

21st Gerald A. Leonards Lecture 11 April 2025, Purdue University, Lafayette Indiana



ENGINEERING FROZEN GROUND UNDERSTANDING THE BEHAVIOUR OF SOIL ON FREEZING AND THAWING





Line 1 of Napoli underground

project layout ground conditions design issues use of Artificial Ground Freezing (AGF)



Line 1 of Napoli underground

early applications (Garibaldi)

observed phenomena heat propagation analyses method optimisation & control of construction



Line 1 of Napoli underground

early applications (Garibaldi & Municipio)

fully coupled THM modelling

predictive capabilities
TX data
thaw behaviour





Line 1 of Napoli underground

early applications (Garibaldi & Municipio)

fully coupled THM modelling

not just AGF

permafrost degradation frost heave apparatus what next?





Line 1 of Napoli underground

early applications (Garibaldi & Municipio)

fully coupled THM modelling

not just AGF

conclusions





13 km (9) completed 1998

8 km (5) completed 2002

6 km (5) completed 2013

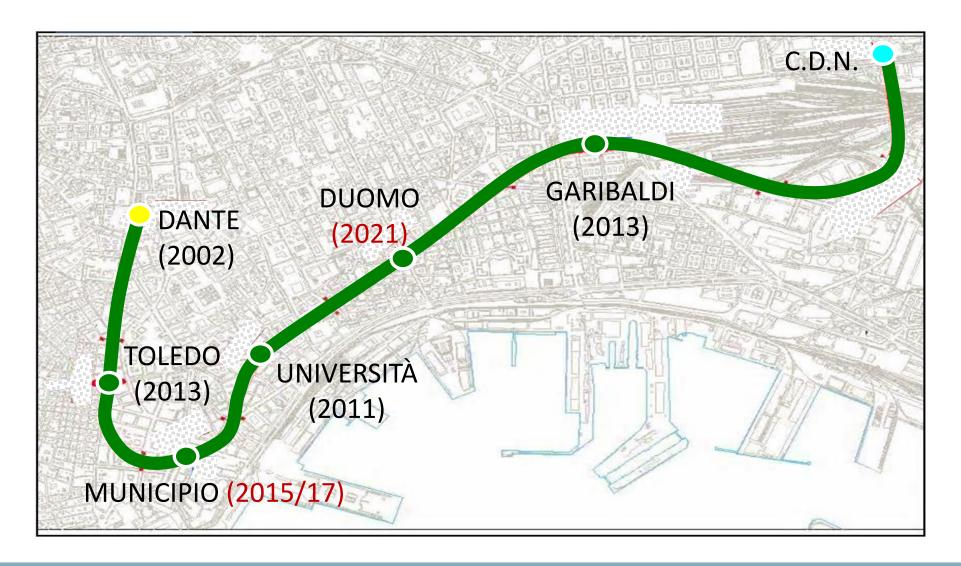
16 km (6) construction

1 km (0) design







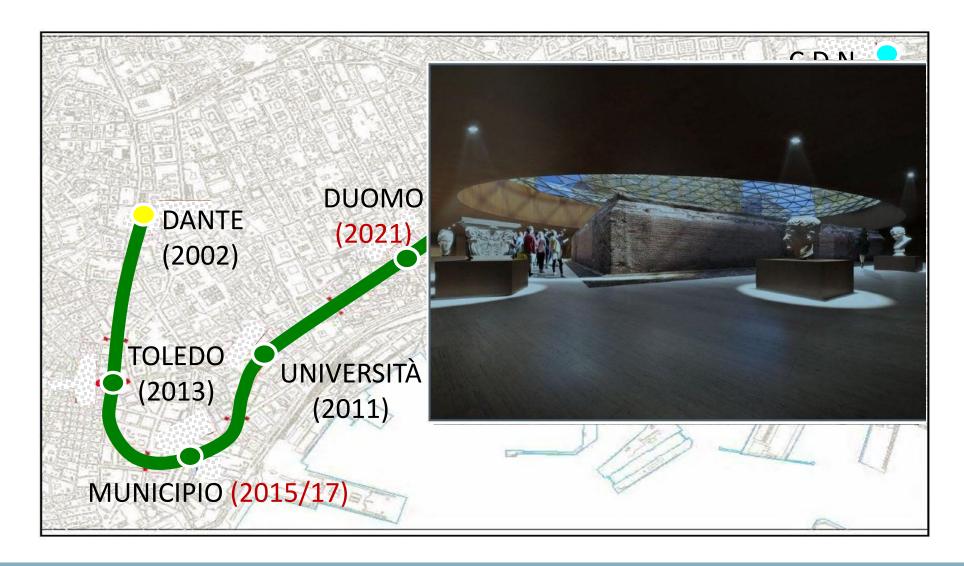






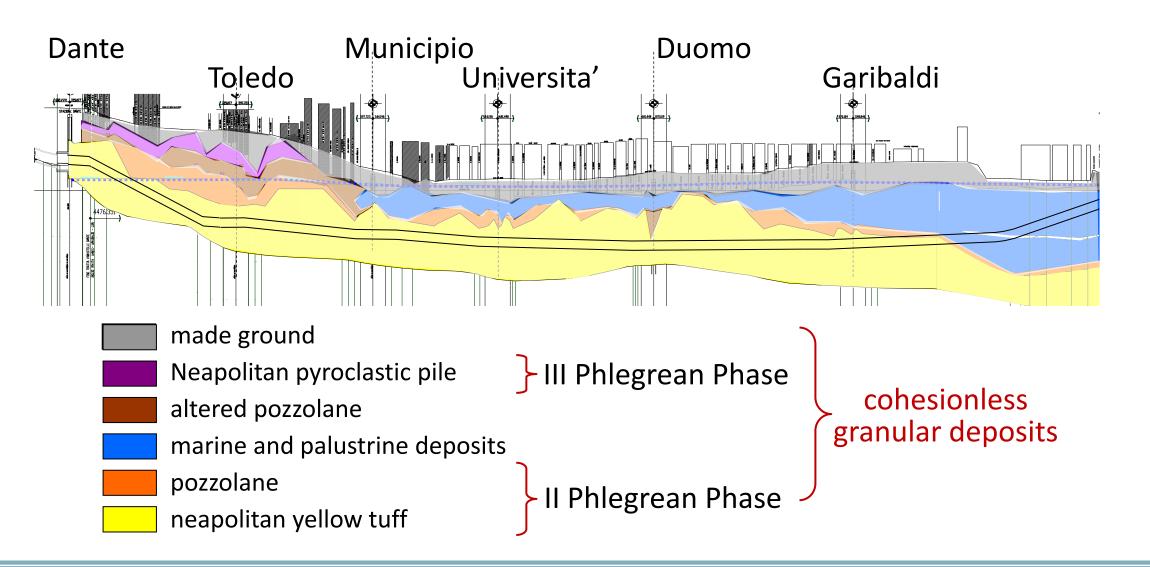






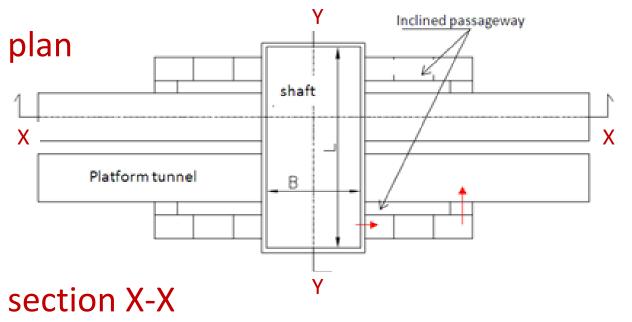




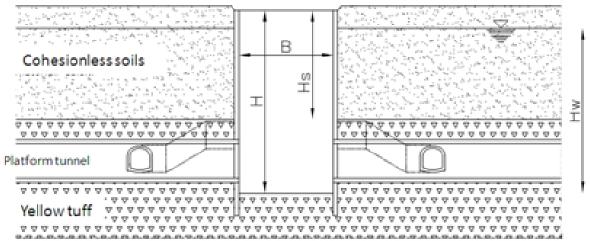




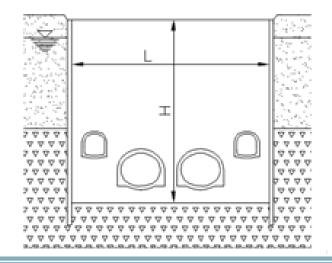




station	B (m)	L (m)	H (m)	Hs (m)	Hw (m)
Municipio	23.40	46.19	36.05	17.20	29.65
Università	16.20	43.55	34.85	20.40	33.50
Duomo	16.20	43.45	35.20	17.00+24.70	35.20
Garibaldi	21.00	46.00	44.70	29.00	35.30



section Y-Y







- bottom of excavation 35 to 50 m b.g.l.

- plan area $\sim 1000 \text{ m}^2$

- thickness of granular soils 20 to 30 m

- thickness of soft rock 10 to 15 m

- high water table 30 to 35 m a.d.l.



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construction techniques

- RC diaphragm walls (hydromill)





- bottom of excavation 35 to 50 m b.g.l.

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- thickness of granular soils 20 to 30 m

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construction techniques

- RC diaphragm walls (hydromill)
- props and anchors





- bottom of excavation 35 to 50 m b.g.l.

- plan area $\sim 1000 \text{ m}^2$

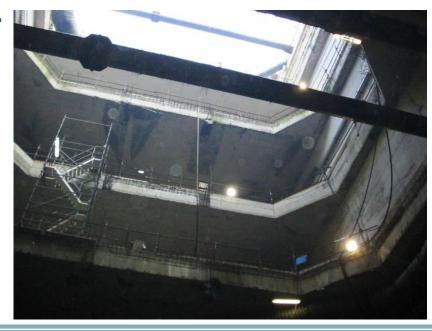
- thickness of granular soils 20 to 30 m

- thickness of soft rock 10 to 15 m

- high water table 30 to 35 m a.d.l.

construction techniques

- RC diaphragm walls (hydromill)
- props and anchors
- top-down construction





LINE 1 station tunnels

platform tunnels fractured soft rock (yellow tuff)

inclined passageways granular soil (pozzolana)

below the water table

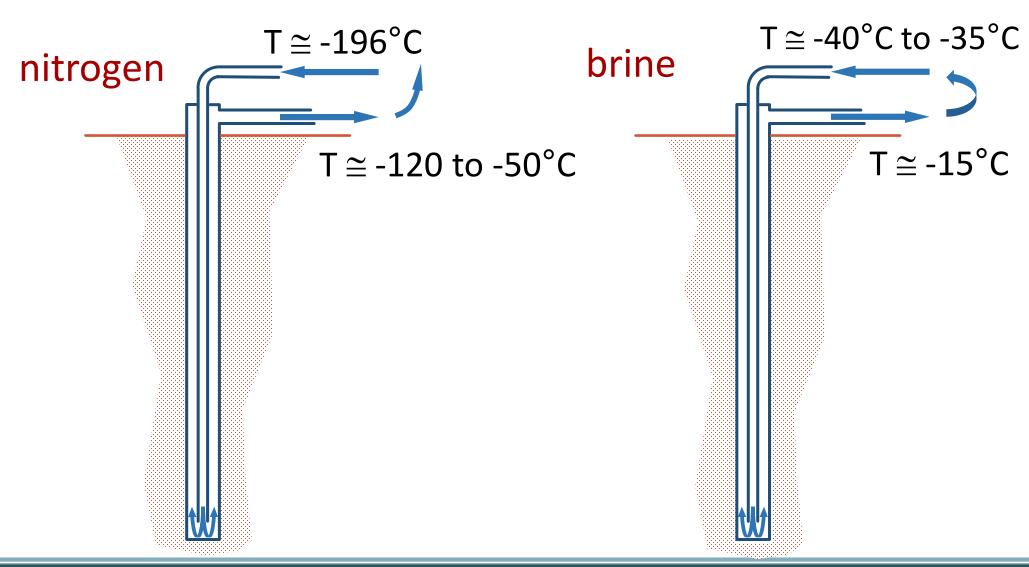
construction techniques







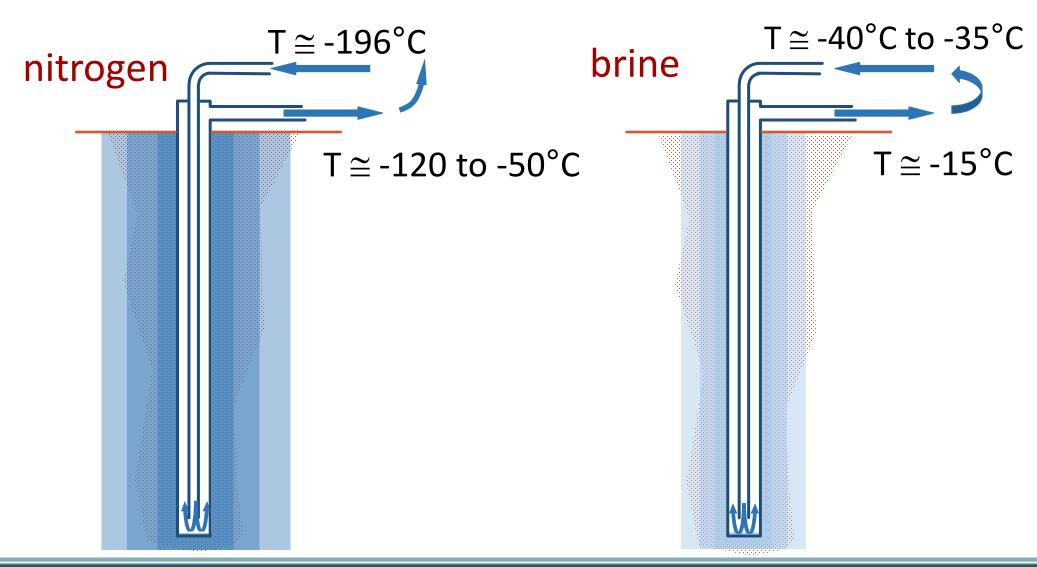
ARTIFICIAL GROUND FREEZING







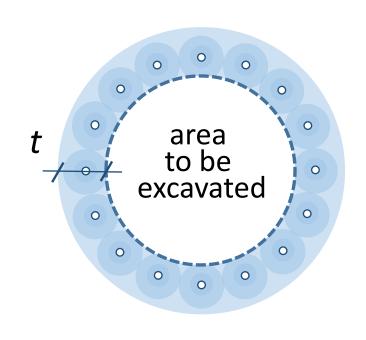
ARTIFICIAL GROUND FREEZING







ARTIFICIAL GROUND FREEZING



- ✓ increased strength
- ✓ low permeability



LINE 1 station tunnels

platform tunnels fractured soft rock (yellow tuff)

