

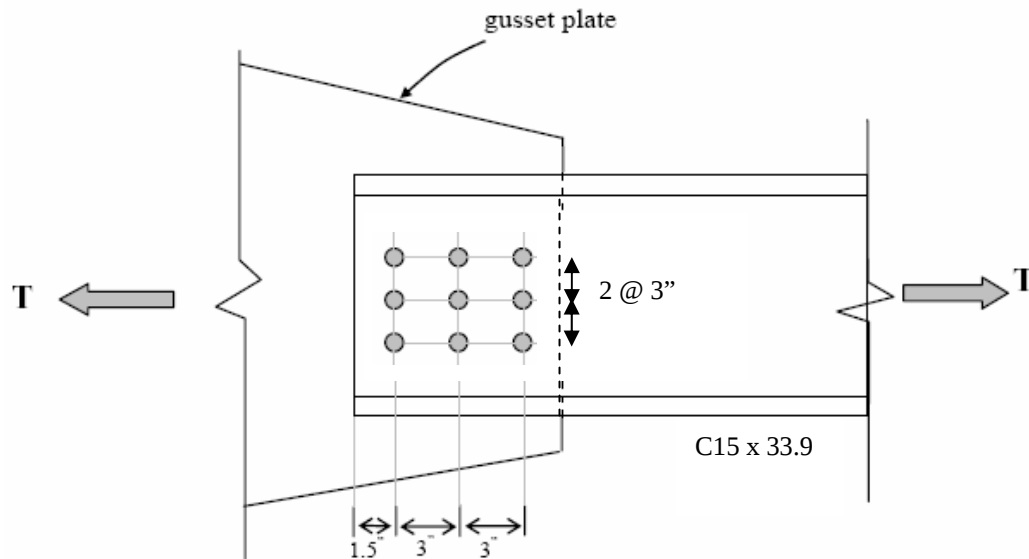
Solution to Homework 4:

In Class Problem:

Given:

Channel section: C15x33.9

A36 Steel: $F_y = 36$ ksi, $F_u = 65$ ksi



Required: Determine the design tensile strength.

Step 1: Limit state of yielding due to tension

$$\phi T_n = 0.9 A_g F_y = 0.9 * 9.96 * 36 = 322.7 \text{ kips}$$

Step 2: Limit state of fracture due to tension

$$A_n = A_g - n d_e t = 9.96 - 3(7/8)(0.4) = 8.91 \text{ in}^2$$

$$U = 1 - (x / L) = 1 - 0.787 / 6 = 0.87 > 0.9 \text{ (ok)}$$

$$A_e = U A_n = 0.87 * 8.91 = 7.75 \text{ in}^2$$

$$\phi T_n = 0.75 A_e F_u = 0.75 * 7.75 * 65 = 375.9 \text{ kips}$$

Step 3: Limit state of block shear rupture

$$A_{gv} = 2*(7.5*0.4) = 6.0 \text{ in}^2$$

$$A_{nv} = 2*(7.5 - 2.5*7/8)*0.4 = 4.25 \text{ in}^2$$

$$A_{gt} = (6*0.4) = 2.4 \text{ in}^2$$

$$A_{nt} = 2.4 - 2*0.4*(7/8) = 1.7 \text{ in}^2$$

$$F_u A_{nt} = 58*1.7 = 98.6 \text{ kips}$$

$$0.6F_u A_{nv} = 0.6*58*4.25 = 147.9 \text{ kips}$$

$$0.6F_u A_{nv} > F_u A_{nt}$$

$$\Rightarrow \phi R_n = 0.75(0.6F_u A_{nv} + F_y A_{gt}) = 0.75(0.6*58*4.25 + 36*2.4) = 175.7 \text{ kips}$$

$$\text{Check: } 0.75(0.6F_u A_{nv} + F_u A_{nt}) = 0.75(0.6*58*4.25 + 58*1.7) = 184.9 \text{ kips (ok)}$$

