



# Unexpectedly High Corrosion Rates Caused by Chlorinating Agents in the Presence of Acetonitrile: Importance of Corrosion Testing for Safe Scale-Up

Yamini Krishnan, Jayachandran Devaraj, Paul Speakman, Kelsi Goshinsky, Aaron Shinkle, Ajit Mishra, John Doyle III, Abraham Schuitman

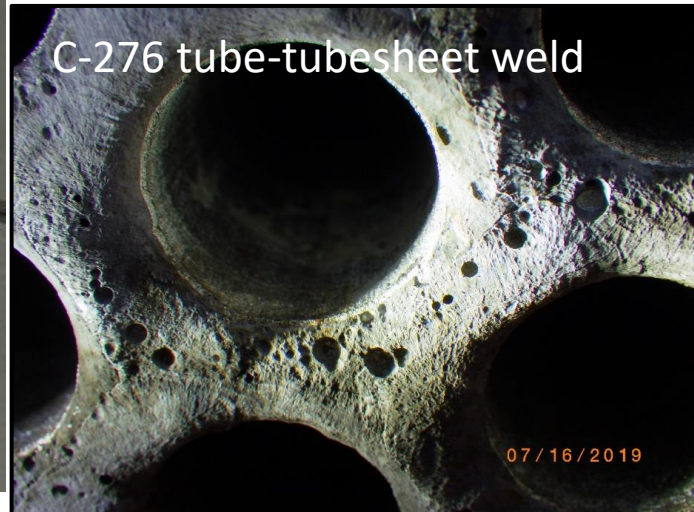
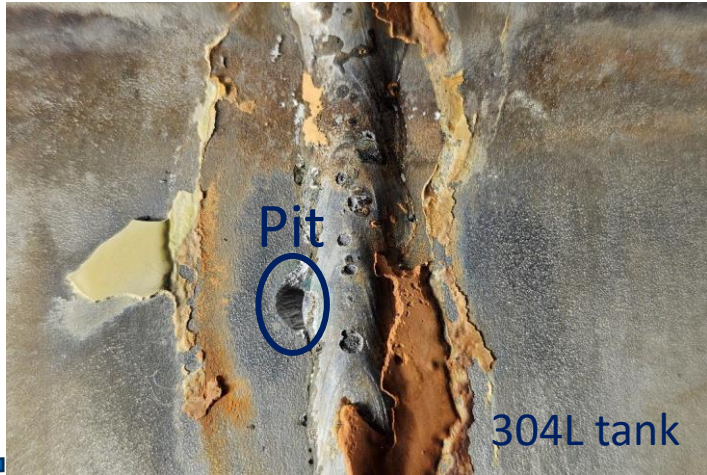
PURDUE PROCESS SAFETY & ASSURANCE CENTER SPRING CONFERENCE  
MAY 8, 2024

# Applications of Metals/Alloys in the Chemical Industry





# Safety Risks Associated with Corrosion



Damage in components can result in product leaks and unexpected shutdowns

# Understanding Corrosion Can Be Important to Meet Regulatory Requirements

Canada's Pest Management Regulatory Agency publishes LOQ values for heavy metals → some are major components in standard equipment metallurgy

Guidance reinforces need for good product stewardship towards corrosion avoidance

PMRA established LOQs for heavy metals in Technical Grade Active Ingredients

Heavy metal	Required LOQ (ppm)
Antimony	1
Arsenic	1
Cadmium	1
Chromium	1
Cobalt	1
Lead	1
Mercury	0.01
Nickel	1
Selenium	1

