs1 =

knots

61.550512610895

61.1114342162578

60.6675228040291

8 *******

- % Compute warning speed. To do this we reepeat all the airspeed calibration steps.
- % Item 10 Indicated airspeed at stall warning.
- % This was input above in the Data Inputs section of this script.
- % The following step is not listed in the NTPS Data Reduction procedure,
- % but we will do this in this and other experiments.
- % Correct indicated altitude for instrument and position errors.
 Hcalibratedwarn=ALTBaron58(Hi,Viwarn,flap)

Hcalibratedwarn =

4497.43439548361

4097,41522249815

4397.4783755843

% The Baron manual assumes that Vinstrumentcorrected (Vic) = Vindicated
(Vi)

% so dVic = 0

dVicwarn=zeros(size(Viwarn)); % forItem 11
Vicwarn=Viwarn+dVicwarn;

 $\mbox{\$}$ Items 11 and 12 Correct for indicated airspeed for instrument, position errors.

Vcalibratedwarn=AS1Baron58(Viwarn,flap) % Airspeed units are KNOTS.

Vcalibratedwarn = 64 66 63 dVpcwarn=Vcalibratedwarn-Vicwarn; % for Item 12 % Items 13 and 14 Compute equivalent airspeed % Item 14a Get standard pressure (p, lbf/ft^2) for calibrated pressure GeometricFlag=0 %Hcalibratedwarn is Geopotential altitude GeometricFlag = 0 [temp,pwarn,rho,Hgeopvector]=atmosphere4(Hcalibratedwarn,GeometricFlag) pwarn pwarn = 1794.16465036291 1821.09027436524 1800.86235967757 % Item 14b Get equivalent airspeed (Vequivalent) [Vequivalentwarn,qcOverp0,qcOverp]=AS2(Vcalibratedwarn,pwarn); %Knots Vequivalentwarn % for Item 14 Vequivalentwarn = 63.9866024589078 65.986736356799 62.9875315476322 dVcwarn=Vequivalentwarn-Vcalibratedwarn; % for Item 13 % Item 15 Warning speed corrected for weight Vwarn=Vequivalentwarn.*sqrt(Ws./Wt) %for Item 15, knots Vwarn = 64.5763531974026 67.2202400486068 64.7790033313736 % Item 16 Stall warning StallWarning=Vwarn-Vs1 % for Item 16, knots

StallWarning =

3.02584058650753

6.10880583234901

4.11148052734453

echo off

% Now let's call a script that writes a formatted table %to the command window in a pretty format. We use a script here simply % cut down on the size of this main script (which is already too long).

Stall Flight Data Data Reduction

	Data	Reduction		
1	Hi(ft)	4500.0	4100.0	4400.0
2	Vi(kts)	61.0	60.0	59.0
3	dVic(kts)	0.0	0.0	0.0
4 5	dVpc(kts)	0.0	0.0	0.0
5	dVc(kts)	-0.0	-0.0	-0.0
6	Ve(kts)	61.0	60.0	59.0
7	Wt(lbf)	5400.0	5300.0	5200.0
8	CLmax	2.2	2.2	2.2
9	Vsl(kts)	61.6	61.1	60.7
10	Vi(kts)	64.0	66.0	63.0
11	dVic(kts)	0.0	0.0	0.0
12	dVpc(kts)	0.0	0.0	0.0
13	dVc(kts)	-0.0	-0.0	-0.0
14	Ve(kts)	64.0	66.0	63.0
15	Vwrn(kts)	64.6	67.2	64.8
16	dV(kts)	3.0	6.1	4.1
17	ignore			
18	ignore			