

Parametric Sensitivity and Thermal Runaway Behavior in Catalytic Fixed-Bed Reactors



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Parametric Sensitivity in Chemical Systems

Effect of wall temperature on

Temperature profiles

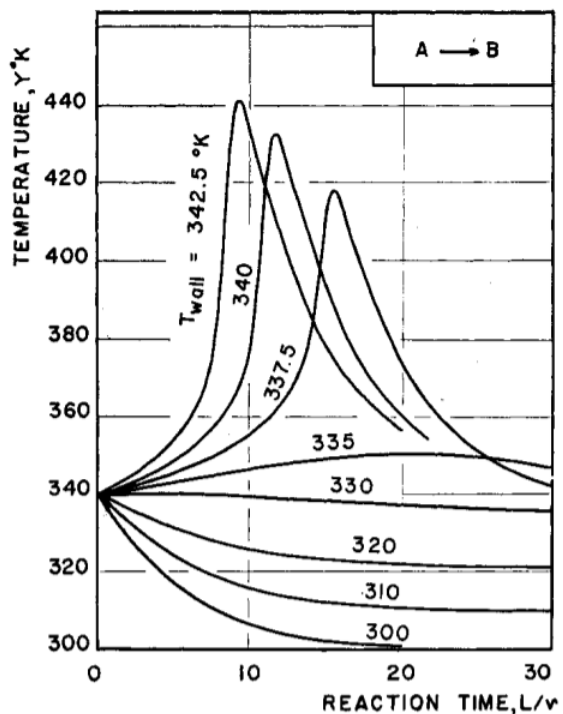


Fig. 2a. Temperature profiles in a tubular reactor; effect of wall temperature. $E = 22,500$, $p = 3.94 \times 10^{12}$, $x_i = 0.20$, $Q = 7,300$, $K = 0.20$, $T_i = 340^\circ\text{K}$.

Concentration profiles

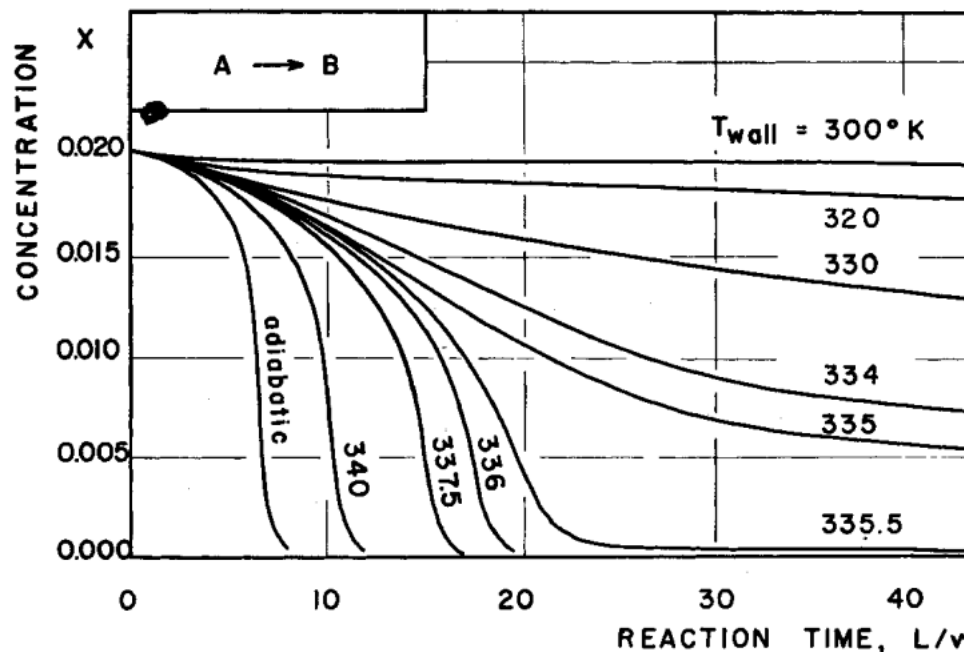


Fig. 2b. Concentration profiles in a tubular reactor; effect of wall temperature. Data are the same as in Figure 2a.