Found in commonly used alloys

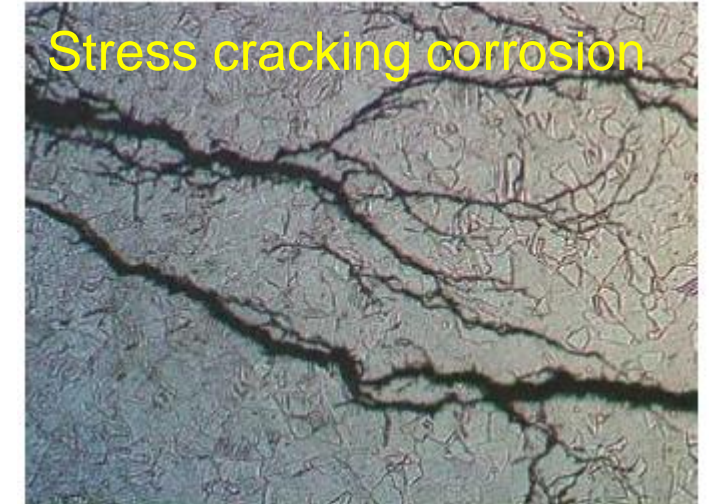


LOQ = limit of quantitation  
ppm = parts per million

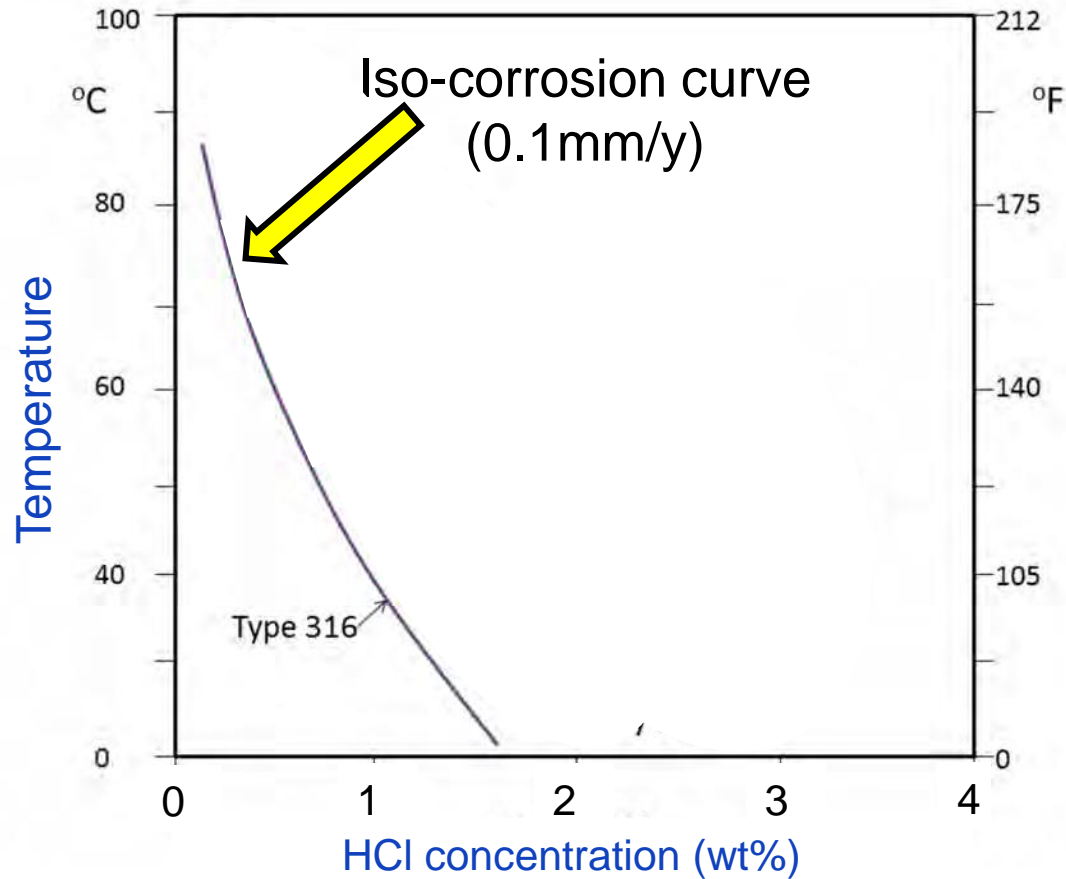


# Types of Corrosion

Uniform, localized, and stress cracking corrosion are the 3 main categories



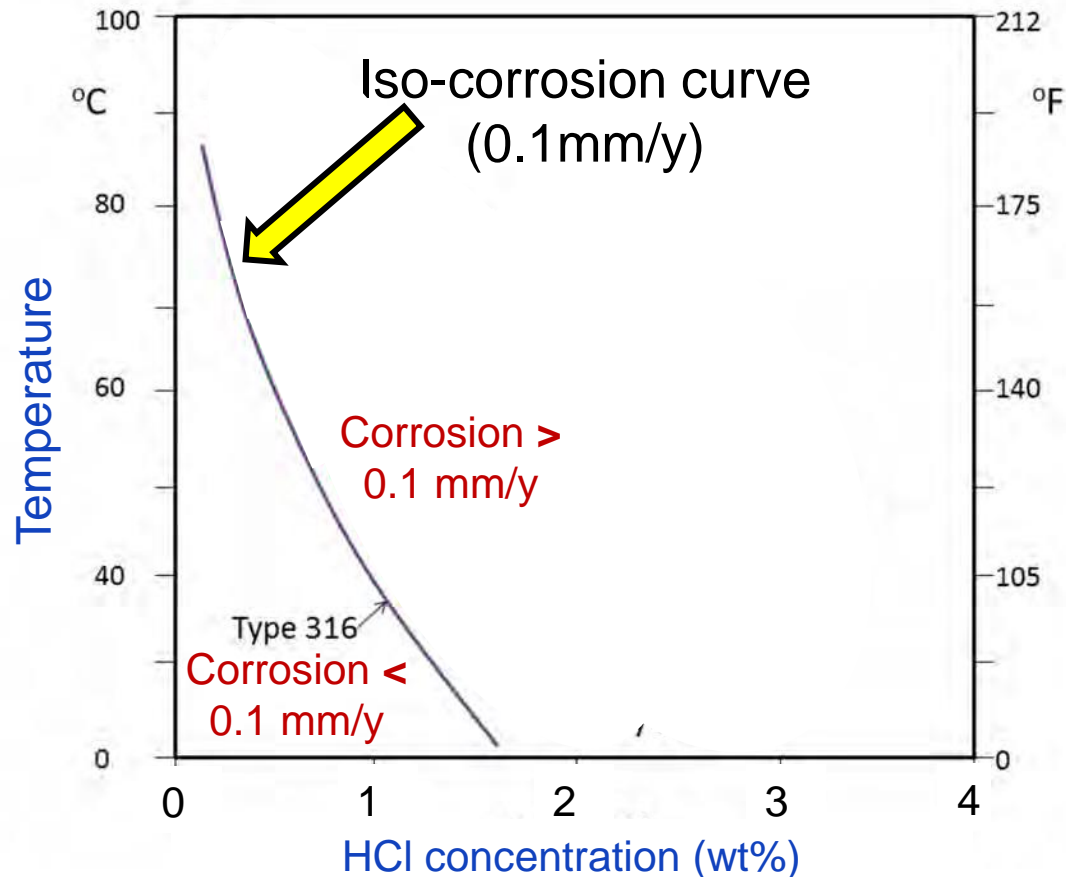
# Corrosion Rates are Concentration and Temperature Dependent



