# Lecture Summary – Combination Chapter 9

- array building
  - o two principal beamwidth shapes suitable for array building
    - 2<sup>nd</sup> order "plateau" type that flattens out in the high frequencies ("constant directivity") – provides consistent unity splay angle → applications in both H and V planes (but in limited quantities)
    - highly sloped 3<sup>rd</sup> order elements useful in highly overlapped coupled array configurations (no consistent unity splay angle) – foremost application is creation of asymmetrical arrays → leader in vertical applications
    - (1st order speakers best suited for "standalone" applications  $\rightarrow$  best for horizontal coverage applications
- role of overlap as a "shaping tool"
  - o can range from half as wide to twice as wide
  - o decisive factor: percentage overlap
  - o control of overlap
    - angular (point in different directions)
    - displacement (moving elements apart)
  - o low overlap: elements retain much of their individual character (yet merge to create "sculpted shapes" unique to arrays)
  - o high overlap: individual elements disappear and merge into combined shape of "new and different" single speaker
  - o overlap is the "shaping tool"

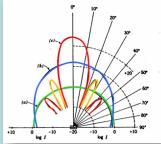
### • limitations of combined shapes

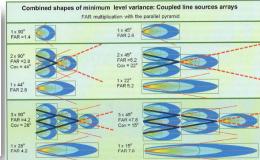
- o will use aspect ratio icons to visualize individual contributions
- o beam concentration and ripple variance aspect of combined response are not apparent in simple icon representation
- role of asymmetry as a "shaping tool"
  - o what asymmetries are available to the array designer
  - o why are asymmetries necessary
  - o which asymmetries are static and which are dynamic
- coupled line source arrays basic idea
  - o stack "aspect ratio icons" end-to-end (for side-by-side speakers)
  - o combined shape of coupled line source visualized as forward extension by means of simple additions of aspect ratio shapes

Recall: Beamwidth of a single speaker approaches  $90^{\circ}$  when the transmitted  $\lambda$  equals the radiating cone size (blue line in figure). Beamwidth is wider if  $\lambda$  > cone size (green line) and narrower if  $\lambda$  < cone size (red line).

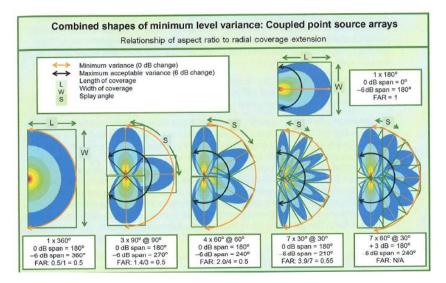
For a coupled line source, vertical coverage is  $72^{\circ}$  when the transmitted  $\lambda$  equals the line length (e.g. beamwidth for a 2m long array will be  $72^{\circ}$  at 170 Hz).

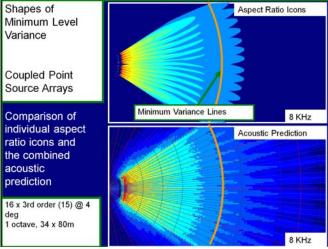
Note that equations relating line length to beamwidth assume omnidirectional ("point") sources.



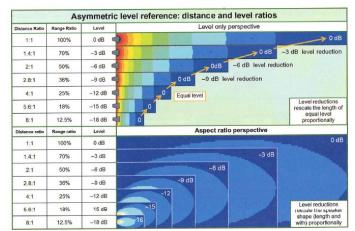


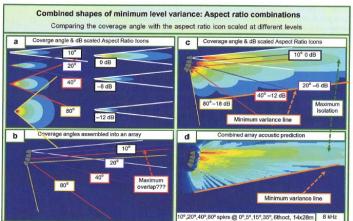
- coupled point source arrays basic idea
  - o arrange aspect ratio icons side-by-side around a virtual point source (unity splay angle)
  - combined shape will strongly resemble radial spread of individual FAR patterns