inclined passageways granular soil (pozzolana)

below the water table

construction techniques

* Artificial Ground Freezing

static inclined passageways

hydraulic platform tunnels/passageways







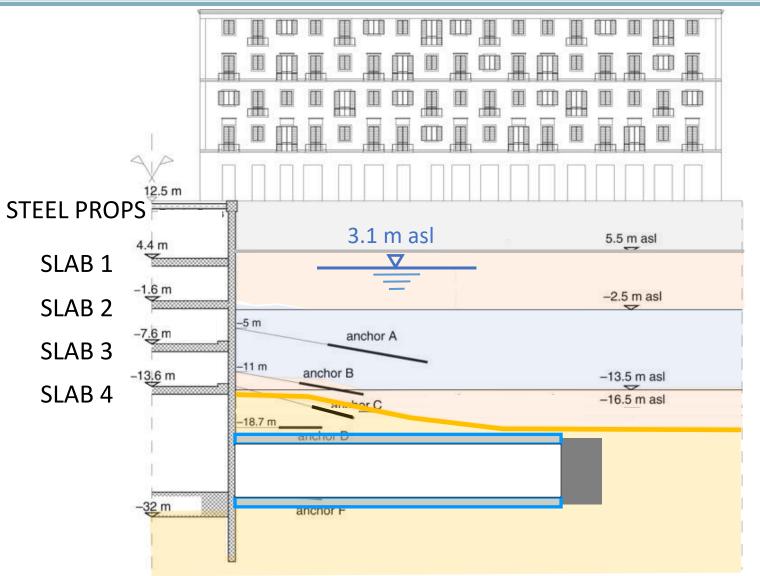
GARIBALDI (2002-2013)







GARIBALDI section



made ground pyroclastic sand

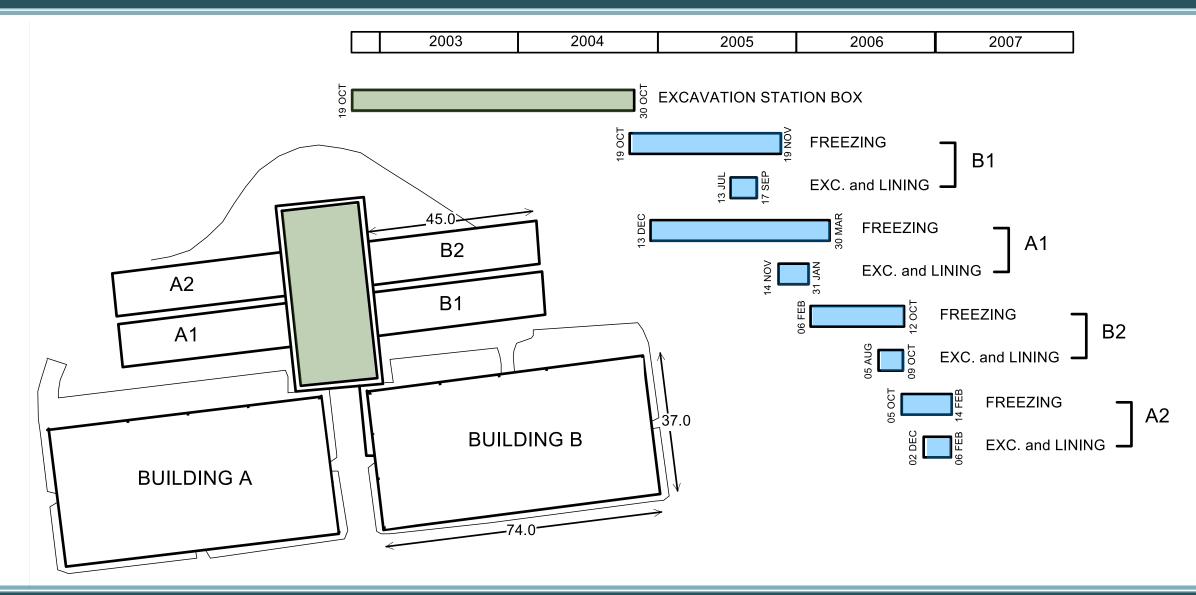
seabed deposits pozzolana

yellow tuff





GARIBALDI construction phases

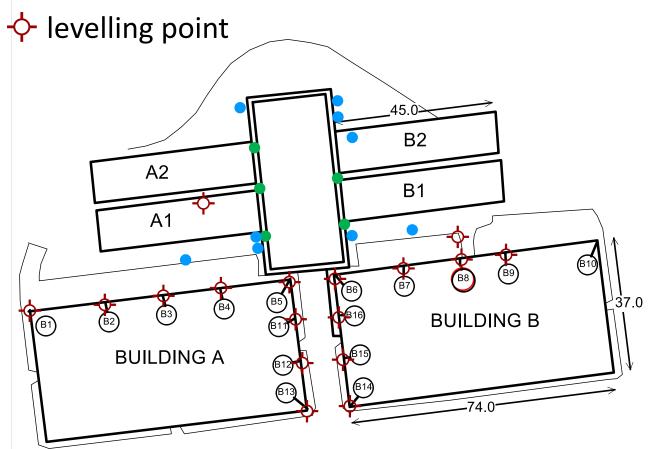






GARIBALDI monitoring

- Casagrande piezometer
- inclinometer



anchor load cells

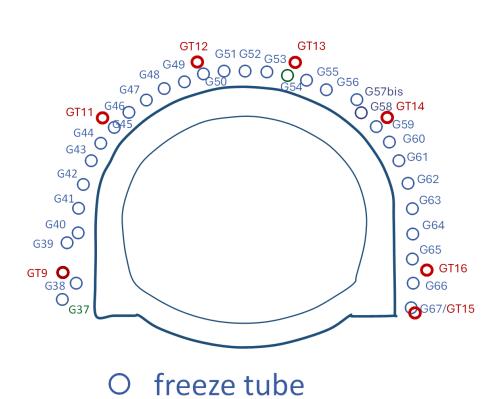


temperatures in the ground (TC in observation holes)