**Stainless steel 316** in dilute HCl

Points on the isocorrosion curve:  
corrosion rate = 0.1 mm/y

# Corrosion Rates are Concentration and Temperature Dependent

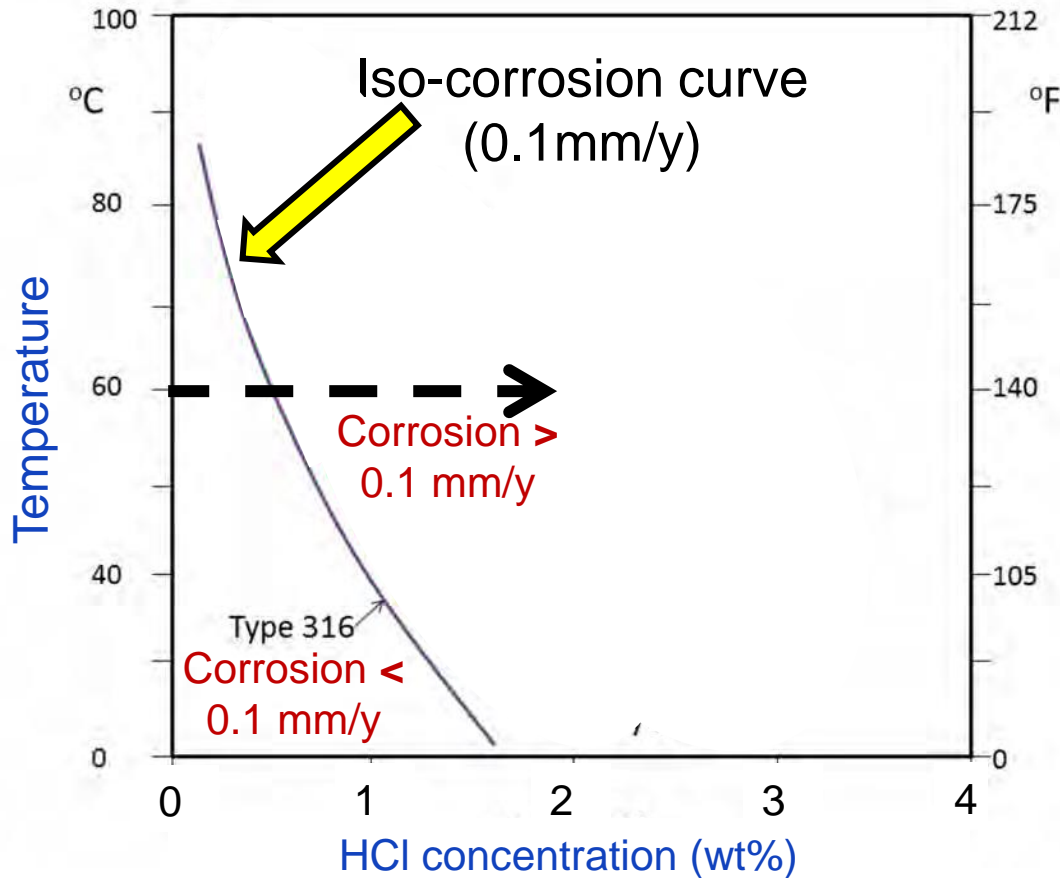


**Stainless steel 316** in dilute HCl

Points on the isocorrosion curve:  
corrosion rate = 0.1 mm/y

Corrosion rate is < 0.1 mm/y below curve  
and > 0.1 mm/y above the curve

# Corrosion Rates are Concentration and Temperature Dependent



**Stainless steel 316** in dilute HCl

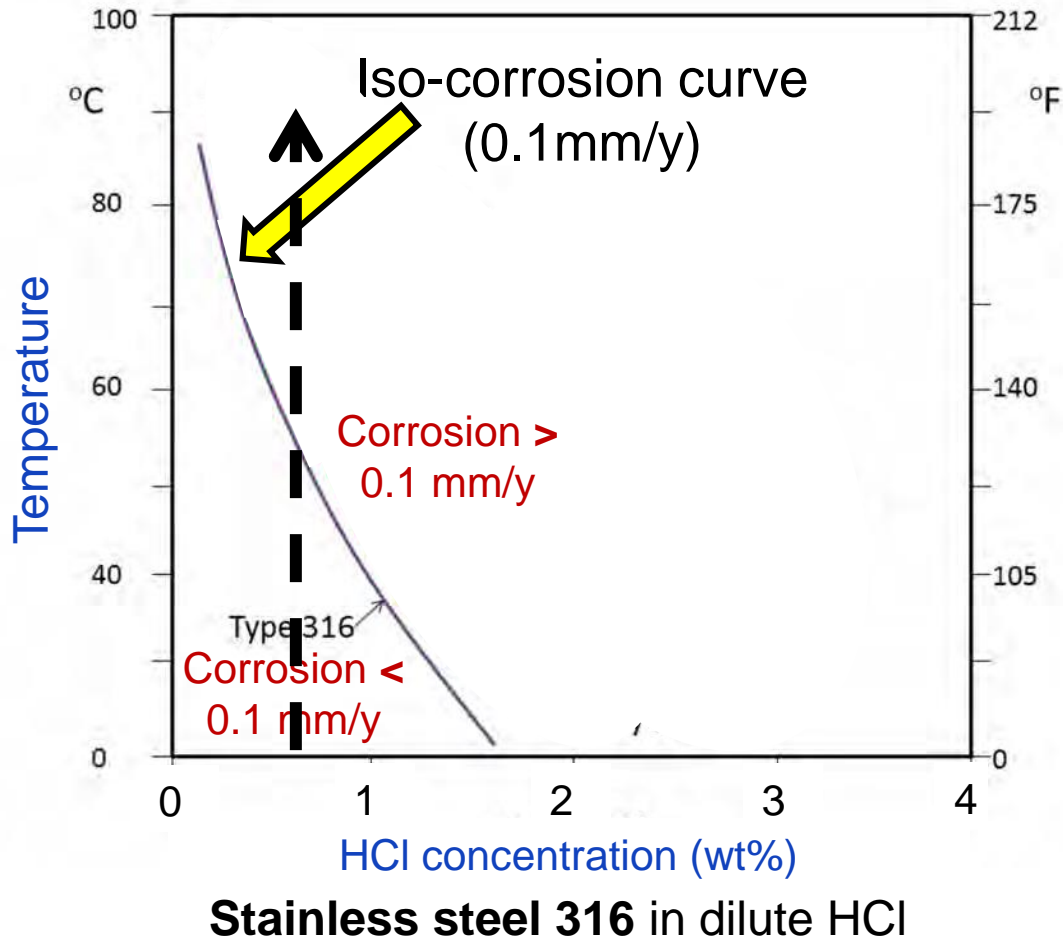
Points on the isocorrosion curve:  
corrosion rate = 0.1 mm/y