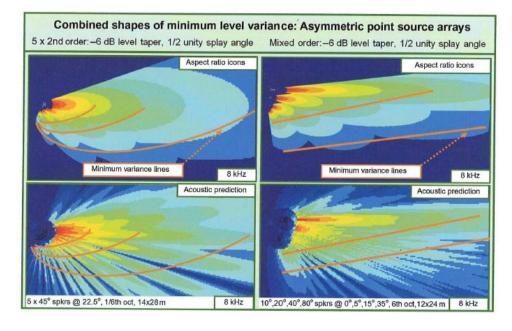




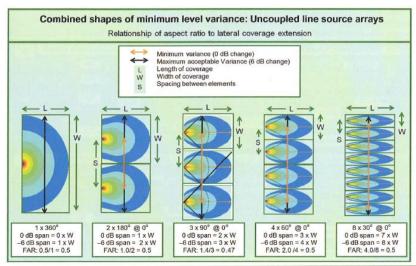
• asymmetric level scaling - size of icon reduced 50% for each reduction in level by 6 dB

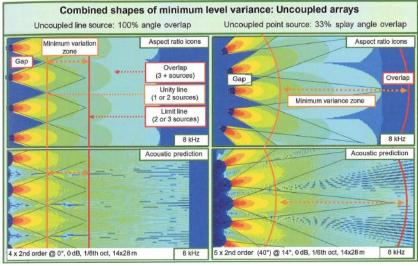


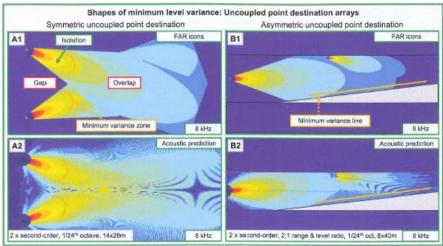




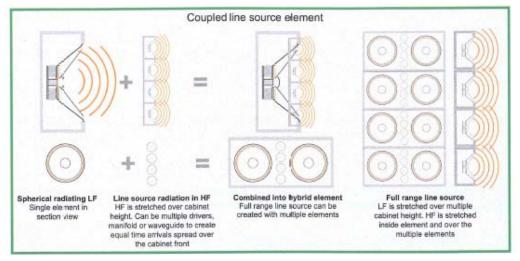
- uncoupled arrays basic idea
  - o best way to deal with overly wide coverage shapes
  - combined shape can be seen as lateral extension by means of simple stacking of aspect ratio shapes
  - o combined aspect ratio becomes wider (while not becoming longer) and therefore lower in number
  - o FAR found by dividing the single element FAR by the number of elements



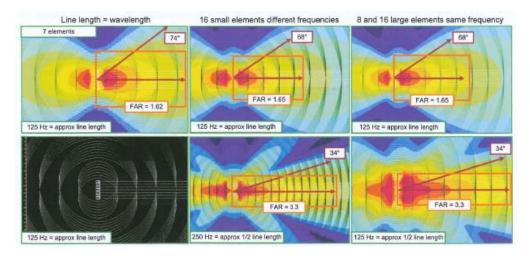




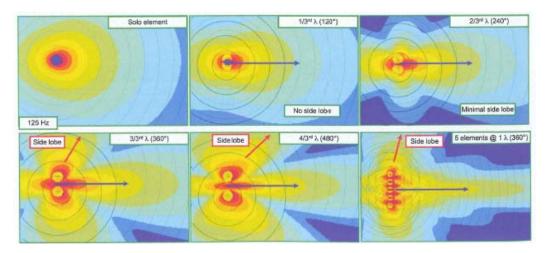
- spectral variance of coupled arrays
  - o possible outcomes of beam combinations
    - concentration/power addition (coupling zone)
    - spreading (isolation zone)
    - "passing through each other" (combing zone)
- spectral variance of coupled line source arrays
  - o representative line source element