O. Bilous and N. R. Amundson, *AIChE J.*, 1 (1955), 513-521 (CSTR)

O. Bilous and N. R. Amundson, *AIChE J.*, 2 (1956), 117-126 (PFR)

Parametric Sensitivity in CSTRs

Unique steady states

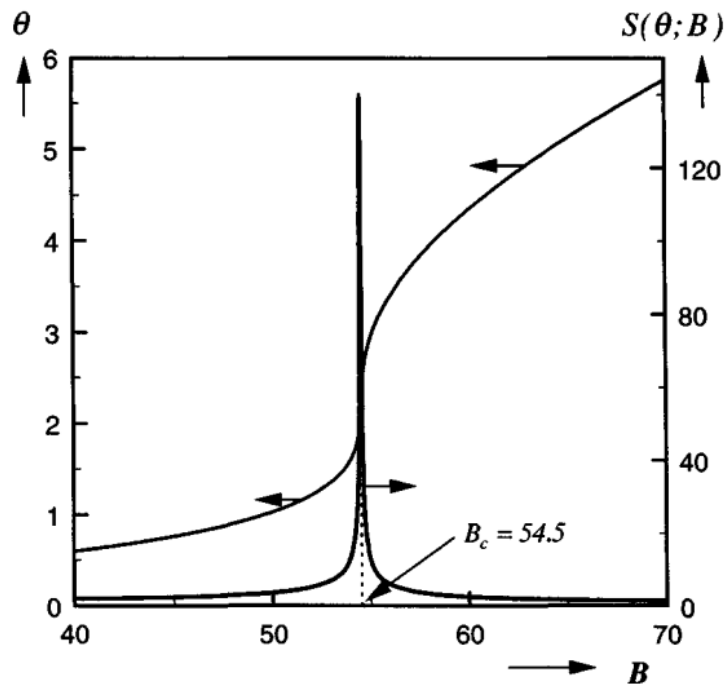


Figure 5.1. Reactor temperature θ and its normalized sensitivity $S(\theta; B)$ as functions of the heat-of-reaction parameter B for a CSTR operating in the region of unique steady states. $Da = 0.11$; $\gamma = 20$; $St = 10$; $n = 1$; $\theta_{co} = 0$. From Chemburkar *et al.* (1986).

Multiple steady states

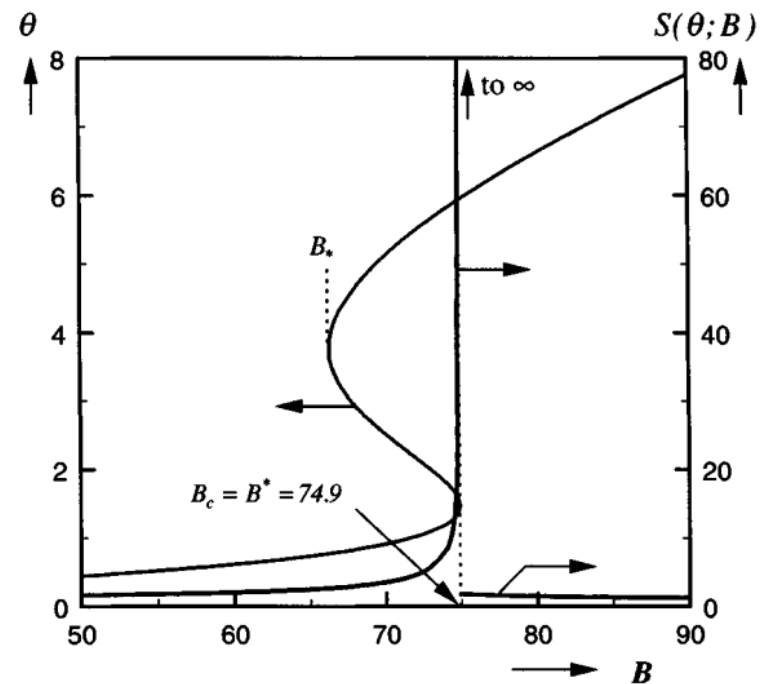
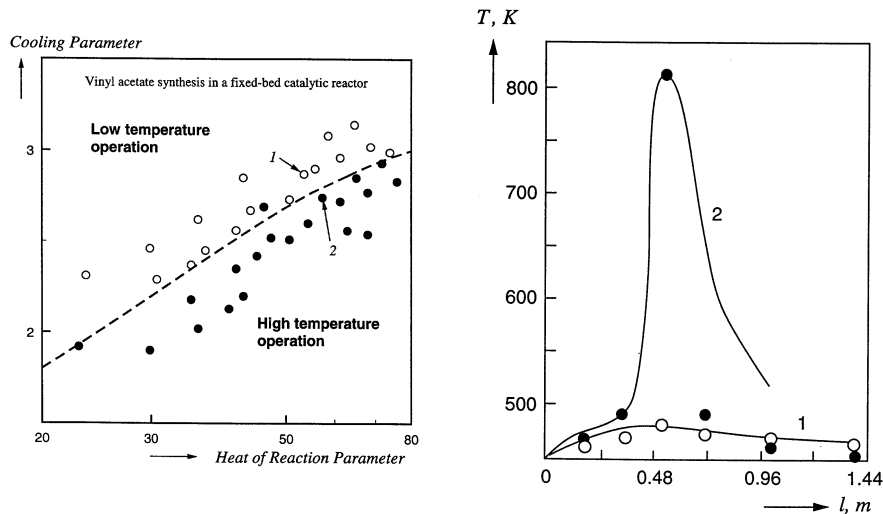