Therefore, the design tensile strength = 175.7 kips

Solution Hwk #4, Prob #1, Text Prob # 3.4 - 4

Member W 16 x 40 (Table 1 - 1, pg. 1 - 18 to 1 - 19)

$$A_g := 11.8 \text{ in}^2 \quad t_w := 0.305 \text{ in} \quad t_f := 0.505 \text{ in} \quad d := 16 \text{ in}$$

$$\phi P_{ny} := 531 \text{ Kips} \quad \phi P_{nu} := 431 \text{ Kips}$$

$$b_f := 7 \text{ in} \quad A_e := 8.85 \text{ in}^2 \text{ (Table 3.1, pp 3 - 18)}$$

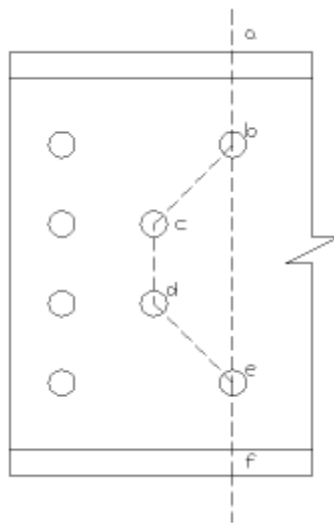
$$\text{A992 Grade Steel} \quad F_y := 50 \text{ Ksi} \quad F_u := 65 \text{ Ksi}$$

$$\text{Yield Strength} = \phi_t P_n = \quad P_{ny} := 0.9 A_g F_y \quad P_{ny} = 531 \text{ Kip}$$

- Calculation of Net Area

$$\text{line a-b-e-f} \quad A_{n1} := A_g - \left[2 \cdot \left(\frac{3}{4} + \frac{1}{8} \right) \cdot t_w \right] \quad A_{n1} = 11.266 \text{ in}^2$$

$$\text{line a-b-c-d-e-f} \quad A_{n2} := A_g - \left[4 \cdot \left(\frac{3}{4} + \frac{1}{8} \right) \cdot t_w \right] + \left[t_w \cdot 2 \cdot \left(\frac{3^2}{4 \cdot 3} \right) \right] \quad A_{n2} = 11.19 \text{ in}^2$$



$$\text{Net Area is lesser of above,} \quad A_n := \text{if}(A_{n1} < A_{n2}, A_{n1}, A_{n2}) \quad A_n = 11.19 \text{ in}^2$$

$$U := 0.75 \text{ Assumed 2 bolts per line} \quad U = 0.75$$

$$\text{Effective Area} \quad A_e := U \cdot A_n \quad A_e = 8.393 \text{ in}^2$$

$$\text{Fracture Strength} = \phi_t P_n = \quad P_{nu} := 0.75 A_e F_u \quad P_{nu} = 409.134 \text{ Kip}$$

. Therefore design strength = 409 kips

Solution Hwk #4, Prob # 2, Text Prob # 3.5 - 3

Member WT 8 x 13 Properties:

$$A_g := 3.84 \text{ in}^2$$

$$t_w := 0.25 \text{ in}$$

$$b_f := 0.345 \text{ in}$$

$$d := 7.85 \text{ in}$$

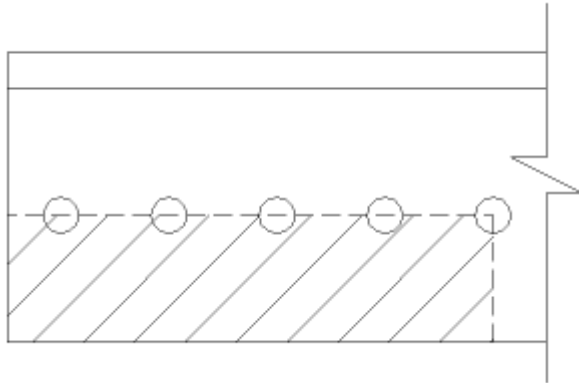
$$t_f := 5.5 \text{ in}$$

$$x := 2.09 \text{ in}$$

A992 Steel

$$F_u := 65 \text{ Ksi}$$

$$F_y := 50 \text{ Ksi}$$



$$7.845 - 4.5 = 3.345$$

$$A_{gv} := 13.5 t_w$$

$$A_{gv} = 3.375 \text{ in}^2$$

$$A_{nv} := A_{gv} - \left[4.5 \left(\frac{7}{8} + \frac{1}{8} \right) \cdot t_w \right]$$

