

$$6.5-6 \quad P_d = \frac{1}{4} 190 \text{ k} = 47.5 \text{ k}$$

$$P_l = \frac{3}{4} 190 \text{ k} = 142.5 \text{ k}$$

$$M_{d, \text{Top}} = \frac{1}{4} 80 \text{ k-ft} = 20 \text{ k-ft}$$

$$M_{l, \text{Top}} = \frac{3}{4} 80 \text{ k-ft} = 60 \text{ k-ft}$$

$$M_{d, \text{Bot}} = \frac{1}{4} 75 \text{ k-ft} = 18.75 \text{ k-ft}$$

$$M_{l, \text{Bot}} = \frac{3}{4} 75 \text{ k-ft} = 56.25 \text{ k-ft}$$

$$P_{nt} = 1.2 D + 1.6 L = 1.2 (47.5) + 1.6 (142.5) = 285 \text{ k}$$

$$M_{nt, \text{Top}} = 1.2 D + 1.6 L = 1.2 (20) + 1.6 (60) = 120 \text{ k-ft}$$

$$M_{nt, \text{Bot}} = 1.2 D + 1.6 L = 1.2 (18.75) + 1.6 (56.25) = 112.5 \text{ k-ft}$$

Find B_1

$$B_1 = \frac{C_m}{1 - \alpha P_r / P_{e1}} = \frac{0.225}{1 - (1.0) \frac{285 \text{ k}}{3012.4 \text{ k}}} = 0.249 \leq 1.0 \quad \text{Use } B_1 = 1.0$$

$$\text{where } C_m = 0.6 - 0.4 \left(\frac{112.5}{120} \right) = 0.225$$

$$\alpha = (1.0)$$

$$P_r = P_{nt} = 285 \text{ k}$$

$$P_{e1} = \frac{\pi^2 E I_x}{(K L)^2} = \frac{\pi^2 (29000 \text{ ksi})(341 \text{ in}^4)}{(15 \cdot 12 \text{ in})^2} = 3012.4 \text{ k}$$

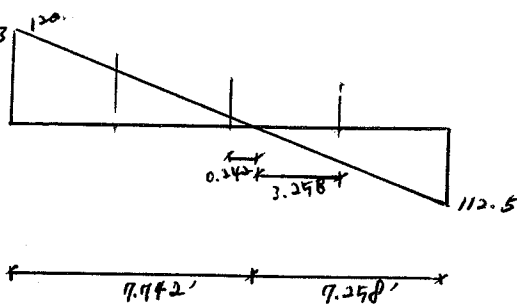
Find $\phi_c P_n$, $\phi_b M_n$

W 10 x 60

$$\phi_c P_n = 554 \text{ k}$$

$$+ \phi_b M_n = 257.25 \text{ k-ft} \rightarrow C_B = 1.0$$

Find C_B



$$M_{max} = 120 \text{ k-ft}$$

$$M_A = 120 \frac{3.992}{7.742} = 61.87 \text{ k-ft}$$

$$M_B = 120 \frac{0.242}{7.742} = 3.75 \text{ k-ft}$$

$$M_C = +112.5 \frac{3.258}{7.258} = 650.5 \text{ k-ft}$$

$$C_b = \frac{12.5 M_{max}}{2.5 M_{max} + 3 M_A + 4 M_B + 3 M_C} = \frac{12.5 (120)}{2.5 (120) + 3 (61.87) + 4 (3.75) + 3 (150.5)}$$

$$= \frac{2.3}{\cancel{4.29}} \leq 3.0$$

$$\rightarrow C_b = 2.3$$

Find $\phi_b M_n$

$$\phi_b M_n = C_b (\phi_b M_n)_{C_b=1.0} \leq \phi_b M_p$$

$$= (2.3)(257.25) = \cancel{28} \frac{591.7}{591.7} \text{ k-ft} \leq 280 \text{ k-ft}$$

$$\rightarrow \phi_b M_n = 280 \text{ k-ft}$$

Check Interaction Equation

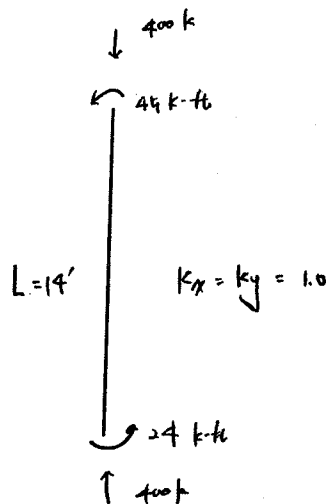
$$\frac{P_r}{P_c} = \frac{285 \text{ k}}{535 \text{ k}} = 0.5185 \geq 0.2 \quad \text{Use H1-1 a}$$

$$\frac{P_r}{P_c} + \frac{8}{9} \left(\frac{M_{rx}}{M_{cx}} + \frac{M_{ry}}{M_{cy}} \right)$$