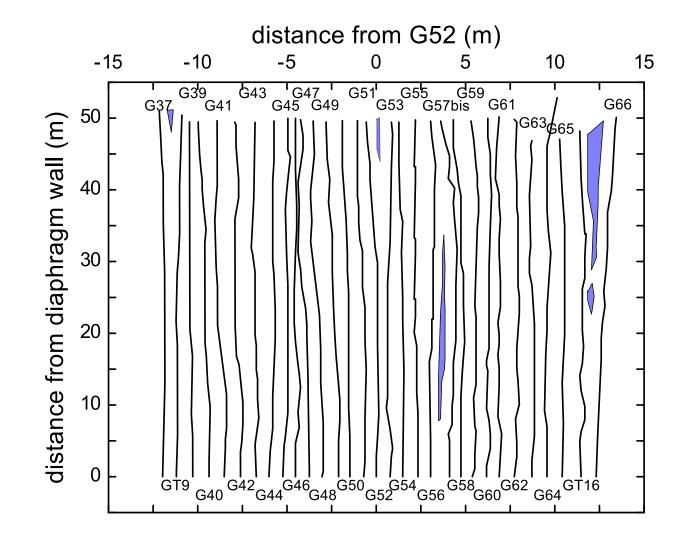




GARIBALDI freezing and observation tubes



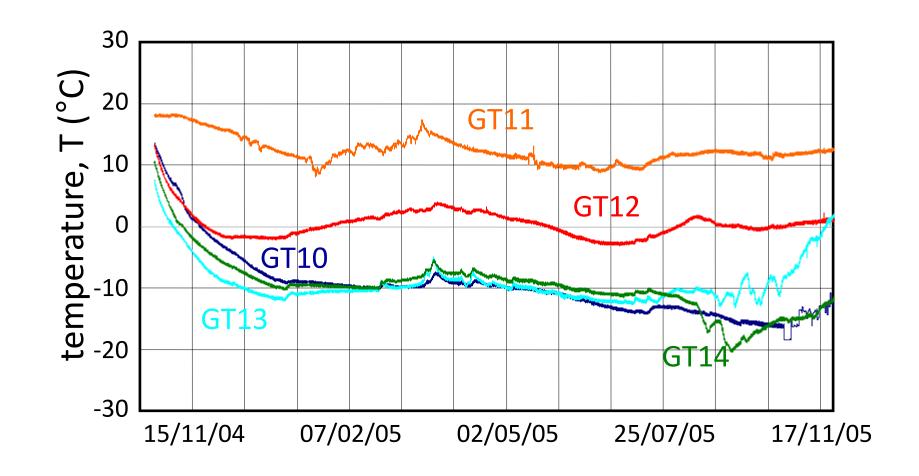
observation hole







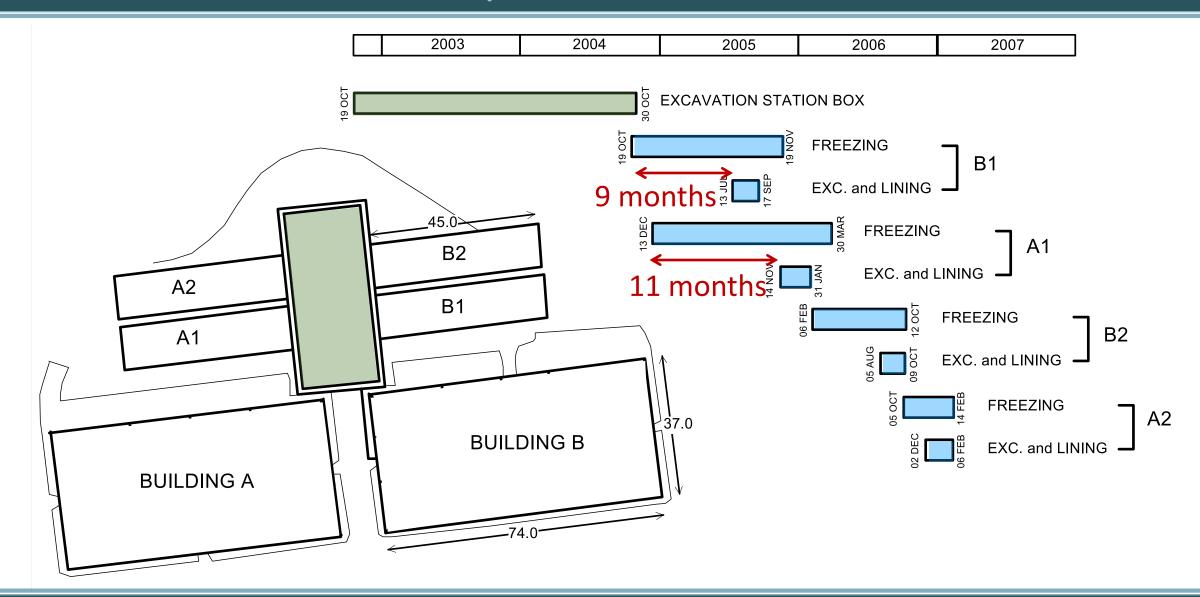
GARIBALDI temperatures







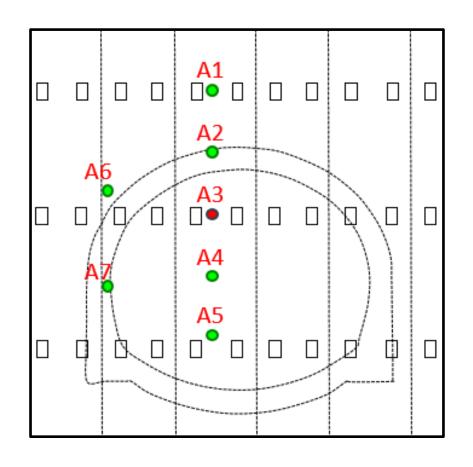
GARIBALDI construction phases

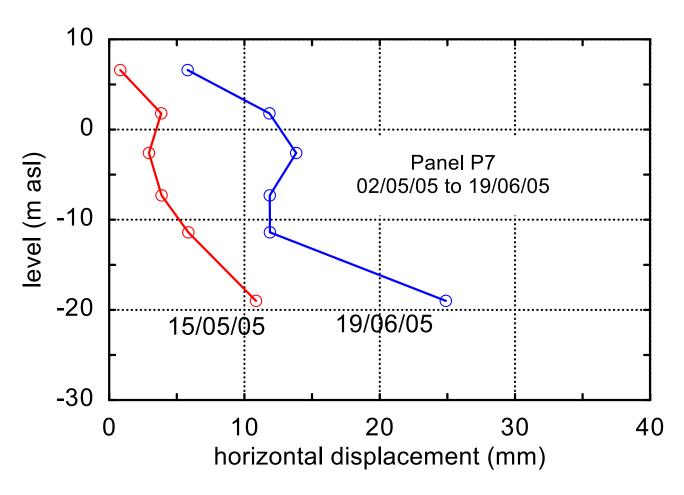






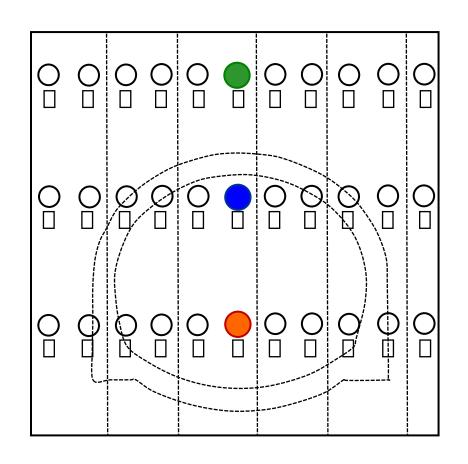
GARIBALDI convergence

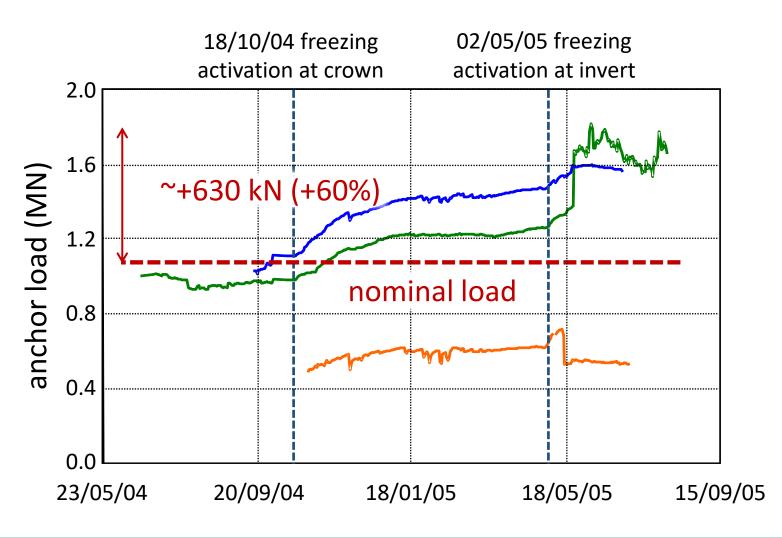






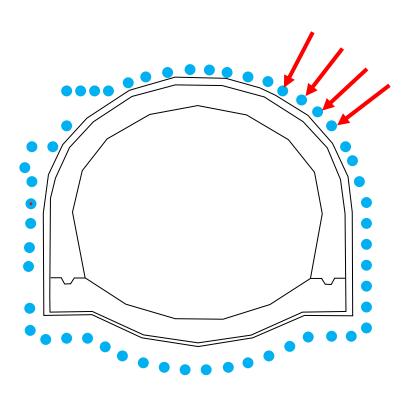
GARIBALDI anchor loads





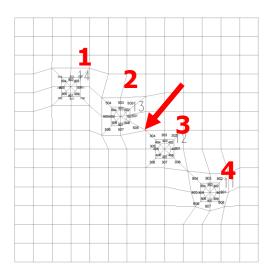




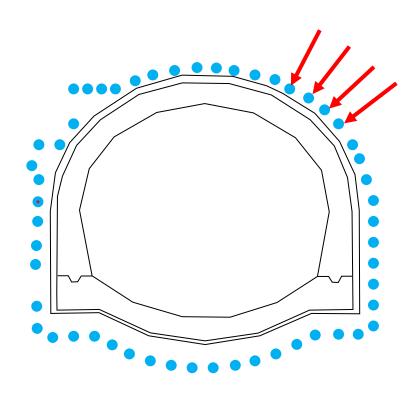


diameter 10.6 m 53 freezing tubes

temperature @ mid point frozen thickness



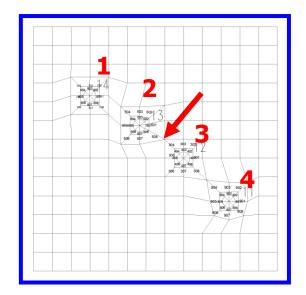




thermal conductivity $1.49 \div 2.69 \text{ W/m}^{\circ}\text{C}$ heat capacity $1604 \div 1134 \text{ J/(kg}^{\circ}\text{C)}$ specific heat $0.84 \div 0.60 \text{ J/m}^{3}^{\circ}\text{C}$

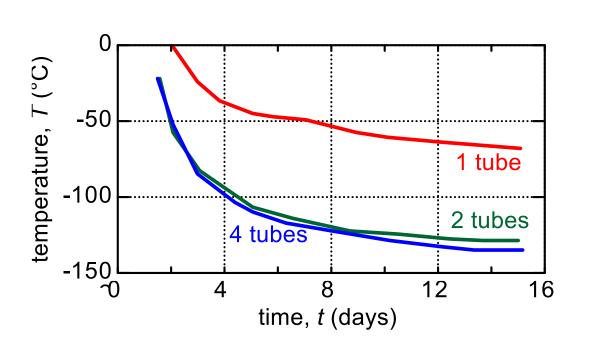
boundary conditions

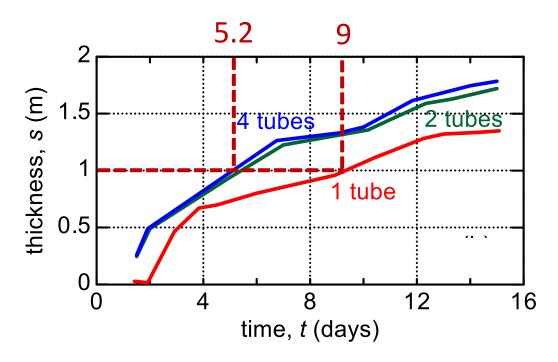
15 °C @ mesh boundary -174/-40 °C @ freeze tubes





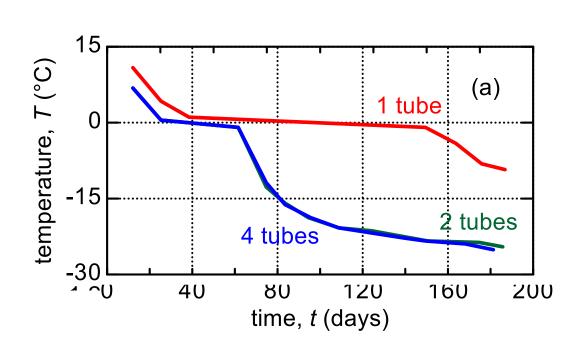
nitrogen activation

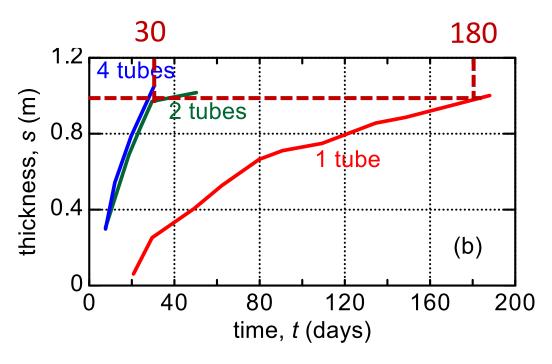






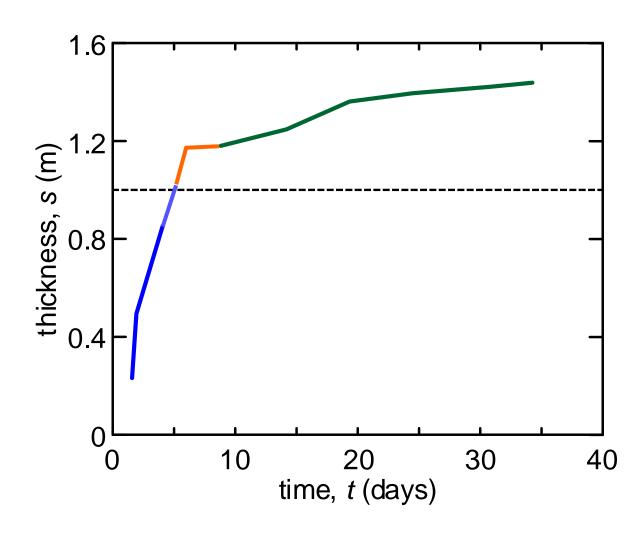
brine activation







OPTIMISATION

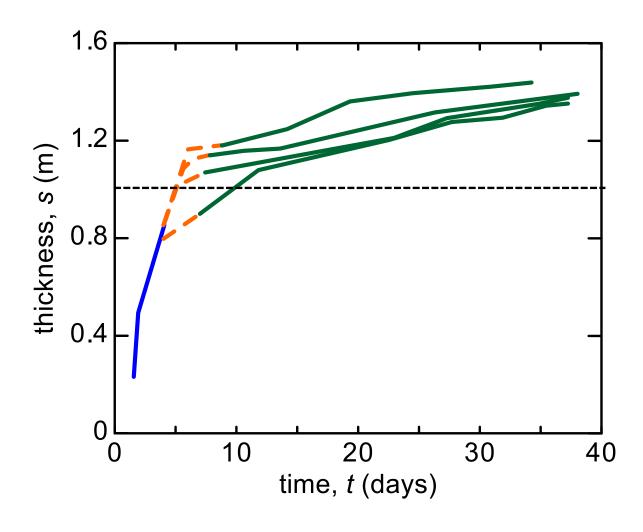


nitrogen activation thawing brine maintenance

1.00 m 1.18 m 1.48 m



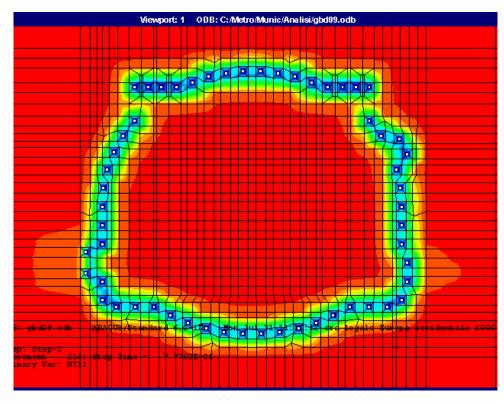
OPTIMISATION



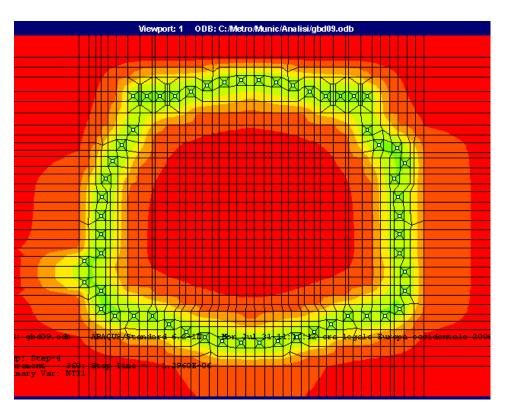
nitrogen activation thawing brine maintenance

1.00 m 1.18 m 1.48 m 0.90 m 1.14 m 1.37 m 0.85 m 1.05 m 1.34 m 0.80 m 0.90 m 1.35 m





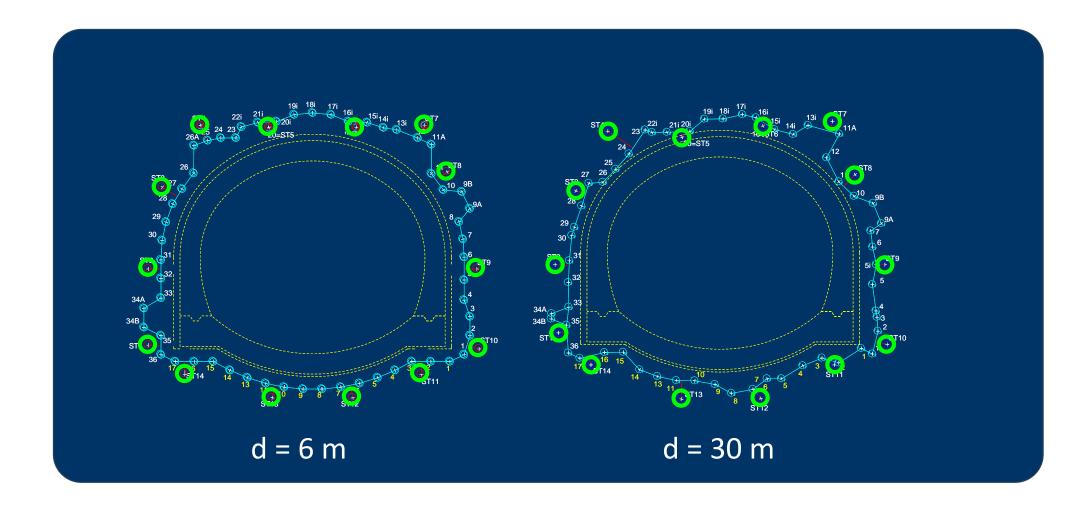
end of nitrogen activation (7dd)



after brine maintenance (26 dd)