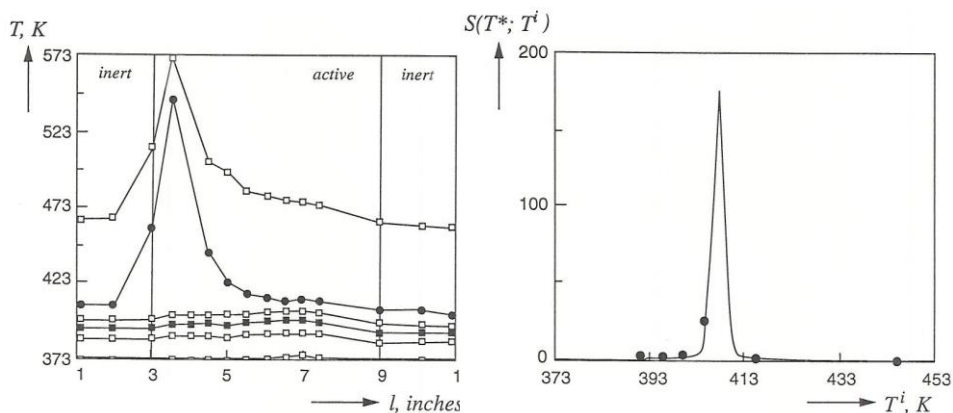
Figure 5.2. Reactor temperature, θ , and its normalized sensitivity, $S(\theta; B)$, as a function of the heat of reaction parameter, B , for a CSTR operating in the region of multiple steady states. $Da = 0.07$; $\gamma = 20$; $St = 10$; $n = 1$; $\theta_{co} = 0$. From Chemburkar, *et al.* (1986).

Parametric Sensitivity in Fixed-Bed Reactors

Vinyl Acetate Synthesis



CO Oxidation



G. Emig, H. Hofmann, U. Hoffmann and U. Fiand, *Chem. Eng. Sci.*, 35 (1980), 249-257

A. Varma, M. Morbidelli and H. Wu, *Cambridge University Press*, (1999; 2005)

E. G. Bauman, and A. Varma, *Chem. Eng. Sci.*, 45 (1990), 2133-2139

Other Topics Investigated

- ❑ Selectivity/Yield Issues:
Parallel or Consecutive Reactions
- ❑ Polymerization Reactions
- ❑ Sensitivity Analysis in Air Pollution
- ❑ Sensitivity Analysis in Metabolic Processes
- ❑ Sensitivity Analysis of Combustion Synthesis
- ❑ Model Reduction via Sensitivity Analysis

~20 original research papers and monograph:

A. Varma, M. Morbidelli and H. Wu, *Cambridge University Press*, (1999; 2005)

A recent example: Low-temperature oxidation of methanol

40% methanol used for formaldehyde production

Industrial Processes

- **Mo-Fe:**
250-400 °C, $S=95\%$, $X=98\%$
- **Ag:**
560-600 °C, $S=70\%$, $X=90\%$
- **Other catalysts:**
 VO_x , Cr-Mo, MoO_3 , etc. $T=300-500$ °C

Target

- *High selectivity ($S > 90-95\%$) at low temp ($< b.p.$).*
- *Long catalyst lifetime*

S = selectivity to formaldehyde
 X = methanol conversion

Table 5
Representative product compositions of methanol low-temperature oxidation under standard operating conditions.