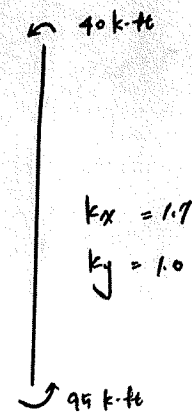
$$= 0.5185 + \frac{8}{9} \left(\frac{120 \text{ k-ft}}{280 \text{ k-ft}} \right) = 0.894 \leq 1.0 \quad \text{o.k.}$$

$\rightarrow$ The member is adequate.

6.6-1



Nonsway



Sway

Determine the critical axis for axial compressive strength:

$$K_y L = 14 \text{ ft}$$

$$\frac{K_x L}{r_x / r_y} = \frac{(1.7)(14')}{2.44} = 9.79' < 14 \text{ ft} \rightarrow KL = 14'$$

From the column load tables, $KL = 14'$, $\phi_c P_n = 1774 \text{ kips}$

Find B_1

$$C_m = 0.6 - 0.4 \left(\frac{M_1}{M_2} \right) = 0.6 - 0.4 \left(\frac{24}{45} \right) = 0.387$$

$$P_{e1} = \frac{\pi^2 EI}{(KL)^2} = \frac{\pi^2 (29000 \text{ ksi})(88 \text{ in}^2)}{(14.12)^2} = 8934.2 \text{ k}$$

$$B_1 = \frac{C_m}{1 - (P_r / P_{e1})} = \frac{0.387}{1 - (400 \text{ k} / 8934.2)} = 0.405 < 1.0$$

$$\rightarrow B_1 = 1.0$$

Find B_2

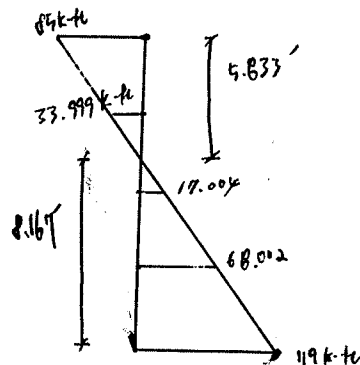
$$B_2 = \frac{1}{1 - \frac{\sum P_{nt}}{\sum P_{e2}}} = \frac{1}{1 - \frac{6000 \text{ k}}{40000 \text{ k}}} = 1.176$$

Find M_r

$$M_r = \beta_1 M_{nt} + \beta_2 M_{lt} \\ = (1.0)(240) + 1.176(95 \text{ k}\cdot\text{ft}) = 135.72 \text{ k}\cdot\text{ft}$$

Find $\phi_c M_n$

$$C_b = \frac{12.5 M_{\max}}{2.5 M_{\max} + 3 M_A + 4 M_B + 3 M_C} = \frac{12.5(119)}{2.5(119) + 3(33.999) + 4(19.004) + 3(68.002)} = 2.215$$



From table 3-10 $\phi_b M_n_{c_b=1} = 477 \text{ k}\cdot\text{ft}$

3-6 $\phi_b M_p = 521 \text{ k}\cdot\text{ft}$

$$\phi_b M_n = (\phi_b M_n_{c_b=1}) C_b \leq \phi_b M_p \\ = (477)(2.215) = 1056.6 \text{ k}\cdot\text{ft} \leq 521 \text{ k}\cdot\text{ft}$$