Corrosion rate is < 0.1 mm/y below curve  
and > 0.1 mm/y above the curve

Corrosion rates increase with HCl  
concentration



# Corrosion Rates are Concentration and Temperature Dependent

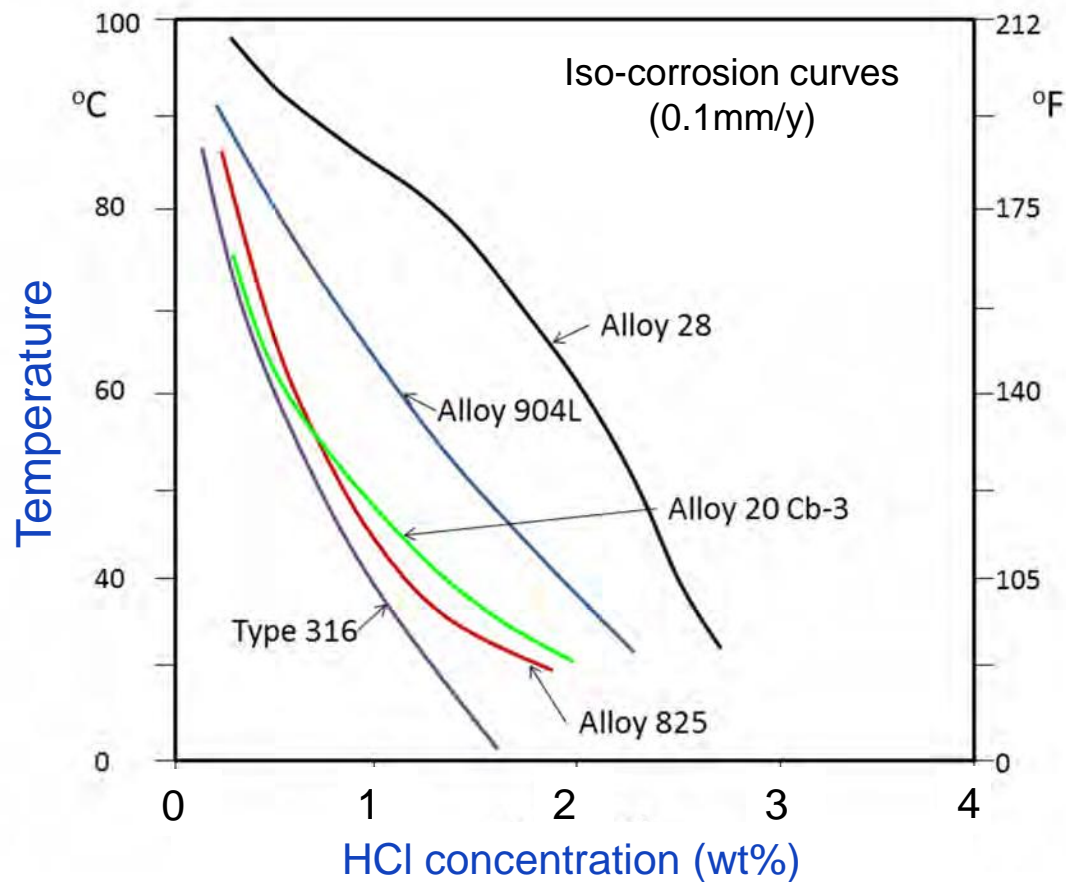


Points on the isocorrosion curve:  
corrosion rate = 0.1 mm/y

Corrosion rate is < 0.1 mm/y below curve  
and > 0.1 mm/y above the curve

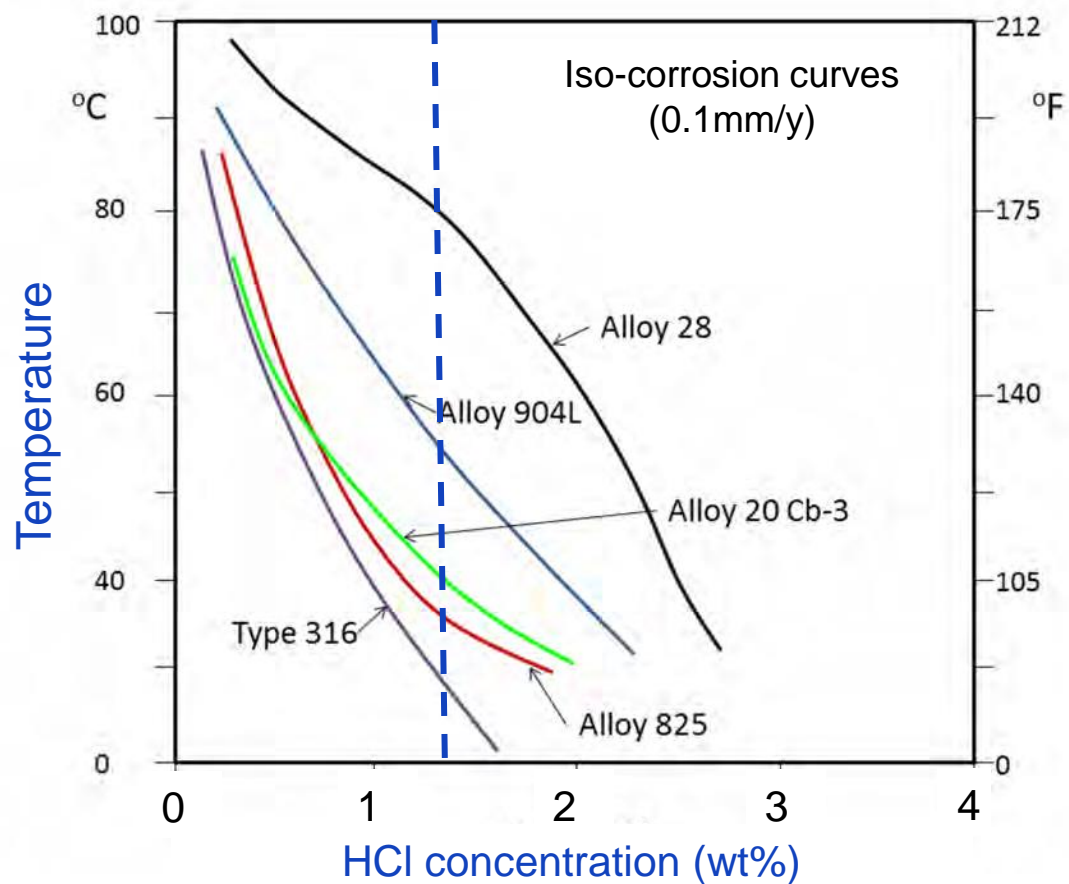
Corrosion rates increase with HCl  
concentration and also with temperature