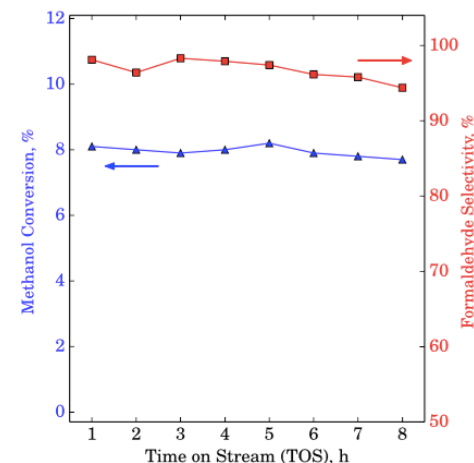
Product, wt%	1% Pt	1% Pt-0.5% Bi	2% Bi
Methanol	89.6	91.9	99.4
Formaldehyde	0.01	7.95	0.06
Methyl formate	2.44	0.03	0.21
Dimethoxymethane	1.08	0.01	0.12
Formic acid	2.39	0.06	0.16
CO ₂	4.48	0.05	0.05

70°C, 1 atm, 0.02 g catalyst, methanol feed rate 0.6 mL/h (liquid, at room temperature), preheated at 70 °C before entering the reactor, total gas flow rate 100 mL/min
methanol b.p.= 65 °C

Y. Xiao, Y. Wang and A. Varma, *J. Catal.*, 363 (2018), 144

Initial test

Stability

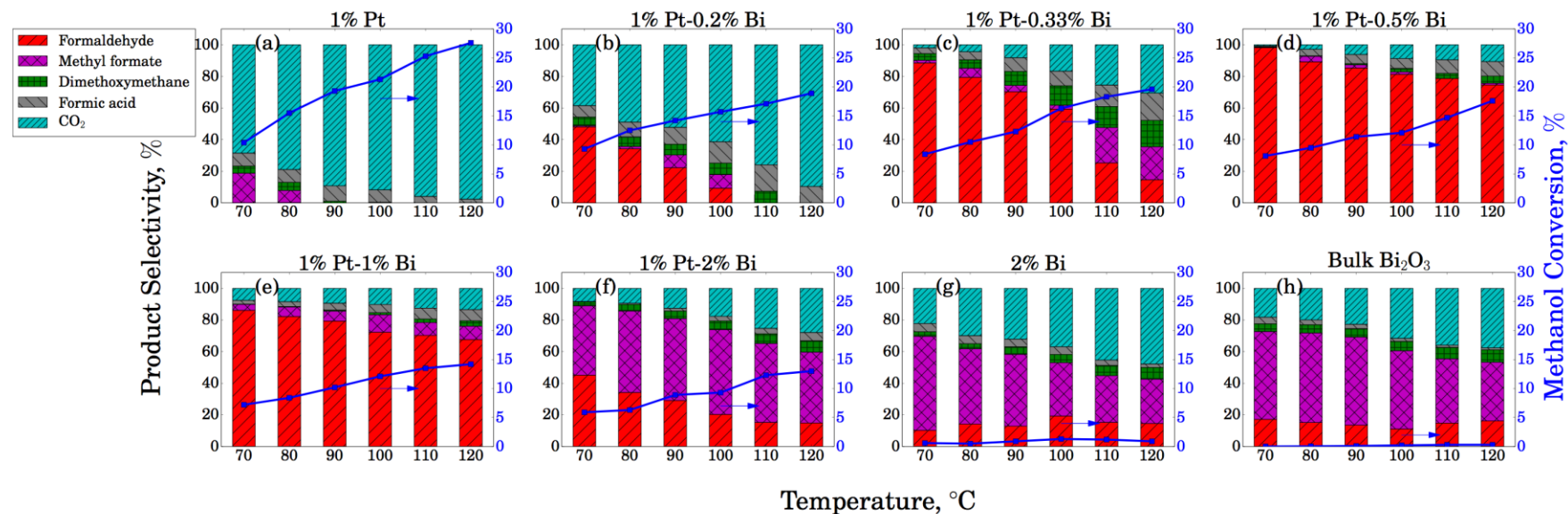


Effect of Bi addition

→ Bi addition to Pt [1]

