# ECE 255, Darlington Pair 

7 November 2017

In order to understand the derivation of Prof. Chen on the Darlington pair in her notes, it will be prudent to do Exercise 8.30 from Sedra and Smith. You are asked to show that (see Figure 1):

1. $R_{\mathrm{in}}=\left(\beta_{1}+1\right)\left[r_{e 1}+\left(\beta_{2}+1\right)\left(r_{e 2}+R_{E}\right)\right]$
2. $R_{\text {out }}=R_{E} \|\left[r_{e 2}+\frac{r_{e 1}+\left[R_{\text {sig }} /\left(\beta_{1}+1\right)\right]}{\beta_{2}+1}\right]$
3. $\frac{v_{o}}{v_{s i g}}=\frac{R_{E}}{R_{E}+r_{e 2}+\left[r_{e 1}+R_{s i g} /\left(\beta_{1}+1\right)\right] /(\beta+2+1)}$

## Answers:

1. The answer is to use the resistance-reflection rule twice. If $Q_{1}$ has an emitter resistance of $R_{E 1}$, then using formula (7.107) of S\&S, one gets

$$
R_{\mathrm{in}}=\left(\beta_{1}+1\right)\left(r_{e 1}+R_{E 1}\right)
$$

But $R_{E 1}$ is the input resistance looking into the base of $Q_{2}$. Using the reflection formula again to get $R_{E 1}$ from $R_{E}$, or

$$
R_{E 1}=\left(\beta_{2}+1\right)\left(r_{e 2}+R_{E}\right)
$$

one gets the above formula in Part 1.
Note: Since $\left(\beta_{1}+1\right) r_{e 1}=r_{\pi 1}$ which can be gotten by comparing the input impedance of the hybrid- $\pi$ model and the T model, the above reflection formula can also be written as

$$
R_{\mathrm{in}}=\left(\beta_{1}+1\right) r_{e 1}\left(1+R_{E 1} / r_{e 1}\right)=r_{\pi 1}\left(1+R_{E 1} / r_{e 1}\right)
$$

Since $g_{m}=\alpha / r_{e 1} \approx 1 / r_{e 1}$, the above formula is often approximated as

$$
R_{\mathrm{in}} \approx r_{\pi 1}\left(1+g_{m 1} R_{E 1}\right)
$$

The above formula is often used in Prof. Chen's notes.
Again, using the approximate reflection formula, one can rewrite $R_{E 1}$ as

$$
R_{E 1}=r_{\pi 2}\left(1+g_{m 2} R_{E}\right)
$$

[^0]
(b)

Figure 1: The Darlington pair or configuration for the analysis in Exercise 8.30 of S\&S (Courtesy of Sedra and Smith).
2. First, one needs to find the Thevenin resistor of the Thevenin equivalence of the source to the left of $R_{E}$. Then $R_{\text {out }}=R_{E} \| R_{\text {Thev }}$. To find $R_{\text {Thev }}$, one shorts out the voltage source, and uses the inverse reflection rule two times to get

$$
R_{\mathrm{Thev}}=\left[r_{e 2}+\frac{r_{e 1}+\left[R_{s i g} /\left(\beta_{1}+1\right)\right]}{\beta_{2}+1}\right]
$$

The inverse reflection formula is based on that, for a BJT, every unit of current that flows in the base, there is $\beta+1$ unit of current that flows in the emitter to arrive at the formula in Part 2.

Using the fact that $g_{m}=\alpha / r_{e} \approx 1 / r_{e}$, and that $\beta+1 \approx \beta$, the above formula can also be approximated as

$$
R_{\mathrm{out}} \approx R_{E} \|\left[1 / g_{m 2}+\frac{1 / g_{m 1}+\left[R_{\mathrm{sig}} /\left(\beta_{1}\right)\right]}{\beta_{2}}\right]
$$

as is found in Prof. Chen's notes.
3. For this problem, it is necessary to find the Thevenin resistor looking to the left of $R_{E}$ from the emitter of $Q_{2}$. This resistor is obtained by shortcircuiting the source, and looking at the impedance to the left of $R_{E}$. This Thevenin resistor is similar to that in Part 2. Next, the equivalent Thevenin voltage source needs to be found. This can be done by opencircuiting the load by letting $R_{E} \rightarrow \infty$. It is seen that $R_{\text {in }} \rightarrow \infty$ in this case. With the small voltage drops between the base and the emitters, it is seen that $v_{\text {Thev }} \approx v_{\text {sig }}$. Hence formula in Part 3 above can be derived usig the Thevenin equivalent circuit and the voltage divider formula.


[^0]:    Printed on November 7, 2017 at 21:27: W.C. Chew and Z.H. Chen.