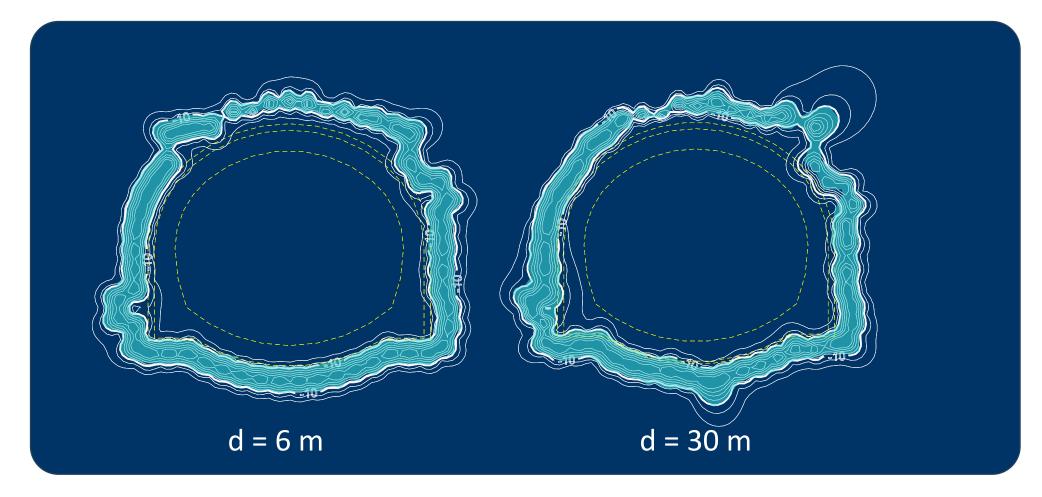






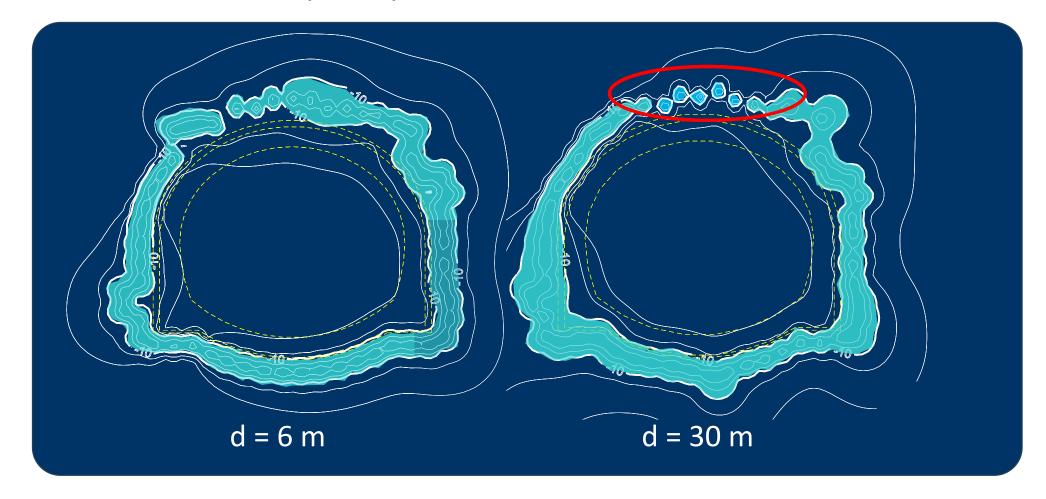


end of nitrogen activation (7dd)



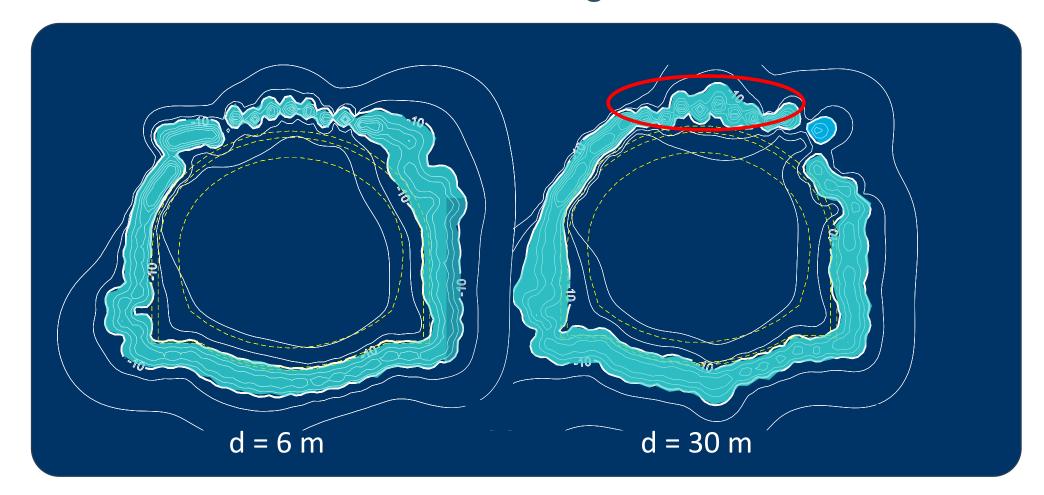


after brine maintenance (26dd)





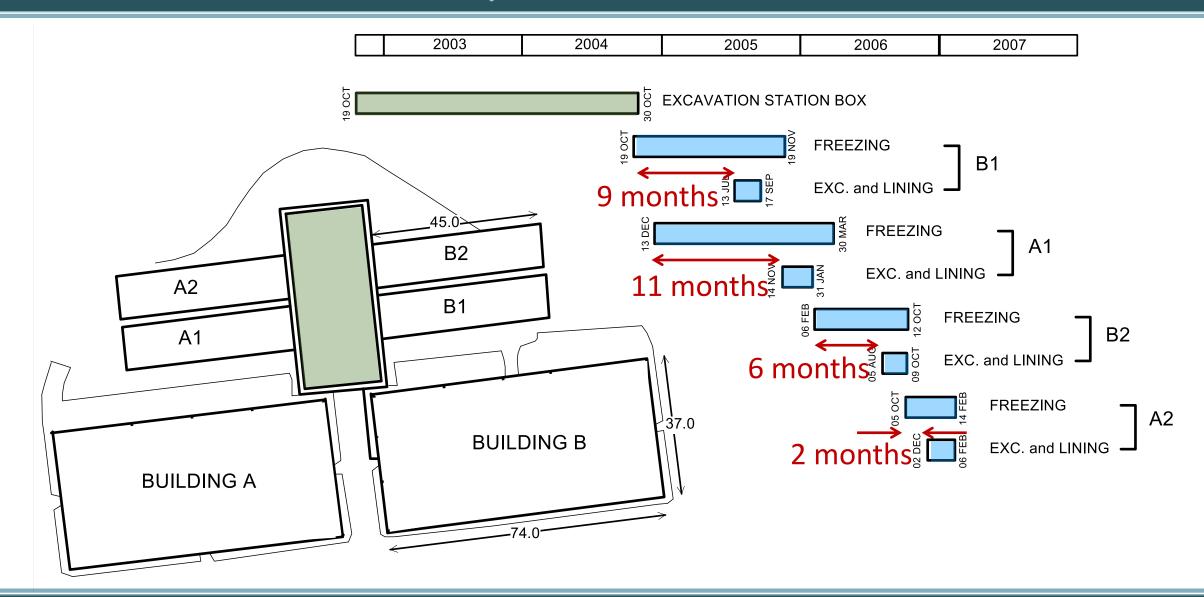
re-activation at crown with localised freezing







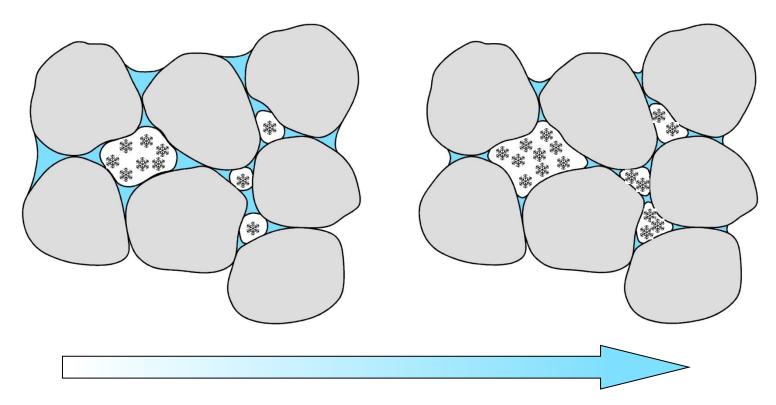
GARIBALDI construction phases







DEVELOPMENT OF SOIL FREEZING

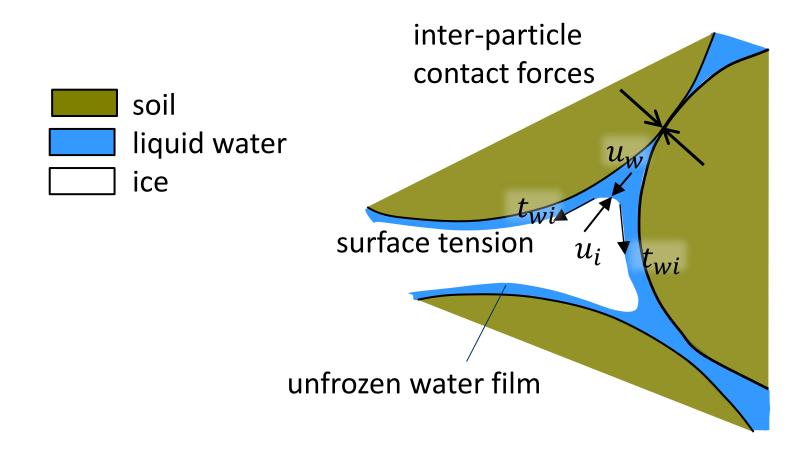


reducing temperature





DEVELOPMENT OF SOIL FREEZING







thermo-dynamical equilibrium (Clausius-Clapeyron equation)

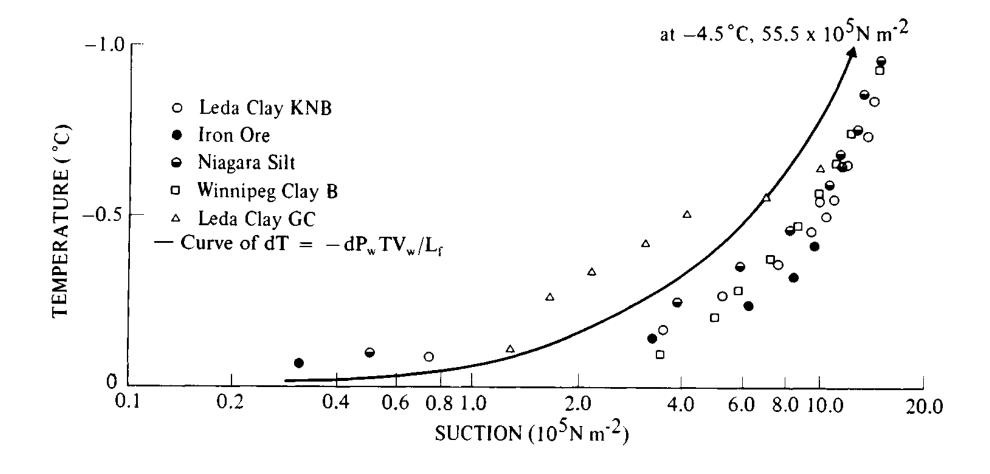
$$p_i = \frac{\rho_i}{\rho_w} p_w - \rho_i L \ln \left(\frac{T}{2/73.15 \text{K}} \right)$$

$$L = (s_l - s_i)T$$

latent heat of melting (333.7 kJ/kg)











thermo-dynamical equilibrium (Clausius-Clapeyron equation)

$$p_i = \frac{\rho_i}{\rho_w} p_w - \rho_i L \ln \left(\frac{T}{2/73.15 \text{K}} \right)$$

ice retention curve (van Genuchten equation)

$$p_{i} = \frac{\rho_{i}}{\rho_{w}} p_{w} - \rho_{i} L \ln \left(\frac{T}{2/73.15 \text{K}} \right) \qquad S_{w} = S_{\text{res}} + (1 - S_{\text{res}}) \left[1 + \left(\frac{p_{i} - p_{w}}{P} \right)^{\frac{1}{1 - M}} \right]^{-M}$$



thermo-dynamical equilibrium

$$p_i = \frac{\rho_i}{\rho_w} p_w - \rho_i L \ln \left(\frac{T}{2 \cdot 73.15 \text{K}} \right)$$

ice retention curve

(Clausius Clapeyron equation) (van Genuchten equation)
$$p_i = \frac{\rho_i}{\rho_w} p_w - \rho_i L \ln \left(\frac{T}{2/73.15 \text{K}} \right) \qquad S_w = S_{\text{res}} + (1 - S_{\text{res}}) \left[1 + \left(\frac{p_i - p_w}{P} \right)^{\frac{1}{1 - M}} \right]^{-M}$$

$$S_{w} = S_{\text{res}} + (1 - S_{\text{res}}) \left[1 + \left(\frac{p_{i}}{\rho_{w}} \right) \frac{1}{p_{w}} - \rho_{i} L \ln \frac{T}{273.15} \right)^{\frac{1}{1 - M}} \right]^{-M}$$



thermo-dynamical equilibrium (Clausius Clapeyron equation)

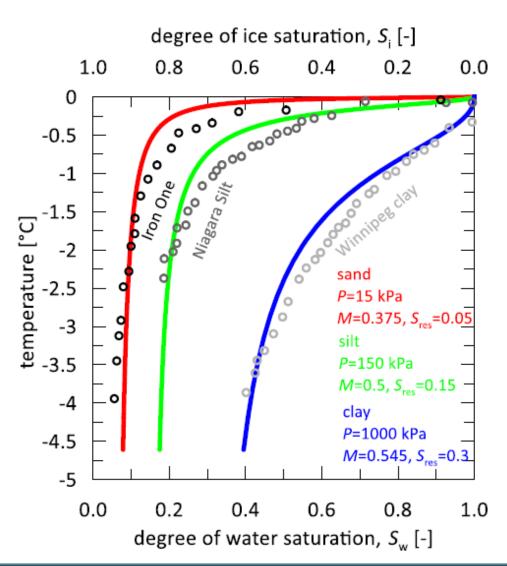
$$p_i = \frac{\rho_i}{\rho_w} p_w - \rho_i L \ln \left(\frac{T}{2/73.15 \text{K}} \right)$$

freezing retention curve (van Genuchten equation)

$$p_{i} = \frac{\rho_{i}}{\rho_{w}} p_{w} - \rho_{i} L \ln \left(\frac{T}{273.15 \text{K}} \right) \qquad S_{w} = S_{\text{res}} + (1 - S_{\text{res}}) \left[1 + \left(\frac{p_{i} - p_{w}}{P} \right)^{\frac{1}{1 - M}} \right]^{-M}$$