Tune selectivity for alcohol oxidation, e.g. glycerol to 1,3-dihydroxyacetone

→ Effects of Bi loading and Temperature [2]



Methanol conversion and selectivity toward formaldehyde over various catalytic materials, (a)–(f) referring to 1% Pt- y % Bi catalysts, when y = (a) 0, (b) 0.2, (c) 0.33, (d) 0.5, (e) 1, (f) 2; (g) for 2% Bi and (h) for bulk Bi_2O_3 .

1. Y. Xiao et al., *AIChE J.*, 63 (2017), 705

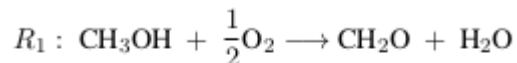
2. Y. Xiao, Y. Wang and A. Varma, *J. Catal.*, 363 (2018), 144

Trend to Runway

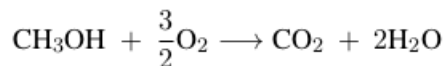
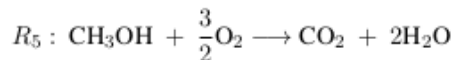
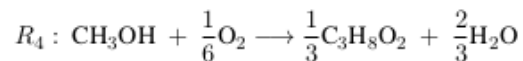
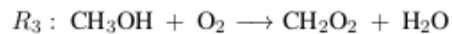
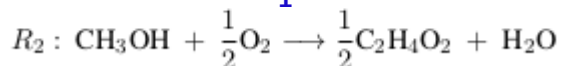
Kinetics and thermodynamics

Table 2: Kinetic and Thermodynamic Parameters over the 1% Pt-0.5% Bi Catalyst

step	R ₁	R ₂	R ₃	R ₄	R ₅
carbon-containing product	CH ₂ O	C ₂ H ₄ O ₂	CH ₂ O ₂	C ₃ H ₈ O ₂	CO ₂
$n_{(i,1)}$	1	1	1	1	1
$n_{(i,2)}$	1	1	1	1	1
E_{a_i}	15.6×10^3	158.0×10^3	95.6×10^3	164.3×10^3	76.9×10^3
A_i	4.35	8.05×10^{16}	4.83×10^{10}	5.24×10^{18}	1.65×10^8
k_i at 343 K	1.86×10^{-2}	6.93×10^{-8}	1.32×10^{-4}	4.97×10^{-7}	3.24×10^{-4}
k_i at 393 K	3.73×10^{-2}	7.99×10^{-5}	9.38×10^{-3}	7.58×10^{-4}	1.00×10^{-2}
ΔH_{r_i}	-179.5×10^3	-217.1×10^3	-419.5×10^3	-76.3×10^3	-676.2×10^3



$$\Delta H_1 = -180 \text{ kJ/mol}$$



$$\Delta H_5 = -676 \text{ kJ/mol}$$

Side reaction:

- strong exothermic
- runaway trend

$$r_i = k P_{\text{CH}_3\text{OH}}^{n_{(i,1)}} P_{\text{O}_2}^{n_{(i,2)}}$$

$$P_j = \frac{P_0}{F_0} F_j$$

Fits of kinetics

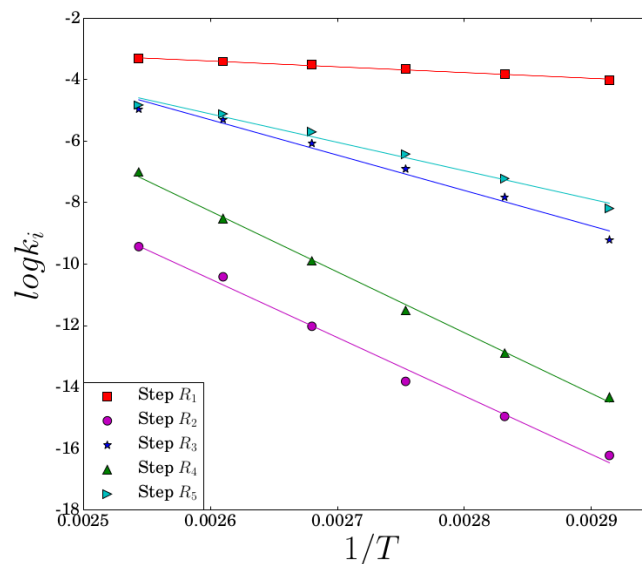
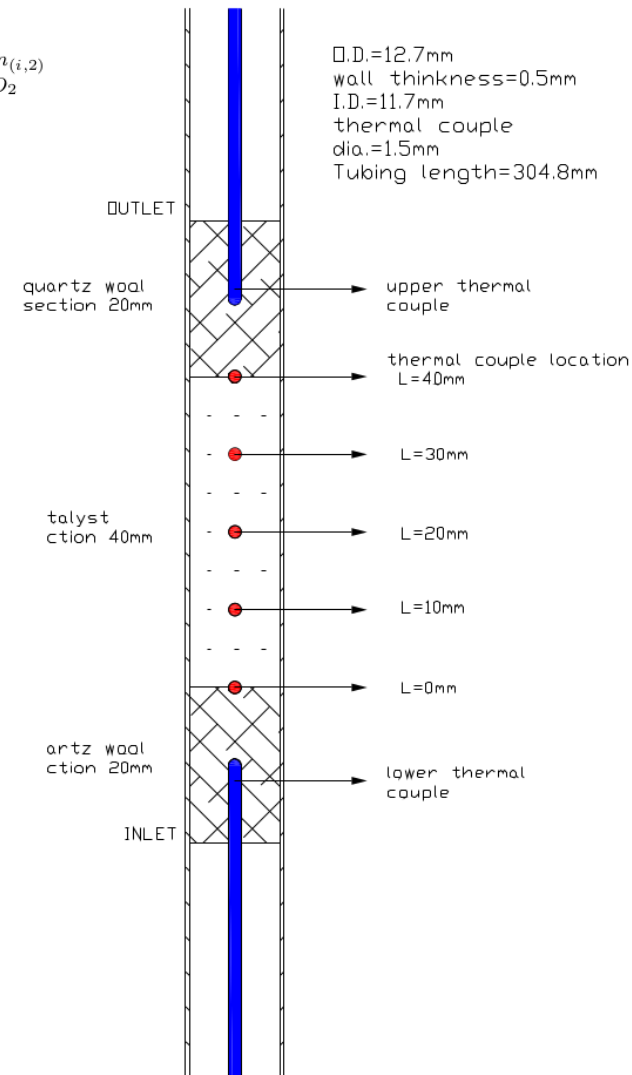


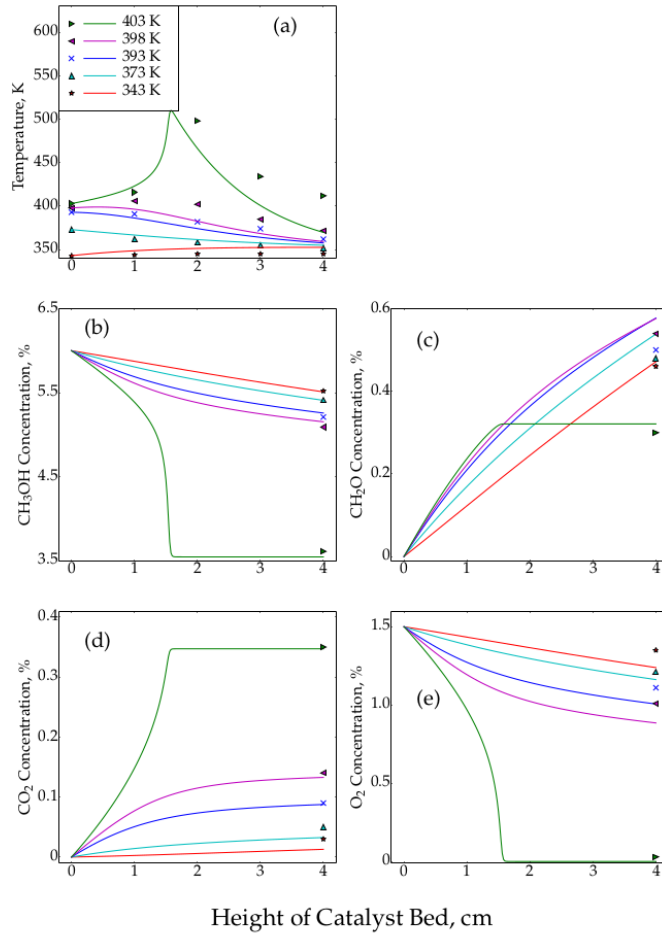
Figure 3: Arrhenius Plots for Rate Constants under Standard Operating Conditions ($T_0=343\text{-}393 \text{ K}$)