# Corrosion Resistant Alloys can Mitigate Risk



Various grades of **stainless steels** in dilute HCl

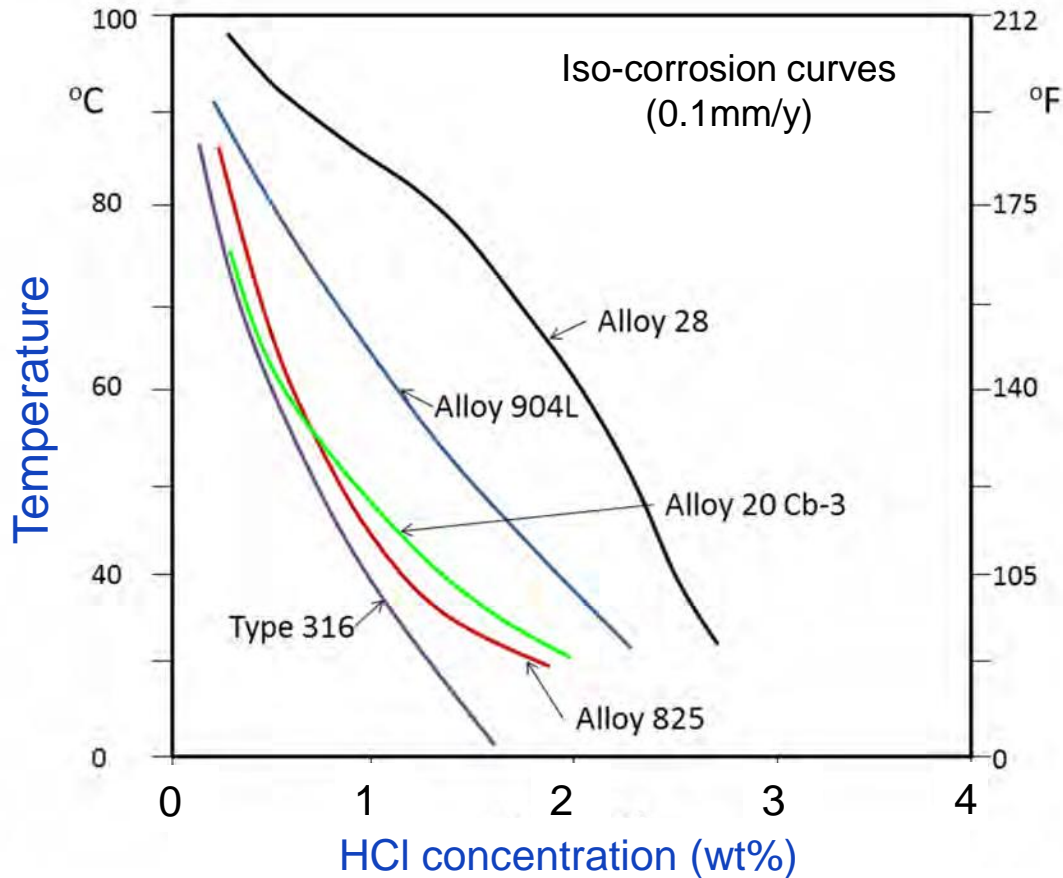
# Corrosion Resistant Alloys can Mitigate Risk



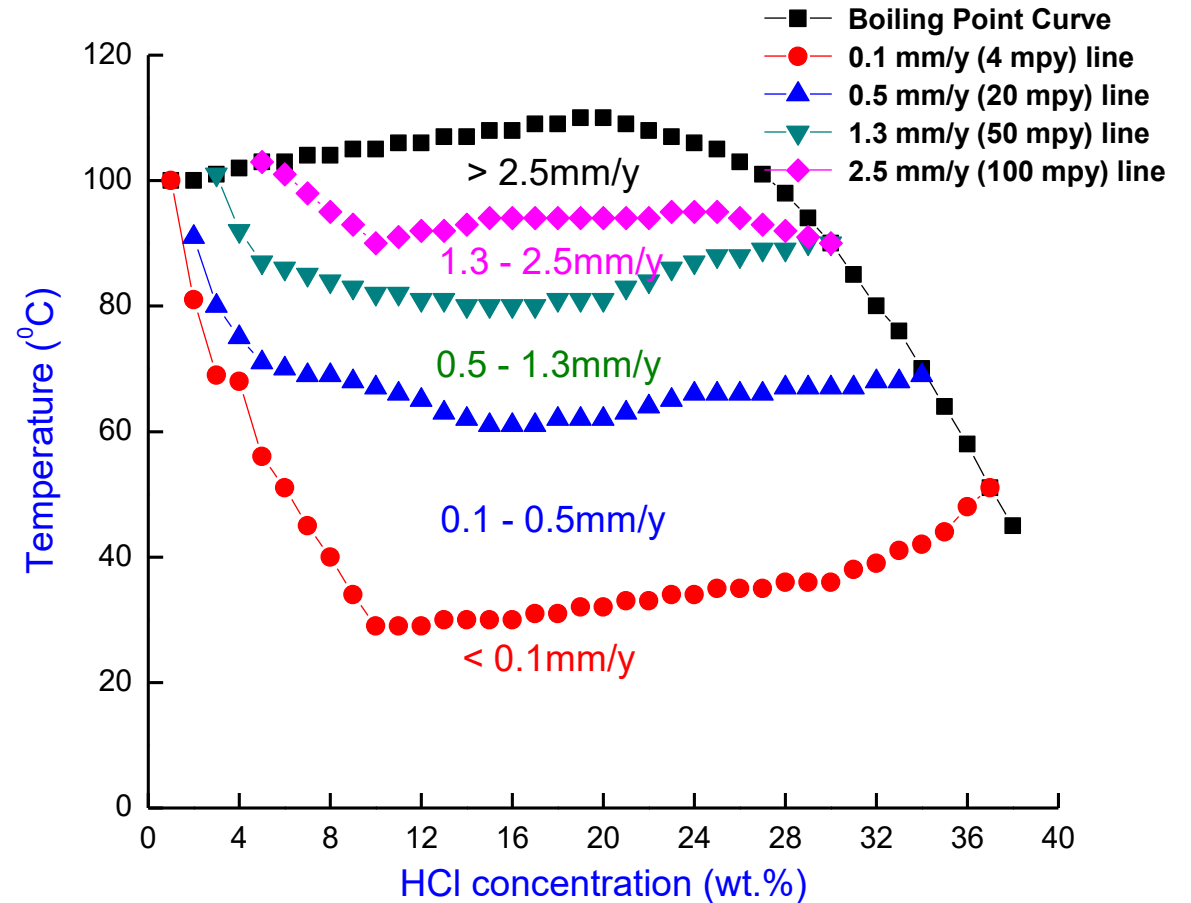
Various grades of **stainless steels** in dilute HCl