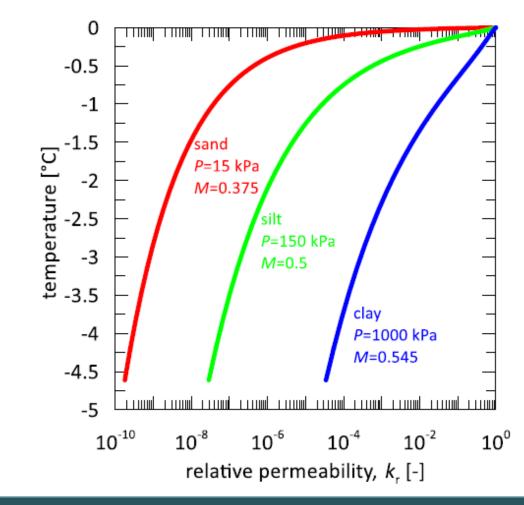
$$S_w = S_{\text{res}} + (1 - S_{\text{res}}) \left[1 + \left(\frac{-\rho_i L \ln \frac{T}{273.15}}{P} \right)^{\frac{1}{1-\mu}} \right]^{-\mu}$$





hydraulic conductivity

$$\mathbf{K} = k_r(S_w)\mathbf{K_{sat}}$$



mass balance of mineral (solid)
$$\frac{\partial}{\partial t} (\theta_s (1-n)) + \nabla (\mathbf{j}_s) = 0$$

mass balance of water (liquid and ice)

$$\frac{\partial}{\partial t} (\theta_l^w S_l n + \theta_i^w S_i n) + \nabla (\mathbf{j}_l^w + \mathbf{j}_i^w) = f^w$$

internal energy balance for the medium

$$\frac{\partial}{\partial t} (E_s \rho_s (1 - n) + E_l \rho_l S_l n + E_i \rho_i S_i n) + \nabla (\mathbf{i}_c + \mathbf{j}_{Es} + \mathbf{j}_{El} + \mathbf{j}_{Ei}) = f^Q$$

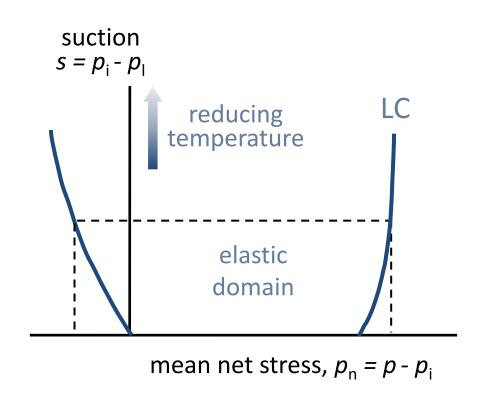
momentum balance for the medium (equilibrium)

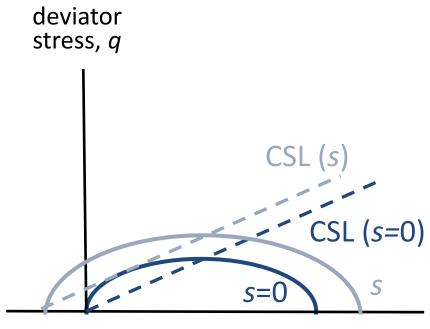
$$\nabla \boldsymbol{\sigma} + \mathbf{b} = 0$$





adaptation of BBM (two stress variable elasto-plastic model)





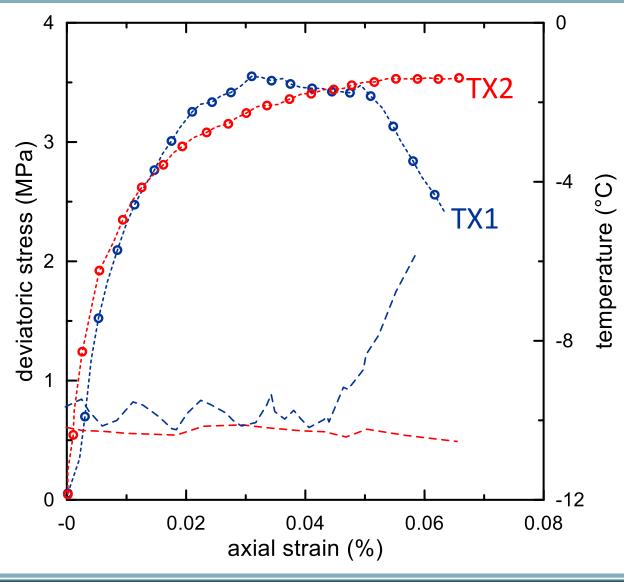
mean net stress, $p_n = p - p_i$

Nishimura et al. (2009)