$$A_{nv} = 2.25 \text{ in}^2$$

$$A_{gt} := 3.345 t_w$$

$$A_{gt} = 0.836 \text{ in}^2$$

$$A_{nt} := A_{gt} - \left[0.5 \left(\frac{7}{8} + \frac{1}{8} \right) \cdot t_w \right]$$

$$A_{nt} = 0.711 \text{ in}^2$$

Now,

$$F_u \cdot A_{nt} = 46.231 \text{ Kips} \quad \& \quad 0.6 F_u \cdot A_{nv} = 87.75 \text{ Kips}$$

Since, $F_u A_{nt} < 0.6 F_u A_{nv}$, Equation with fracture shear path governs....

$$\phi R_n := 0.75 (0.6 F_u \cdot A_{nv} + F_y \cdot A_{gt})$$

$$\phi R_n = 97.172 \text{ Kips}$$

Problem 3

$$L := 175 \text{ kips}$$

$$D := 175 \text{ kips}$$

$$P := 1.2 \cdot D + 1.6 \cdot L \rightarrow 490.0 \text{ kips}$$

$$F_y := 50 \text{ ksi} \quad F_u := 65 \text{ ksi} \quad L := 8 \text{ in}$$

W10x49

$$A_g := 14.4 \text{ in}^2 \quad \bar{x} := 0.807 \text{ in} \quad t_f := 0.56 \text{ in} \quad b_f := 10 \text{ in}$$

$$\phi_{Pny} := A_g \cdot F_y \cdot 0.9 \rightarrow 648.00 \text{ kips} \quad \text{Gross Yield}$$

$$A_n := A_g - 4 \cdot \left(1.25 + \frac{1}{8} \right) \cdot t_f \quad A_n = 11.32 \text{ in}^2$$

$$U := 1 - \frac{\bar{x}}{L}$$

$$A_e := U \cdot A_n \quad A_e = 10.178 \text{ in}^2$$

$$\phi_{Pnf} := A_e \cdot F_u \cdot 0.75 \rightarrow 496.182131250000000000 \text{ kips} \quad \text{Fracture Strength}$$

For Block Shear

$$A_{gv} := 10.5 \cdot t_f \cdot 4 \quad A_{gv} = 23.52 \text{ in}^2$$

$$A_{nv} := A_{gv} - 4 \cdot \left[2.5 \cdot \left(\frac{5}{4} + \frac{1}{8} \right) \cdot t_f \right] \quad A_{nv} = 15.82 \text{ in}^2$$

$$A_{gt} := 4 \cdot 2 \cdot t_f \quad A_{gt} = 4.48 \text{ in}^2$$

$$A_{nt} := A_{gt} - 4 \cdot \left[0.5 \cdot \left(\frac{5}{4} + \frac{1}{8} \right) \cdot t_f \right] \quad A_{nt} = 2.94 \text{ in}^2$$

Now,

$$F_u \cdot A_{nt} = 191.1 \text{ Kips} \quad \& \quad 0.6 \cdot F_u \cdot A_{nv} = 616.98 \text{ Kips}$$

Since, $F_u A_{nt} < 0.6 F_u A_{nv}$, Equation with fracture shear path governs....

$$\phi_{R_n} := 0.75 \cdot (0.6 \cdot F_u \cdot A_{nv} + F_y \cdot A_{gt}) \quad \phi_{R_n} = 630.735 \text{ Kips}$$

Design strength = 496 kips > 490 kips

$$\text{Max Length} = 300r = 300 \cdot 2.54 / 12 = 63.5 \text{ ft} > 30 \text{ ft (ok)}$$