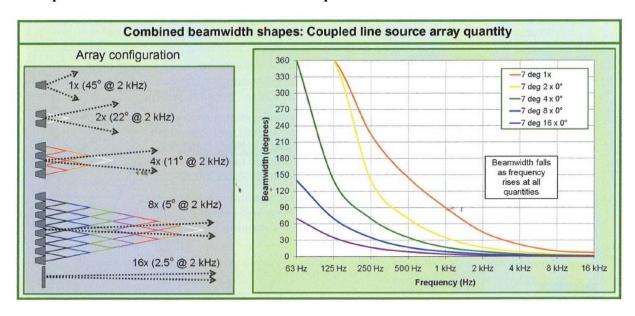
coupled line source length effects



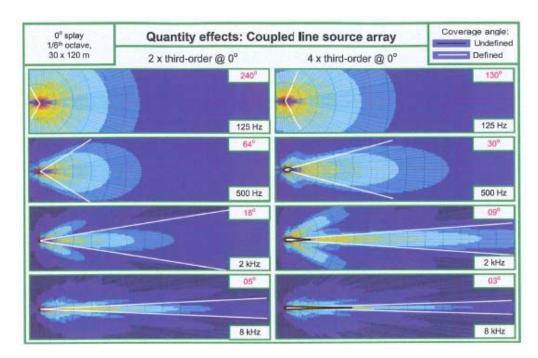
o coupled line source element spacing effects



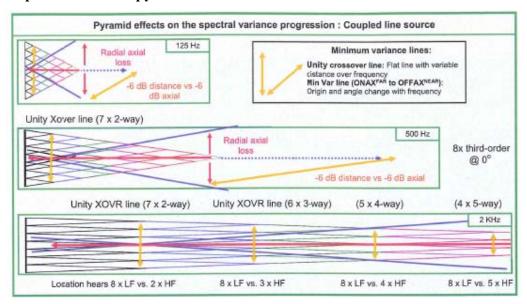
# o coupled line source element beamwidth shapes



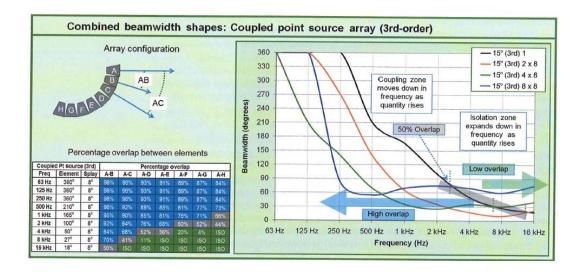
- o coupled line source element quantity effects
  - coverage pattern narrows as quantity rises
  - ratio of spectral variance unchanged by quantity
  - beam concentration is primary driving force
  - larger quantities give appearance of reduced spectral variance if range of viewing does not extend far enough for coupling to occur over the full frequency range



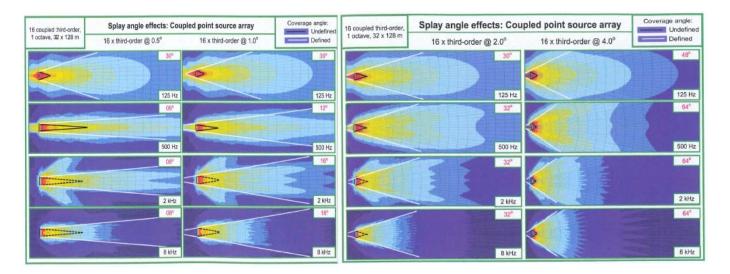
## o coupled line source pyramid effects



- coupled line source speaker order effects
  - line length is dominate force at lower frequencies (where line length  $\geq \lambda/2$ )
  - side lobes vary with speaker order but main lobes are still matched at mid frequencies
  - at high frequencies, low-order array coverage degenerates into ripple, while high-order array maintains focus
- o coupled line source level tapering effect
  - effectively reduces number of elements contributing to the "pyramid"
  - behavior mimics an array of shorter length
  - (aside frequency dependent amplitude tapering not considered in text, nor is delay tapering – accomplished using DSP)
- spectral variance of coupled point source arrays
  - o beamwidth shapes

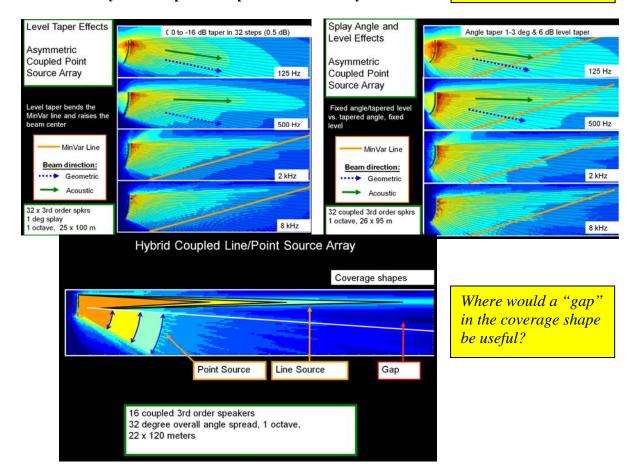


- o splay angle effects
  - even a small splay angle creates an opportunity for reduced spectral variance (that cannot be found in a coupled line source...unless DSP techniques are used)
  - isolation (even in small measure) will counteract pattern narrowing