COUPLED THM MODELLING TX data

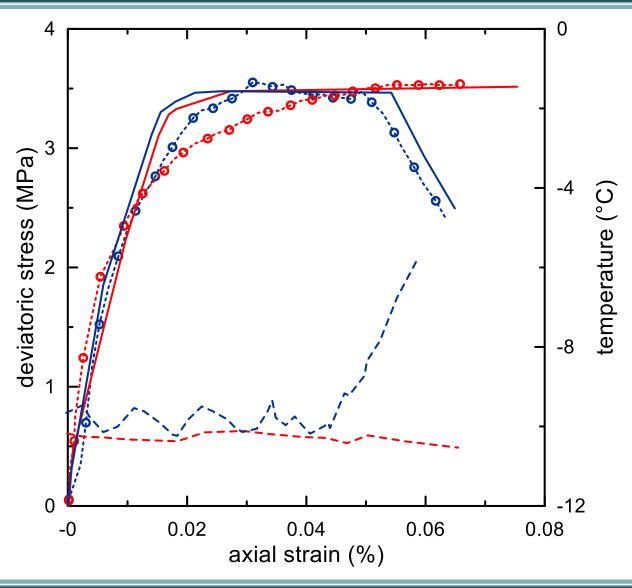


POZZOLANA

...... 200 kPa 350 kPa

 $\dot{\varepsilon}_{ax} = 0.06 \text{ mm/min}$

COUPLED THM MODELLING TX data vs model



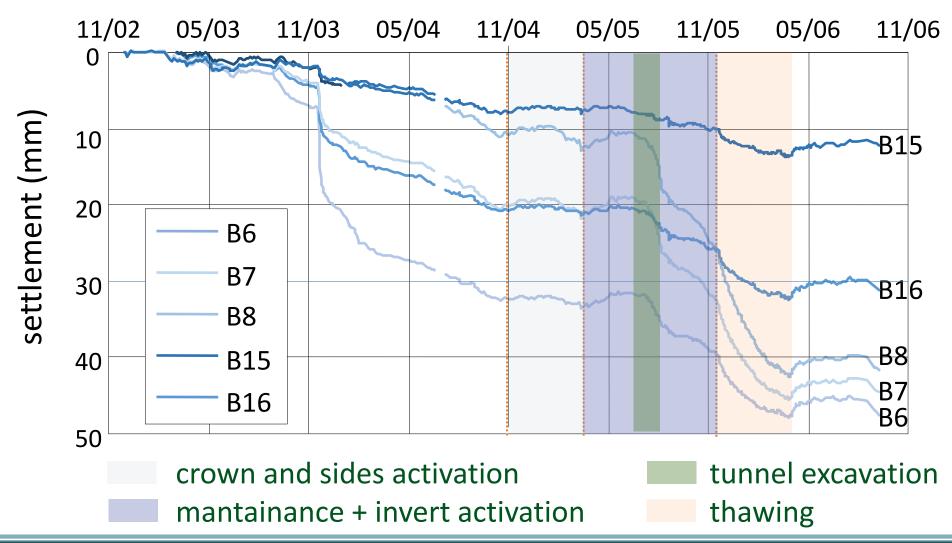
POZZOLANA

----- 200 kPa ----- 350 kPa

 $\dot{\varepsilon}_{ax} = 0.06 \text{ mm/min}$



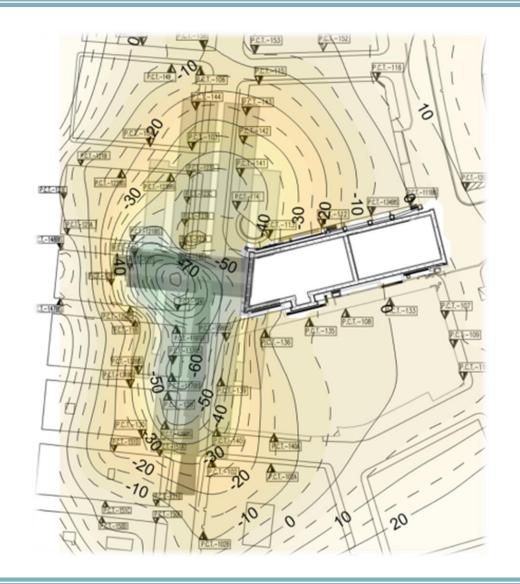
GARIBALDI surface settlements

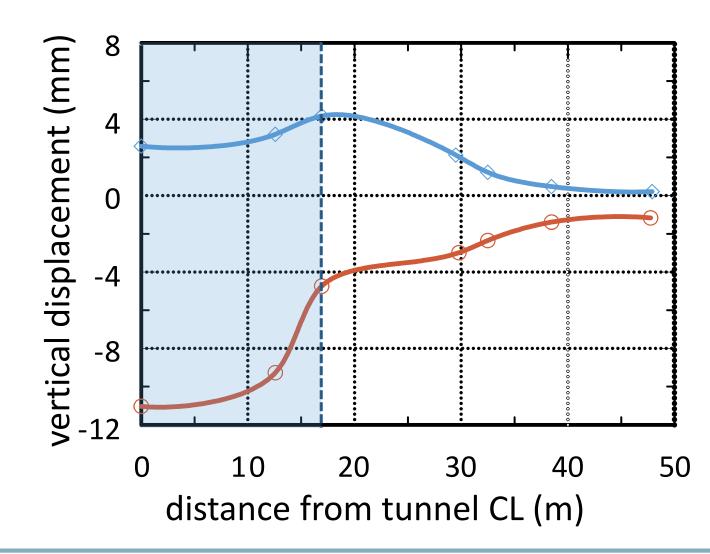






TOLEDO surface settlements

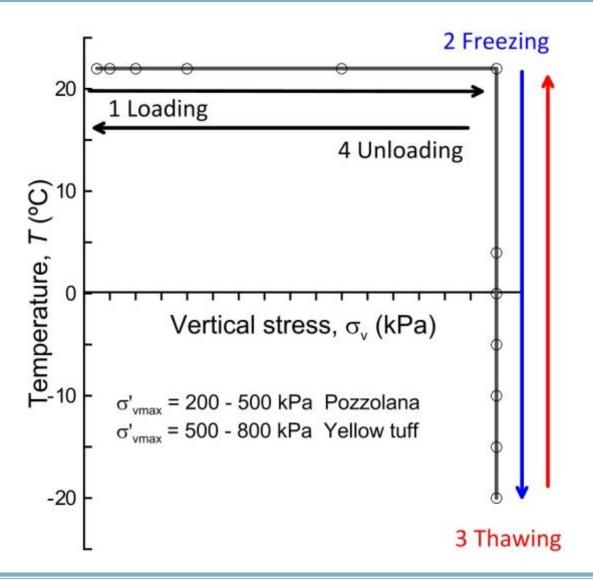








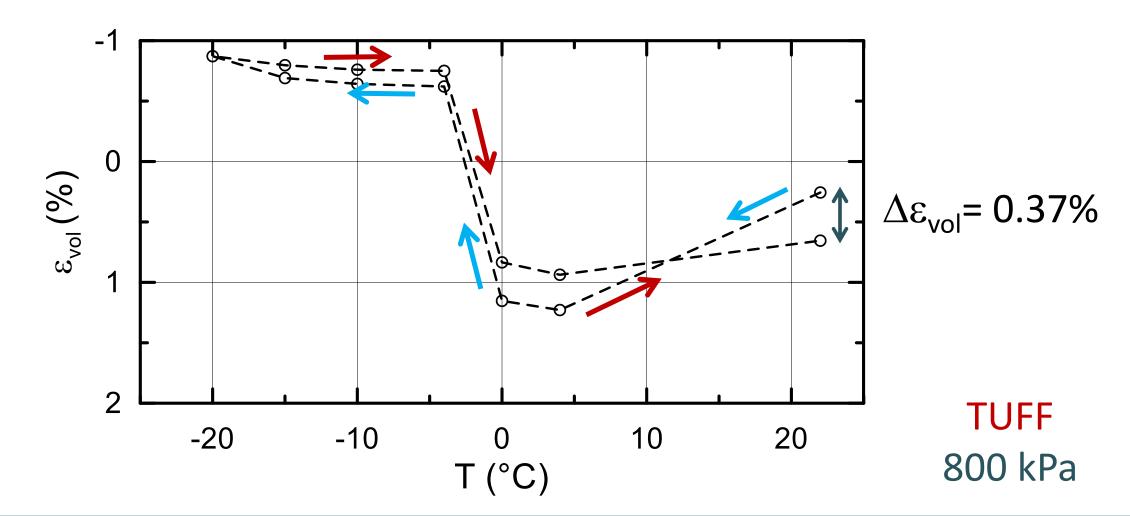
THAW BEHAVIOUR testing programme







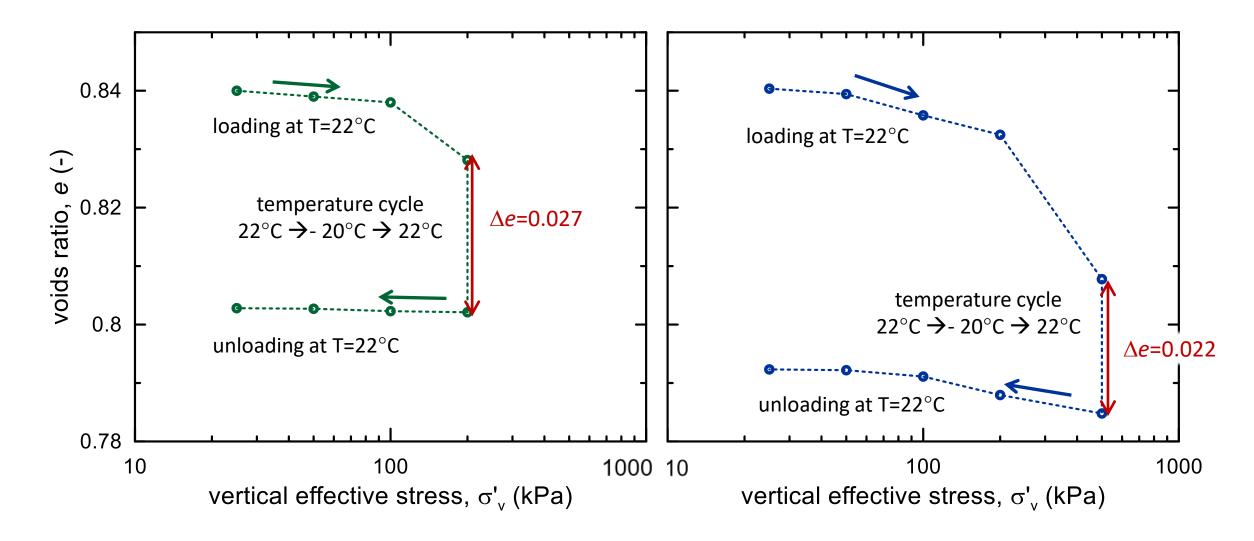
THAW BEHAVIOUR results







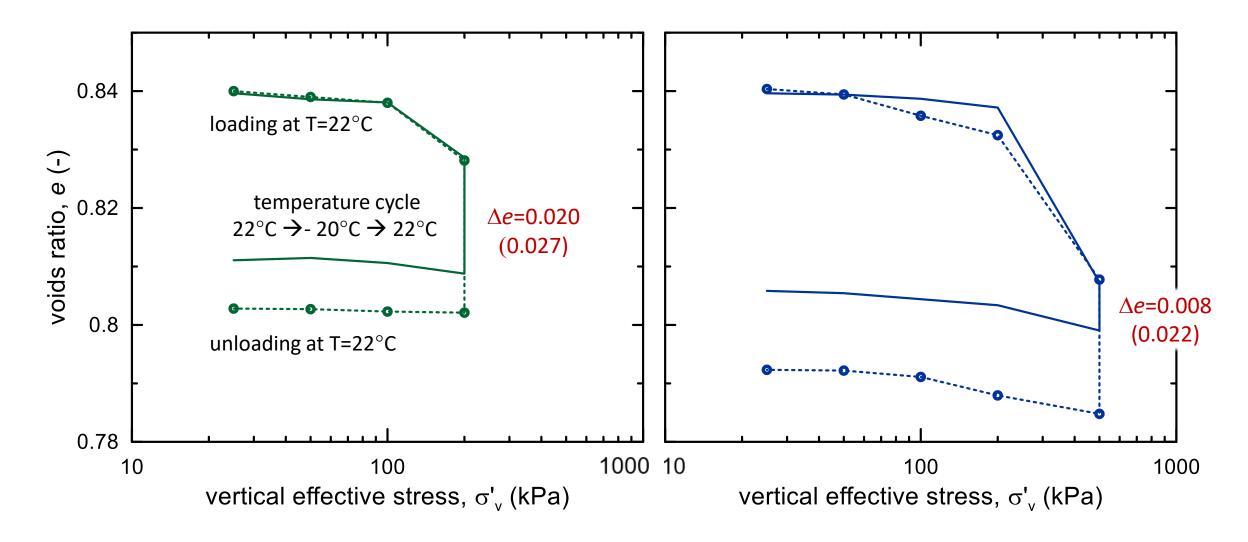
THAW BEHAVIOUR results







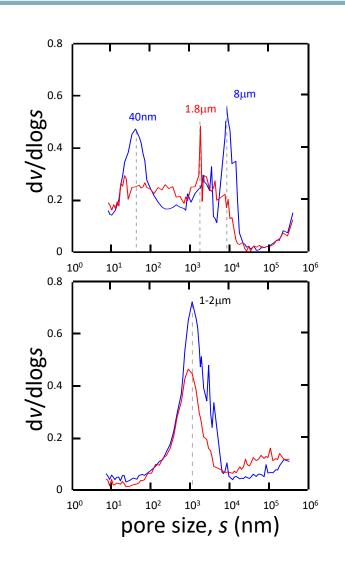
THAW BEHAVIOUR results

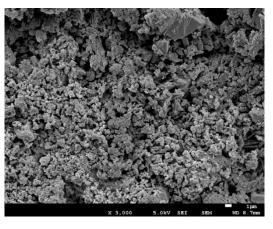


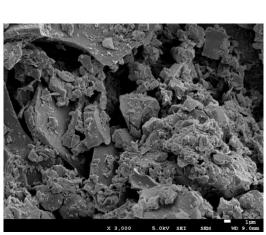




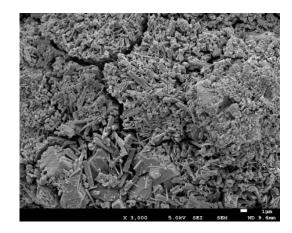
THAW BEHAVIOUR microstructure











X 3,000 2,00kV SEI SEM KI 10, 2m

after freezing



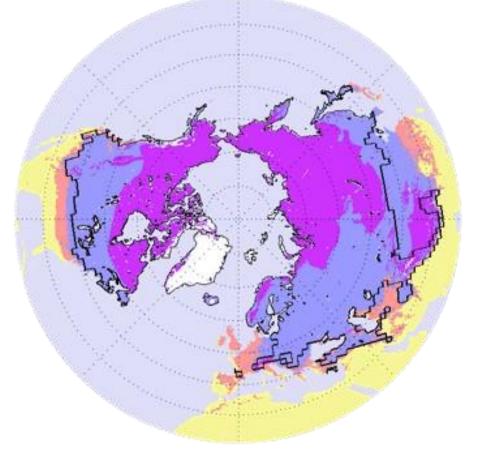
POZZOLANA





SEASONAL FREEZING/THAWING

55 to 60% of exposed land surface in northern hemisphere freezes & thaws seasonally



permanently frozen groundseasonally frozen ground (≥15 days/year)intermittently frozen ground (<15 days/year)





SEASONAL FREEZING/THAWING effects on infrastructure

irrigation canals



Li et al., 2019

road pavements

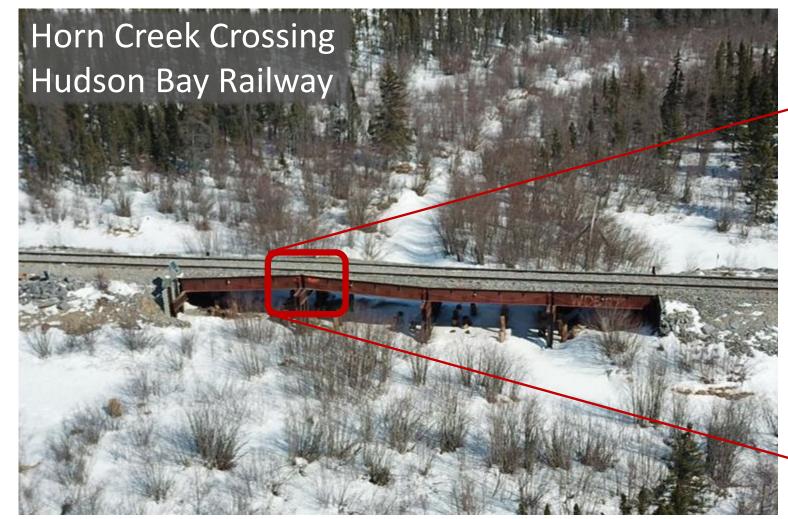


Ystenes, 2011





SEASONAL FREEZING/THAWING effects on infrastructure



bridges



Arpin, Beddoe & Take (2023)





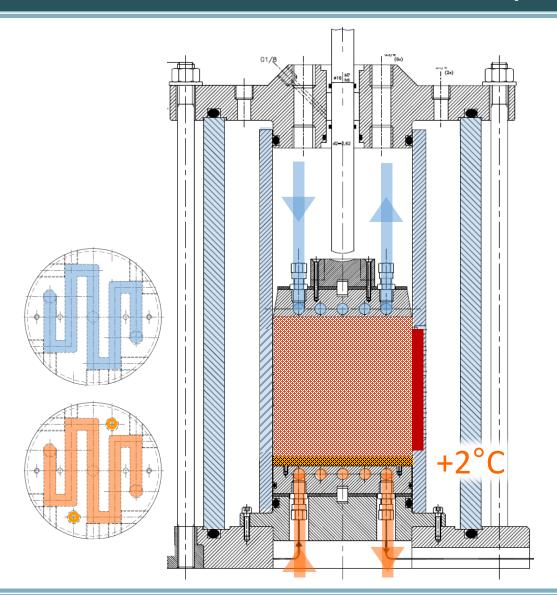
THAW BEHAVIOUR equipment

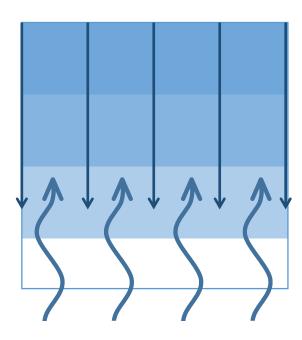






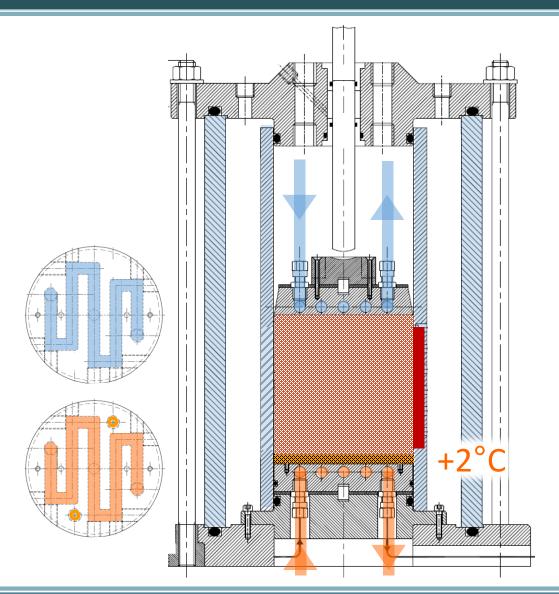
FROST HEAVE APPARATUS (FHA)

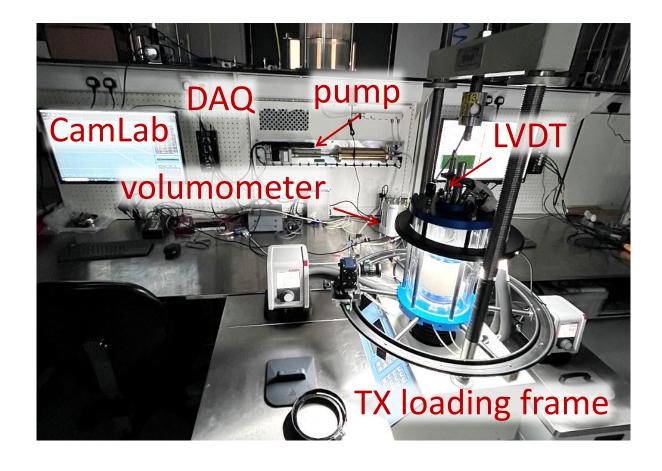






FROST HEAVE APPARATUS (FHA)









(PSEUDO) 3D PHOTOGRAMMETRIC MODEL



DaHeng Vision MARS1231 camera (1/3 sample surface)

"one-shot" calibration (constant radius constraint)