$$\phi_b M_n = 521 \text{ k}\cdot\text{ft}$$

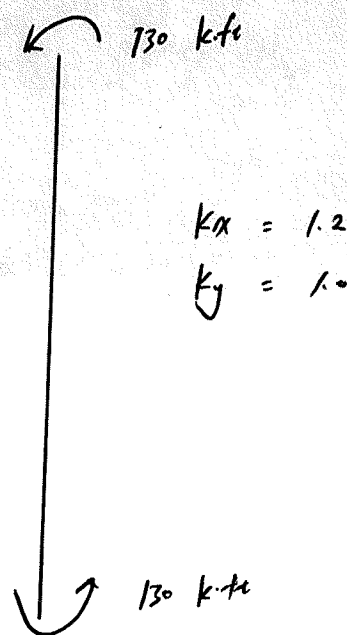
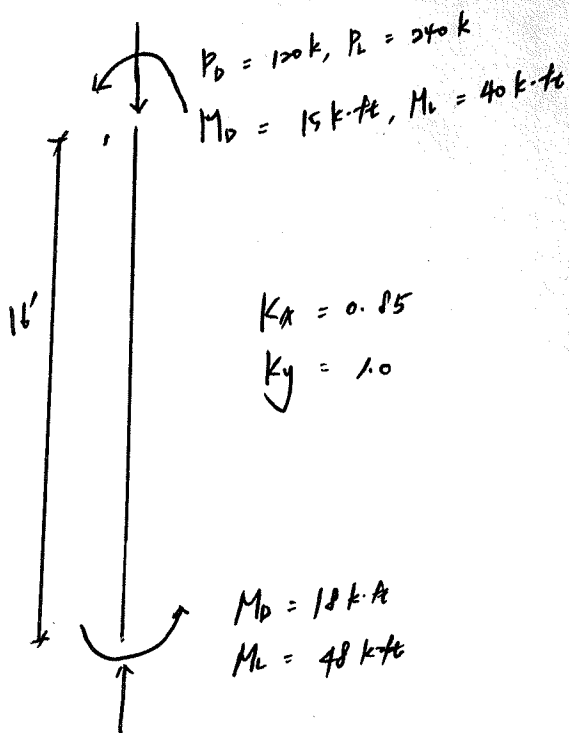
Check Interaction equation

$$\frac{P_r}{P_c} = \frac{400 \text{ k}}{774 \text{ k}} = 0.516 > 0.2 \quad \text{Use H1-1a}$$

$$\frac{P_r}{P_c} + \frac{8}{9} \left(\frac{M_{rx}}{M_{cx}} \right) = 0.516 + \frac{8}{9} \left(\frac{135.72 \text{ k}\cdot\text{ft}}{521 \text{ k}\cdot\text{ft}} \right) \\ = 0.748 \leq 1.0 \quad \text{O.K.}$$

Thus, the member satisfies the provisions of the AISC.

6.6-2



Load Case 1 : $1.2D + 1.6L$

The critical axis for axial compressive strength

$$K_y L = 16'$$

$$\frac{K_x L}{r_x/r_y} = \frac{(0.85)(16')}{2.44} = 5.57'$$

$$= \frac{(1.2)(16')}{2.44} = 10.26' \rightarrow K_L = 16'$$

$\phi_c P_n$

From table $\phi_c P_n = 628 \text{ kips}$, $K_L = 16'$
 $528 \text{ k} = 1.2D + 1.6L$

$82 \text{ k-ft} = 1.2D + 1.6L$

98.4 k-ft

$$C_m = 0.6 - 0.4 \left(\frac{82}{98.4} \right) = 0.267$$

Find B_1

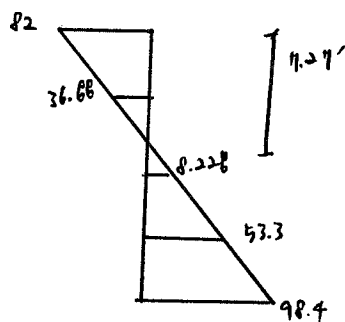
$$B_1 = \frac{C_m}{1 - (P_r/P_{el})} = \frac{0.267}{1 - (528k/9467k)} = 0.27 \leq 1.0 \rightarrow B_1 = 1.0$$

$$P_{el} = \frac{\pi^2 EI}{(KL)^2} = \frac{\pi^2 (29000 \text{ ksi}) (881 \text{ in}^4)}{(0.85 \times 16 \times 12)^2} = 9467 \text{ k}$$

$$M_{1z} = 0 \rightarrow B_2 = 0$$

Find M_r

$$\begin{aligned} M_r &= B_1 M_{1z} + B_2 M_{1z} \\ &= (1.0)(98.4) + 0 \\ &= 98.4 \text{ k-ft} \end{aligned}$$

Find C_b 

$$\begin{aligned} C_b &= \frac{12.5 M_{max}}{2.5 M_{max} + 3M_1 + 4M_2 + 3M_3} \\ &= \frac{12.5 (98.4)}{2.5 (98.4) + 3(36.66) + 4(8.228) + 3(53.3)} \\ &= 2.24 \end{aligned}$$