# Corrosion Resistant Alloys can Mitigate Risk



Various grades of **stainless steels** in dilute HCl

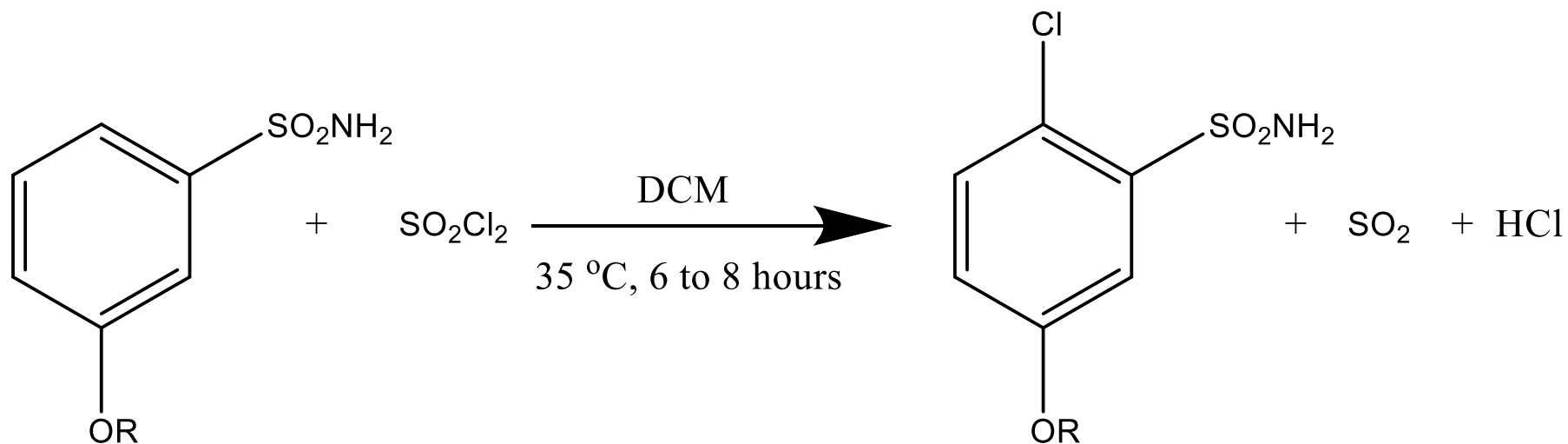


**Hastelloy C-276** in reagent grade hydrochloric acid

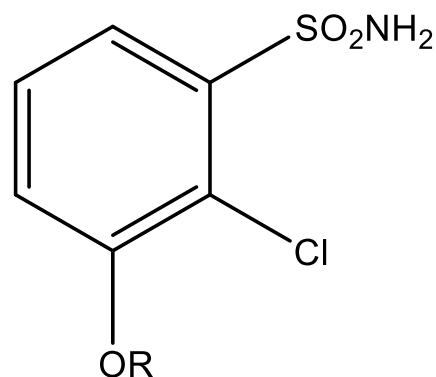
Higher corrosion-resistant alloys (like Hastelloy C-276, C-22) can provide an extended service life compared to stainless steels in highly corrosive conditions.