new photogrammetric model cell wall-induced distortions

Stanier & Lattuada



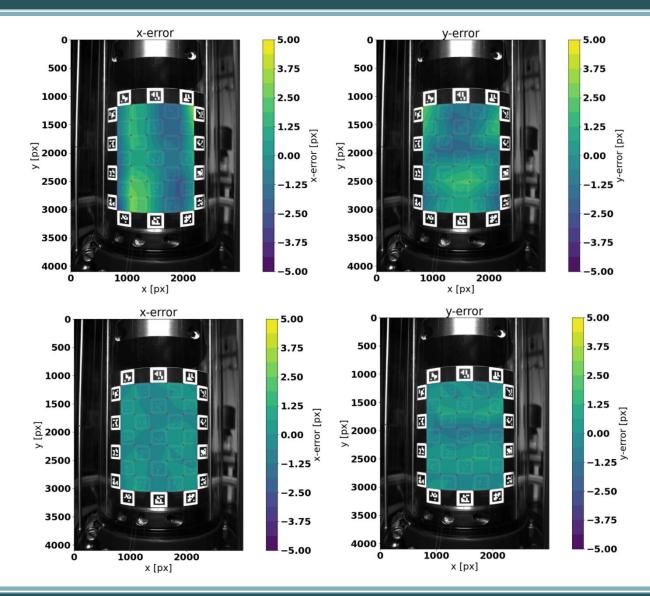


(PSEUDO 3D) PHOTOGRAMMETRIC MODEL

OpenCV model exhibits systematic residual errors

newly implemented cubic model reduces errors by ~66%

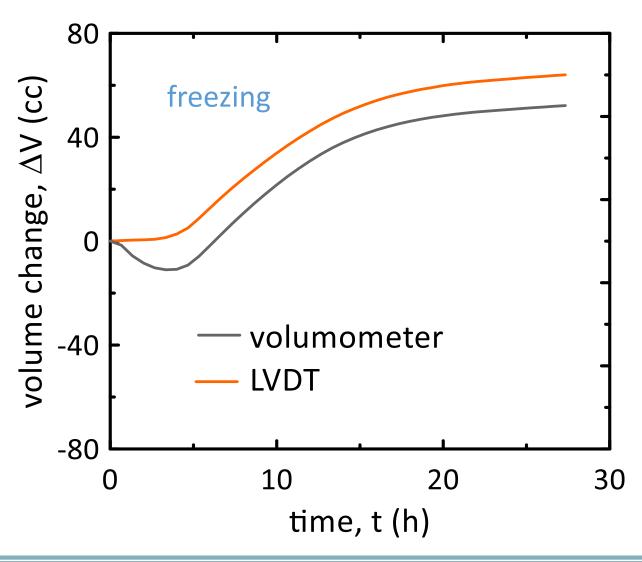
precision in the micron range possible







FREEZING



50% Kaolin + 50% Hostun Sand

vertical stress: $\sigma_v = 100$ kPa

head temperature: +20°C to -10°C

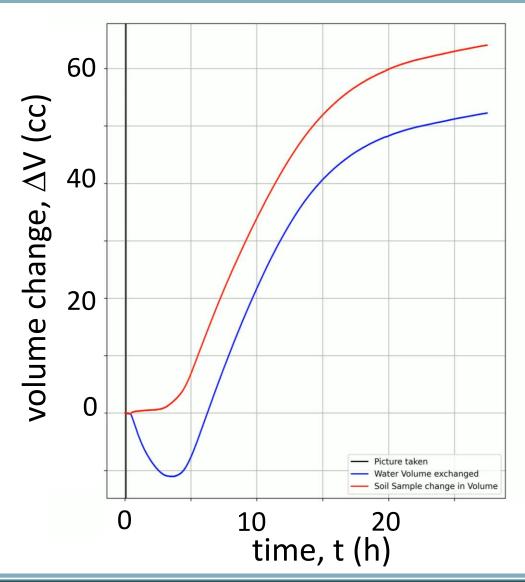
base temperature: +2°C

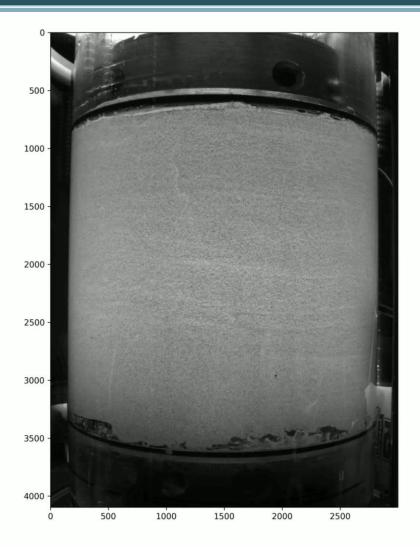
free drainage: $u_{base} = 0$





FREEZING

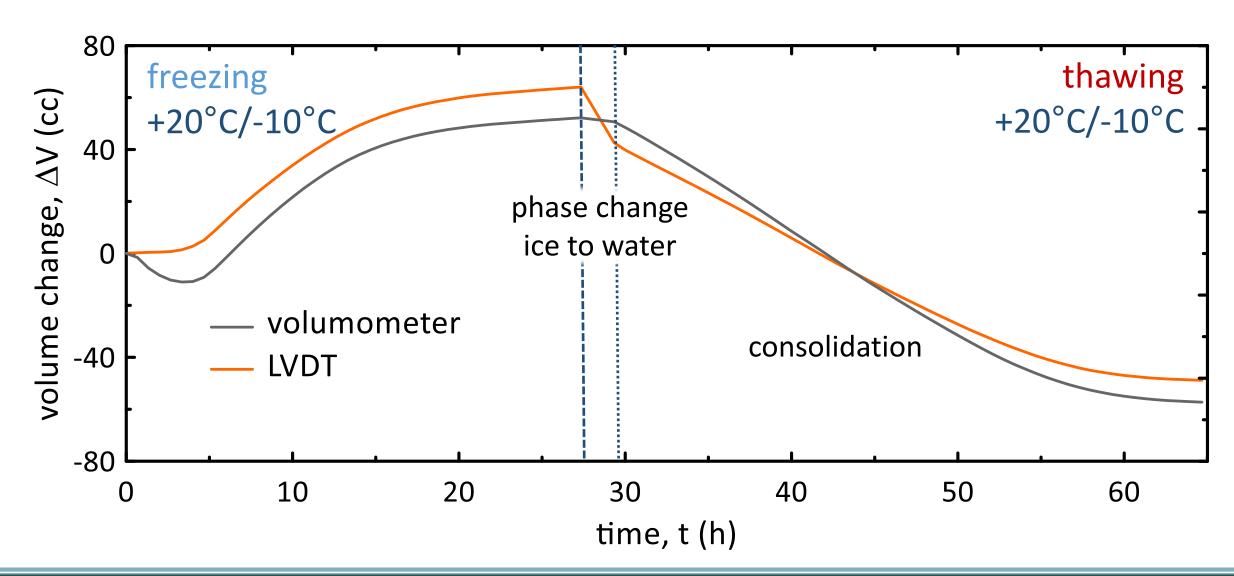








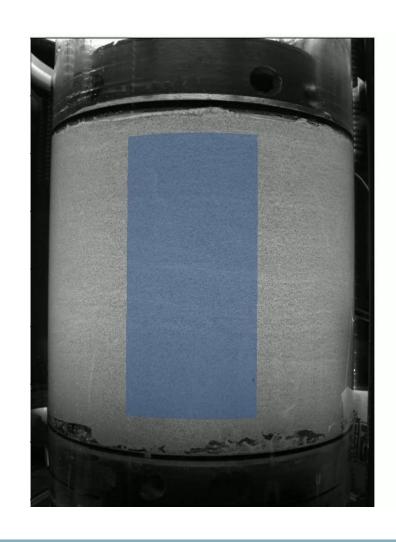
FREEZING/THAWING 50%K-50%S -100kPa

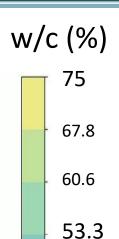






w/c contours by PIV





46.1

38.9

31.7

24.4

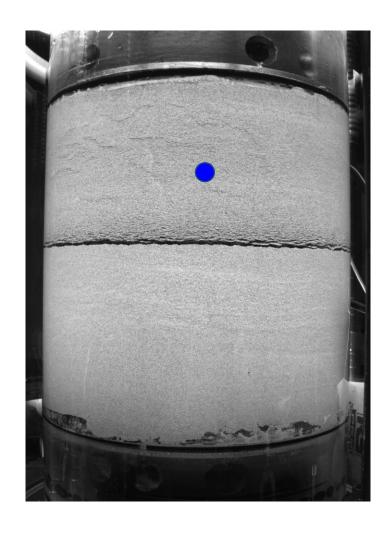
17.2

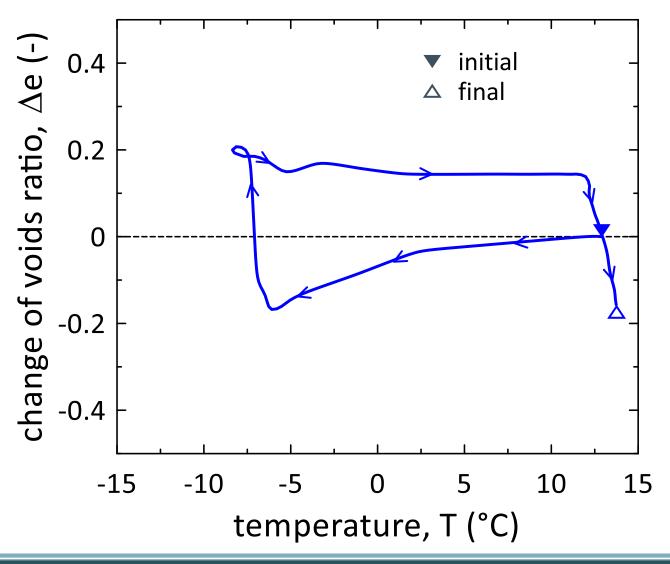
10.0

initial w/c $\approx 32\%$

final w/c $\approx 24\%$

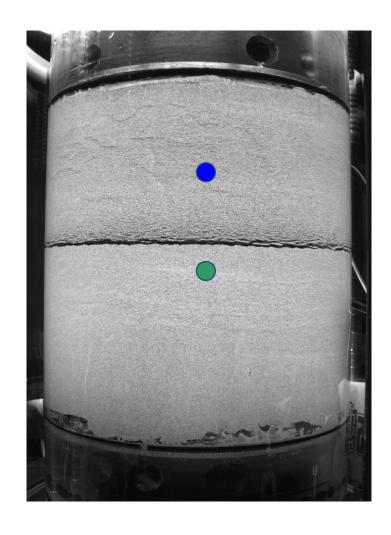
FREEZING/THAWING

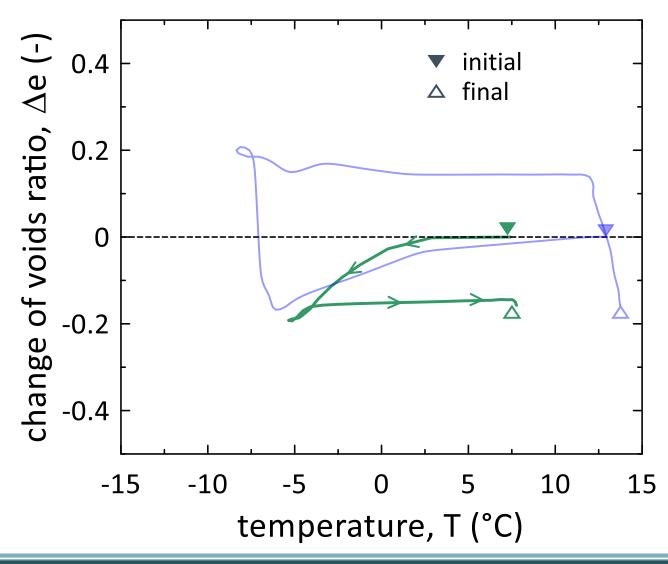






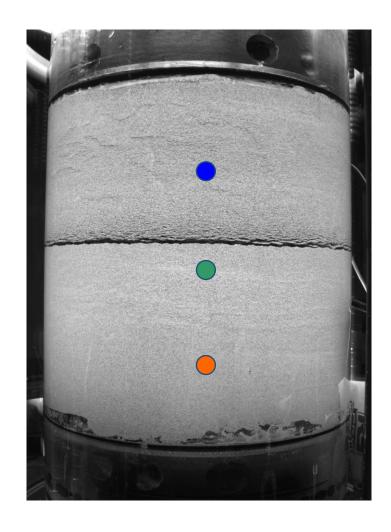
FREEZING/THAWING

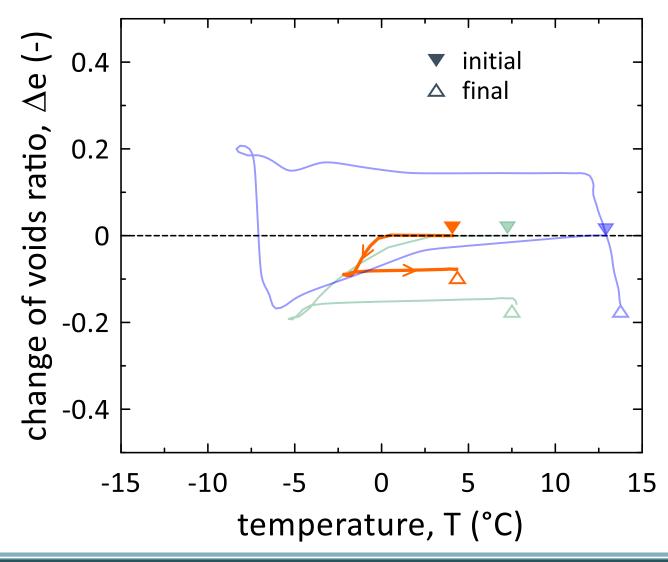






FREEZING/THAWING

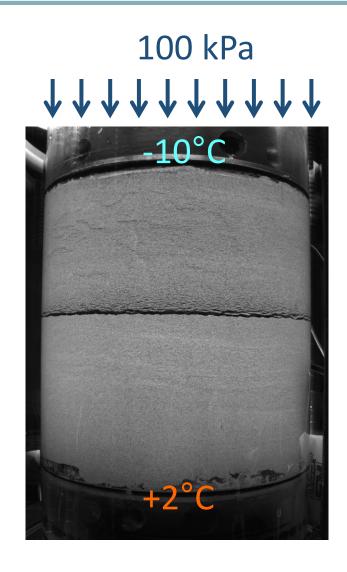


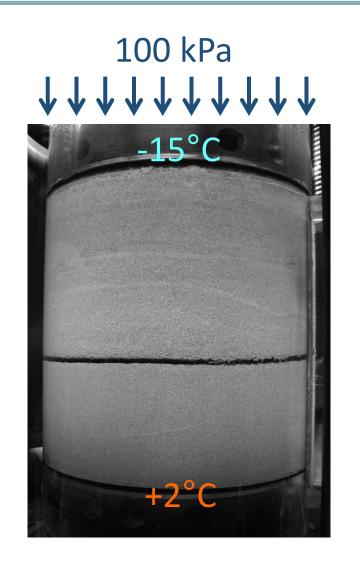






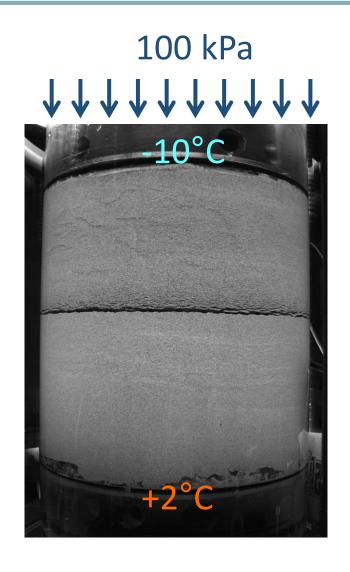
thermal BC

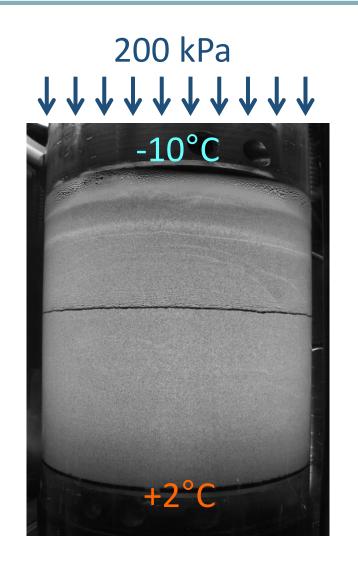






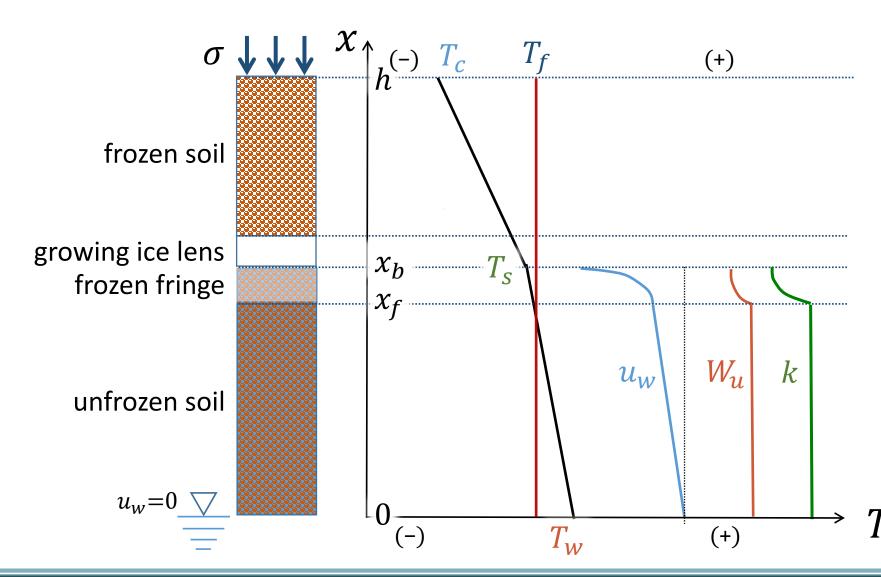
mechanical BC







FROST HEAVE SUSCEPTIBILITY



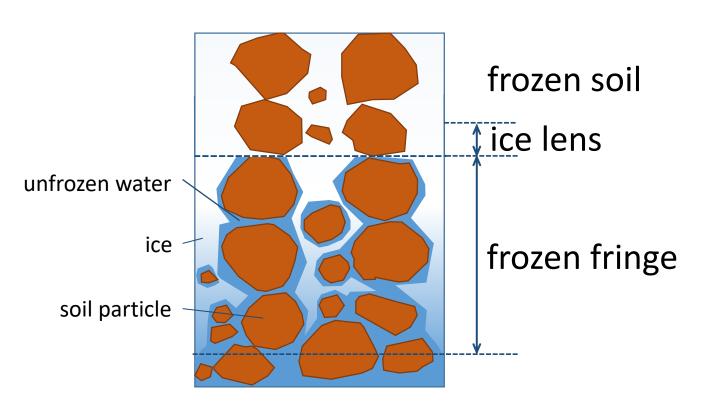
$$\frac{u_w}{\rho_w} - \frac{u_i}{\rho_i} = L \ln\left(\frac{T}{T_0}\right)$$

Daichao Sheng et al. (1995)





ICE LENS INITIATION