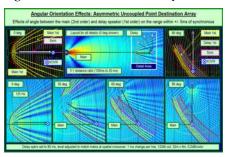
- o asymmetry (symmetry percentage) ratio of angular coverage above and below center
  - level taper
  - splay (angle) taper
  - mixed loudspeaker orders
  - lateral spacing/level offsets
  - forward spacing/level offsets
  - hybrid coupled line/point source arrays

Level tapering bends the minimum variance line and raises the beam center



- uncoupled arrays
  - o line source
  - o point source
  - o point destination

# Lateral Spacing and Level Effects O GB O GB A x 1st order (90) Spacing is tapered by 50% as level is reduced by 6 dB 1/6th octave 21 x 42 meters



### • conclusions

- o 1st order speakers
  - most suitable for single-element applications with a low proximity ratio
  - least suitable for angular overlap
  - least suitable for combination (power addition)
  - beamwidth must not widen as frequency rises (once plateau reached must remain constant)
  - should be arrayed at or near unity splay angle based on beamwidth plateau
- o 2nd order speakers
  - most suitable for single-element applications with a medium proximity ratio
  - suitable for combination (power addition) on a limited basis
  - no beamwidth reversal (widening as frequency increases)
  - should be arrayed at or near unity splay angle based on beamwidth plateau
- 3<sup>rd</sup> order speakers
  - least suitable for single-element applications
  - most suitable for angular overlap
  - suitable for combination (power addition)
  - constant downward beamwidth slope (with no reversals) as frequency increases
  - should be arrayed at an angle greater than 0° (relative)
- power capability
  - coupled arrays can increase concentrated power capability beyond a single element while maintaining minimum variance over long distances
  - the coupled point source has the highest ratio of increased power to variance over the widest frequency span and spatial area
  - the coupled line source can provided "unlimited" power but is incapable of minimum spectral variance over the space
  - asymmetric level tapering will decrease the overall power capability at the geometric center of the array but provide the opportunity for minimum variance over an asymmetric space
  - uncoupled arrays can increase distributed power capability beyond a single element while maintaining minimum variance, but only over a very limited distance
- o minimum variance coverage shapes
  - rectangle: individual speaker
  - arc: symmetric point source
  - right triangle: asymmetric coupled point source
- o minimum variance principles
  - single speakers
    - position the speakers with the lowest possible proximity ratio to the audience in at least one plane
    - use speakers that have minimum beamwidth ratio over frequency ( $1^{st}$  or  $2^{nd}$  order)

- match the properties of symmetry (symmetric orientation for symmetric shapes, asymmetric orientation for asymmetric shapes)
- match speaker aspect ratio to audience coverage shape
- if speaker coverage pattern overlap on to room surfaces is too strong, use an array instead
- o minimum variance principles, continued...
  - symmetric point source coupled arrays
    - fill the arc angle required to fit the shape of the audience area (number of elements required will depend on speaker order)
      - o low-order speakers must have minimal overlap
      - o high-order speakers can be overlapped for power addition
    - beam spreading will shape (widen) the HF coverage
    - beam concentration will shape (narrow) the LF coverage
    - apply these principles to make shapes meet in the mid-range
  - uncoupled arrays
    - achieve isolation by angular offset and/or displacement
    - as angular offset falls, the usable depth range falls as well
    - uncoupled array depth is initiated by overlap
      - o before overlap, response is as a single element
      - o after overlap begins, array behavior and ripple variance begin
    - uncoupled array depth is limited by overlap multiple overlap provides the ending limit for depth
    - uncoupled arrays can be scaled by relative level to appropriate depth