# Unexpected Corrosion Surprises with Resistant Alloys: 3 Case Studies

# Selectivity Challenges for an Agrochemical Intermediate



The regioisomer of the desired product was a major impurity

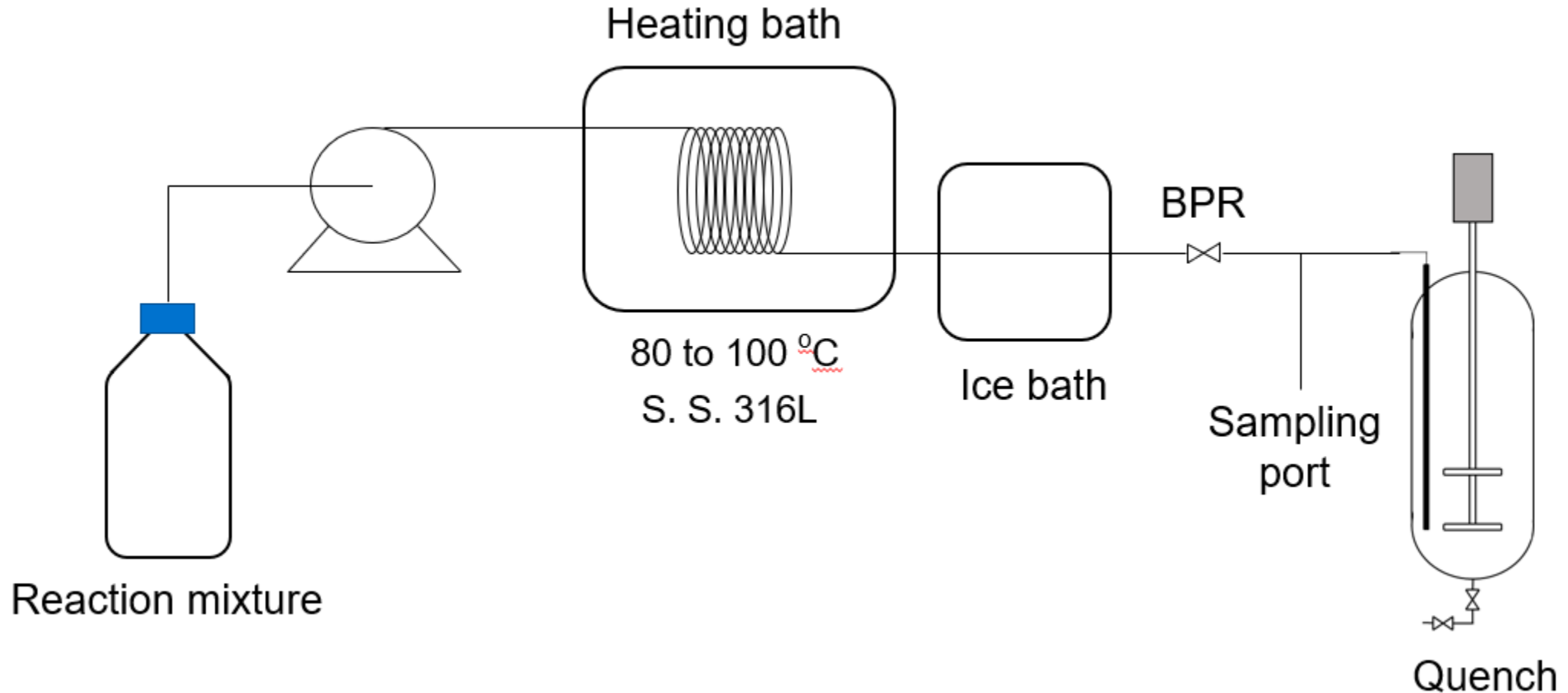


Impurity:Product ratio ~ 10%



# Attempts to Improve Selectivity

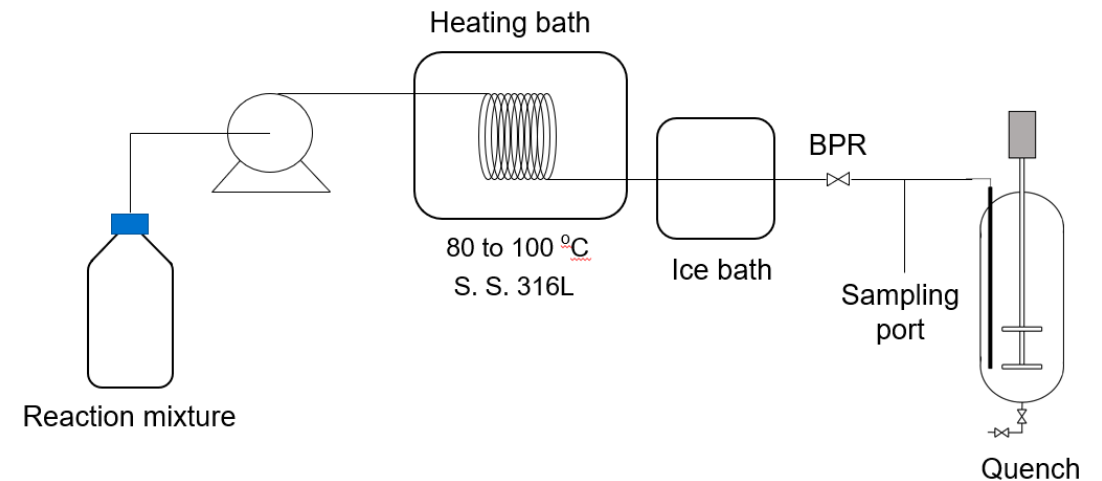
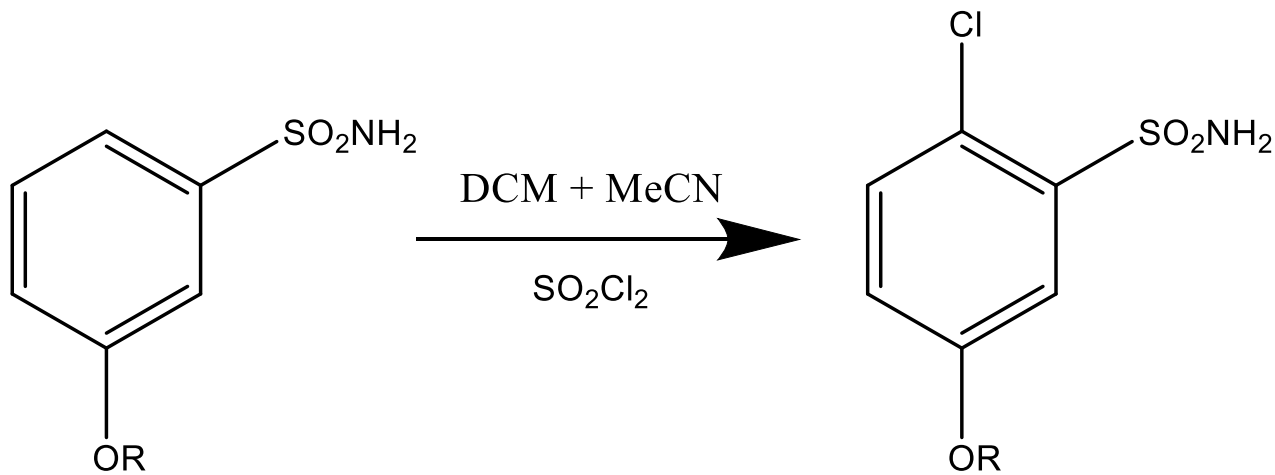
Run reaction at high temperature in a coiled tube reactor