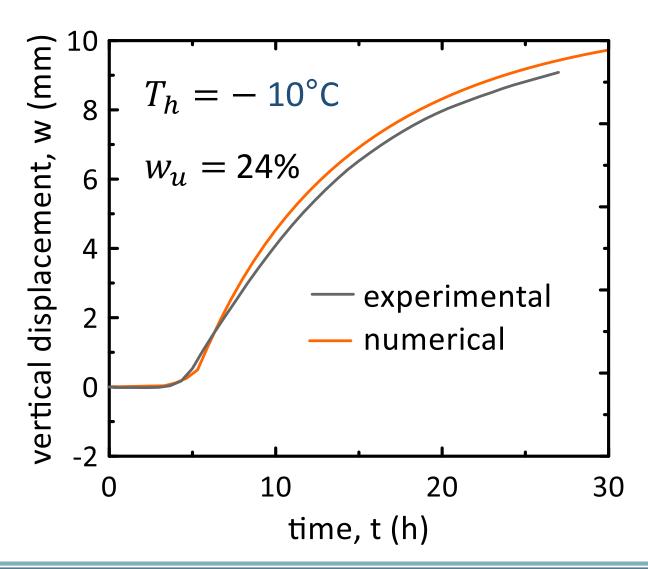


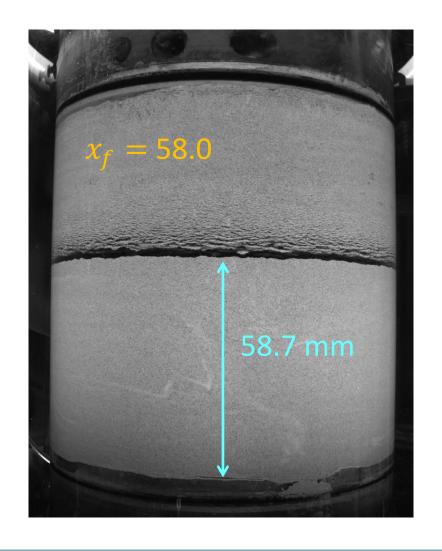
$$\sigma' = \sigma - u_n$$

$$u_n = \frac{n - I}{n} u_w + \frac{I}{n} u_i$$



ICE LENSING





Pico RP2040 based I2C wireless data acquisition



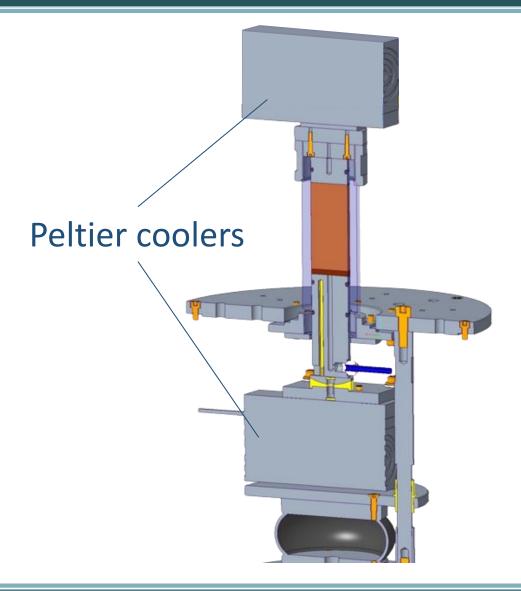


measurement of suction

TE MS5837-02BA

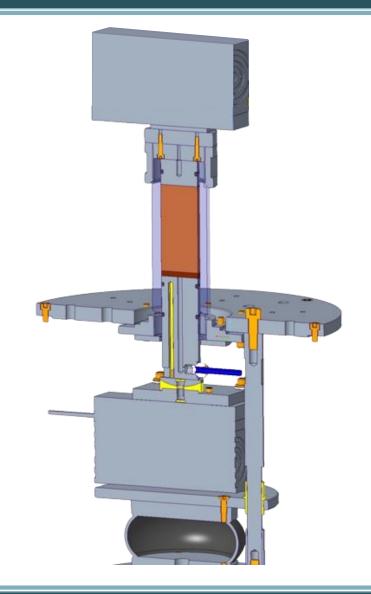
3.3×3.3×2.75 mm

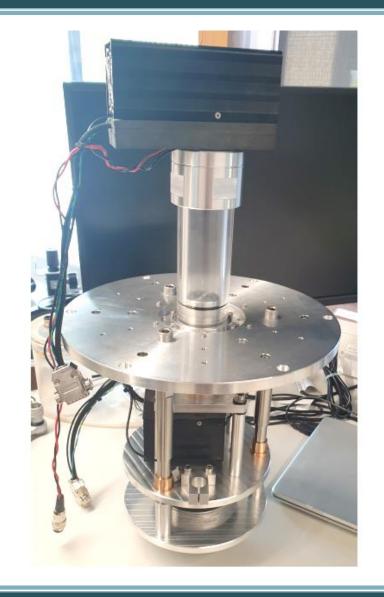




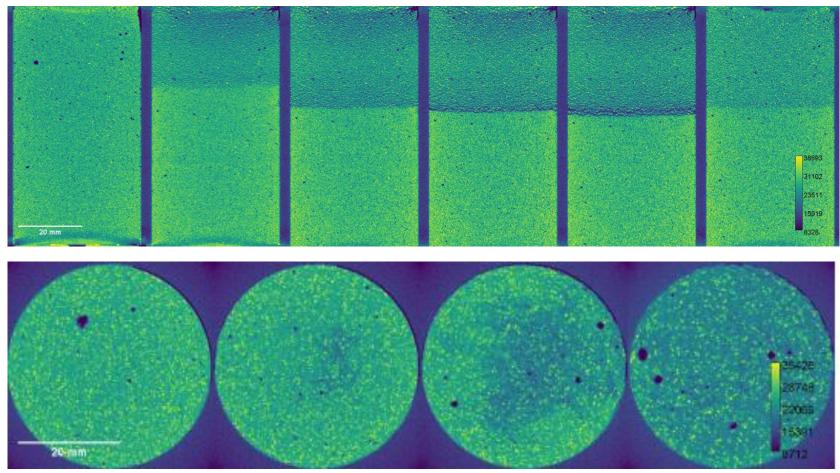
miniature X-Ray transparent FHA









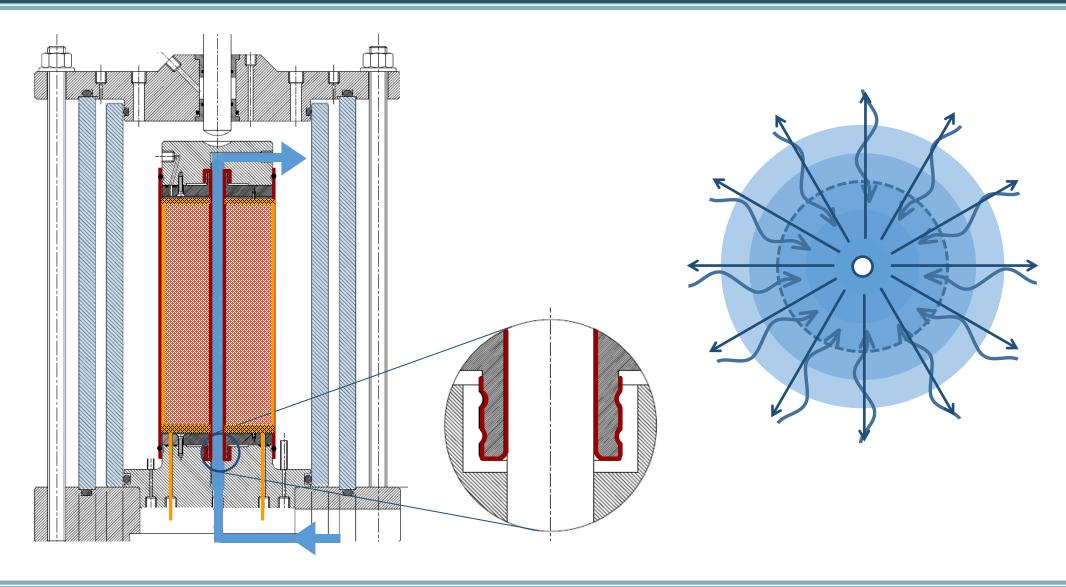


Tom Mlady MSc (2023) Cino Viggiani, Giulia Guida





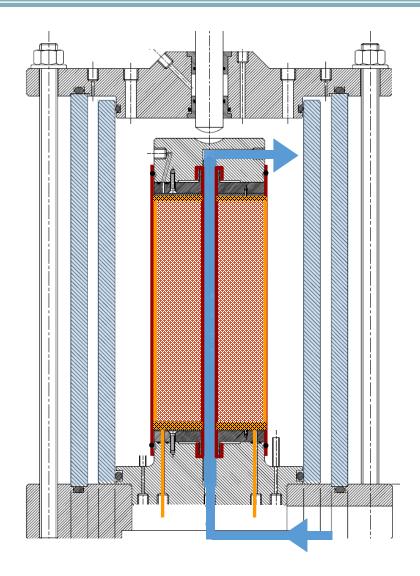
WHAT'S NEXT? THM-TX







WHAT'S NEXT? THM-TX







WHAT'S NEXT? THM-TX

true 3D imaging system

originally developed @ UWA

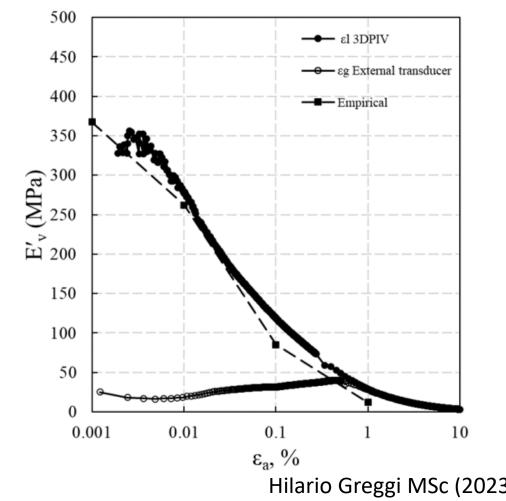
Raspberry Pi Zero W and HQ camera modules

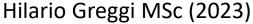
UDP controlled acquisition via Python scripts

PIV-driven - stereophotogrammetry

all codes available on GitHub

displacements resolved to µm precision comparable with internal local gauges









CONCLUSIONS

relevance underground construction - AGF

climate change induced seasonal freezing and thawing

monitoring construction effects/ control processes

collect evidence

analysis data reduction

modelling

THM coupling volume expansion on freezing driven by

mass transfer under temperature gradients

equipment thermal & hydraulic boundary conditions

full field measurements of deformations by PIV





[...] Many of his research interests were motivated by his consulting activities wherein the state of the art fell short of explaining performance. [...]

Milton Harr (1998)