Reactor configuration

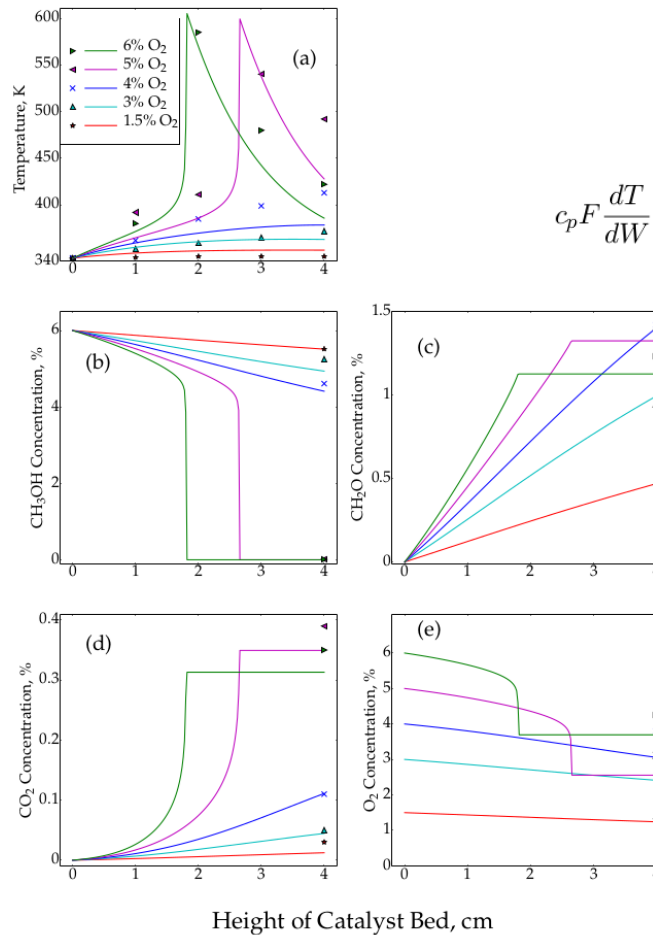


Runaway: Experiment and Theory

Feed temperature effect



O₂ concentration



One-dimensional model

$$\frac{dF_j}{dW} = \sum_{i,j=1}^{i=5,j=9} \alpha_{(i,j)} r_i$$

$$c_p F \frac{dT}{dW} = \sum_{i=1}^{i=5} (-\Delta H_{ri}) \cdot r_i - \frac{4U}{d_t \rho_{cat}} (T - T_c)$$