Find $\phi_b M_n$

$$\phi_b M_n, C_b = 1.0 \quad \text{from table 3-10} \quad 462 \text{ k-ft}$$

$$\phi_b M_p \quad \text{from table 3-6} \quad 521 \text{ k-ft}$$

$$\begin{aligned} \phi_b M_n, C_b = 2.24 &= (2.24)(462 \text{ k-ft}) \leq 521 \text{ k-ft} \\ &= 1034 \text{ k-ft} \leq 521 \text{ k-ft} \end{aligned}$$

$$\phi_b M_n = 521 \text{ k-ft}$$

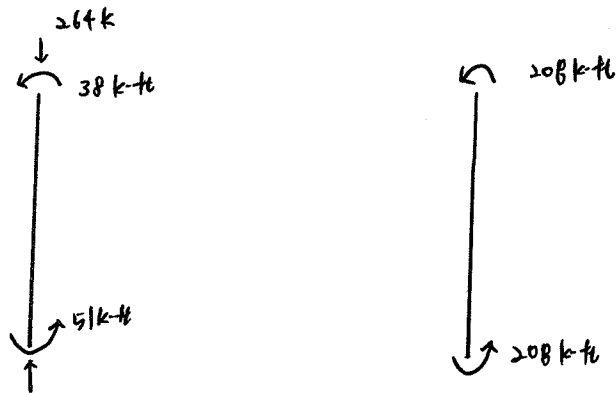
Check Interaction equation

$$\frac{P_r}{P_c} = \frac{528k}{261k} = 0.796 \geq 0.2$$

Use H1-1 a

$$\frac{P_r}{P_c} + \frac{8}{9} \left(\frac{M_{rx}}{M_{cx}} \right) = \frac{0.756}{\cancel{0.57}} + \frac{8}{9} \left(\frac{98.4}{521} \right) = \frac{0.924}{\cancel{0.57}} < 1.0 \quad o.k$$

Load Case 2 : 1.2D + 0.5L + 1.6W



$$C_m = 0.6 - 0.4 \left(\frac{38}{51} \right) = 0.302$$

$$P_{e1} = 9467 \text{ k}$$

$$\beta_1 = \frac{C_m}{1 - P_r/P_{e1}} = \frac{0.302}{1 - 264/9467} = 0.31 < 1.0 \rightarrow \beta_1 = 1.0$$

$$\beta_2 \approx \frac{1}{1 - (P_u/P_{e2})} = \frac{1}{1 - \left(\frac{264}{4750.17} \right)} = 1.06$$

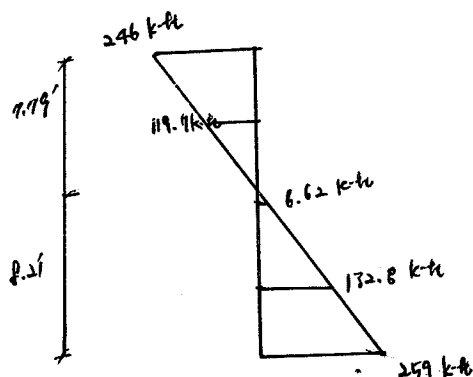
$$\text{where } P_u = 264 \text{ k}$$

$$P_{e2} = \frac{\pi^2 EI}{(K_x L)^2} = \frac{\pi^2 (29000 \text{ ksi})(88 \text{ in}^2)}{(12 \cdot 16 \cdot 12)^2} = 4750.17 \text{ k}$$

$$M_r = \beta_1 M_{nt} + \beta_2 M_{lt}$$

$$= (1.0)(51 \text{ k-ft}) + 1.06(208 \text{ k-ft}) = 271.5 \text{ k-ft}$$

Find C_b



$$C_b = \frac{12.5 M_{max}}{2.5 M_{max} + 3 M_A + 4 M_B + 3 M_C}$$

$$= \frac{12.5(259)}{2.5(259) + 3(119.9) + 4(6.62) + 3(132.8)} = 2.26$$

Find $\phi_b M_n$

$$C_b_{1.2D+1.6L} \approx C_b_{1.2D+0.5L+1.6W}$$

$$\rightarrow \phi_b M_n = 521 \text{ k-ft}$$

Check Interaction equation

$$\frac{P_r}{P_c} = \frac{264 \text{ k}}{698 \text{ k}} = 0.38 \geq 0.2 \quad \text{Use H1-1 a}$$

$$\frac{P_r}{P_c} + \frac{8}{9} \left(\frac{M_{rx}}{M_{cx}} \right) = 0.38 + \frac{8}{9} \left(\frac{271.5}{521} \right) = 0.841 \leq 1.0 \quad \text{O.K.}$$

→ The member is in compliance with the AISC spec.