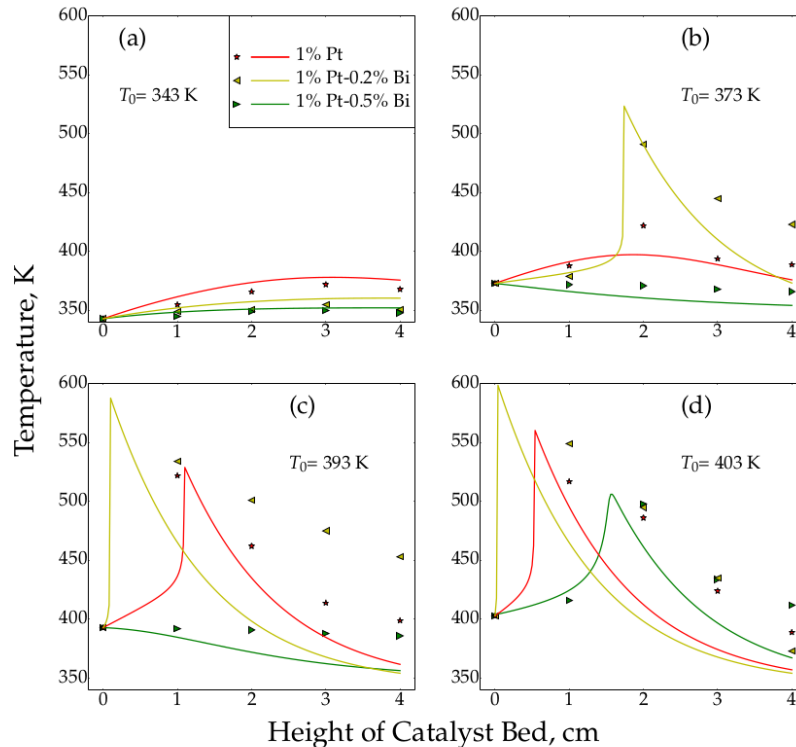
$$\frac{1}{U} = \frac{1}{\alpha_i} + \frac{d}{\lambda} \frac{A_b}{A_m} + \frac{1}{\alpha_u} \frac{A_b}{A_u}$$

Comparison for Experiments and Model Predictions under Standard Operating Conditions over the 1% Pt-0.5% Bi Catalyst for (a) Temperature Profile, (b) CH₃OH Concentration, (c) CH₂O Concentration, (d) CO₂ Concentration (e) O₂ Concentration

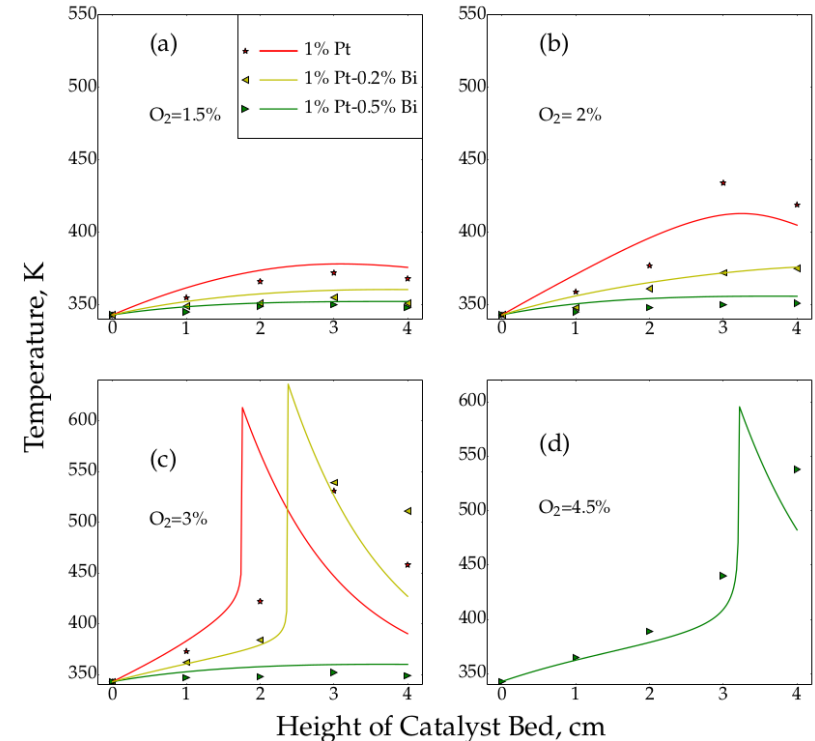
The onset of reactor runaway predicted successfully

Runaway: Caused by catalyst design

Effect of feed temperature



Effect of O₂ concentration



Sensitivity of Catalyst Design: Reactor Thermal Runaway under Standard Operating Conditions

The onset of reactor runaway predicted successfully

Effects of Bi addition:

- *Tuning selectivity to target product*
- *influencing reactor thermal behavior*

Thank You!