**Challenge:** Reaction mixture is a slurry that caused pumping issues

# Attempts to Improve Selectivity

**Challenge:** Reaction mixture is a slurry that caused pumping issues



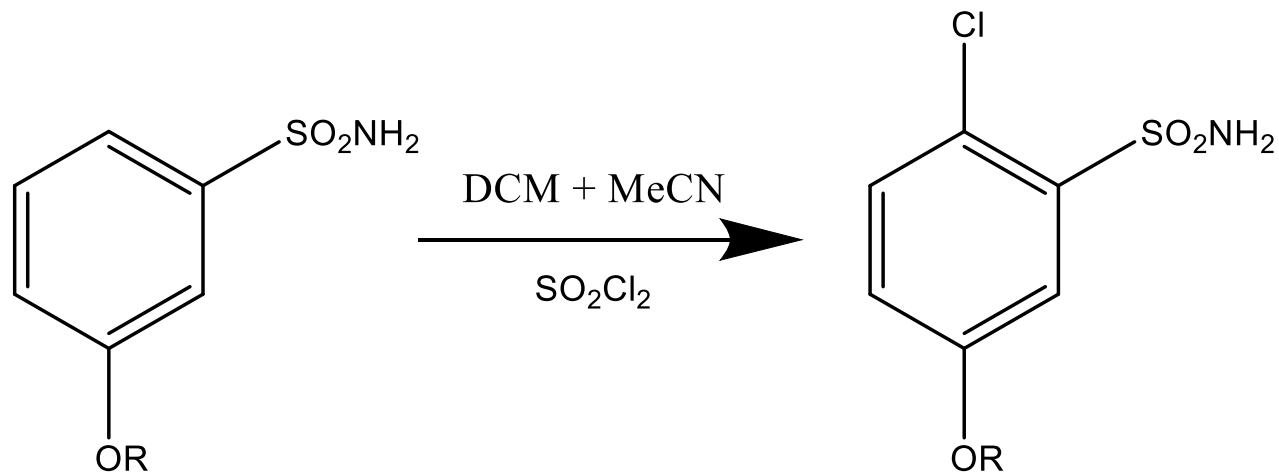
**Work-around:** Add acetonitrile to improve starting material solubility

# Attempts to Improve Selectivity

Reactions were also run at high temperature and pressure in a Parr reactor

Temperature range: 70 to 120 °C

Pressure range: 60 to 400 psi



100mL Parr reactor  
Hastelloy C-22



# Both Reactor Types Showed Signs of Corrosion

Water was used to quench the mixture at the end of the reaction

Samples from aqueous layer sent for ICP analysis

Samples had high levels of elements found in SS 316L and HC-22

<b>Element</b>	<b>Coiled Tube Reactor Expt (ppm)</b>	<b>Parr Reactor Expt (ppm)</b>
	Stainless Steel	Hastelloy C-22
Chromium	1880	714
Iron	6500	367
Manganese	148	6.1
Molybdenum	246	404
Nickel	1345	1204

LOQ = 2 µg/g (ppm)

# Coupon Testing was Performed to Quantify Corrosion Rate

Hastelloy C-276 and Hastelloy C-2000 coupons were used in a 1L Parr reactor

Coupon	Initial weight (g)
H C-276	8.1130
H C-2000	7.6087

Test conditions:

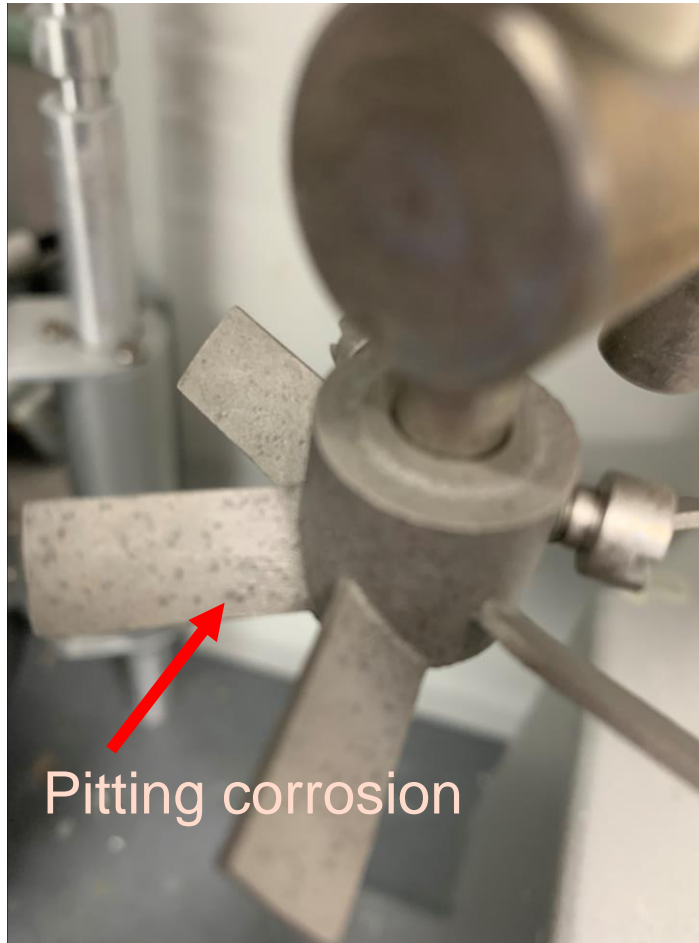
80 °C and 346 psi for 25 hours

2.5 wt% starting material, 4 eq.  $\text{SO}_2\text{Cl}_2$ ,  
18 wt% acetonitrile, rest DCM



# Coupon Testing was Performed to Quantify Corrosion Rate

End of test → Agitator and reactor surfaces had significant visible corrosion





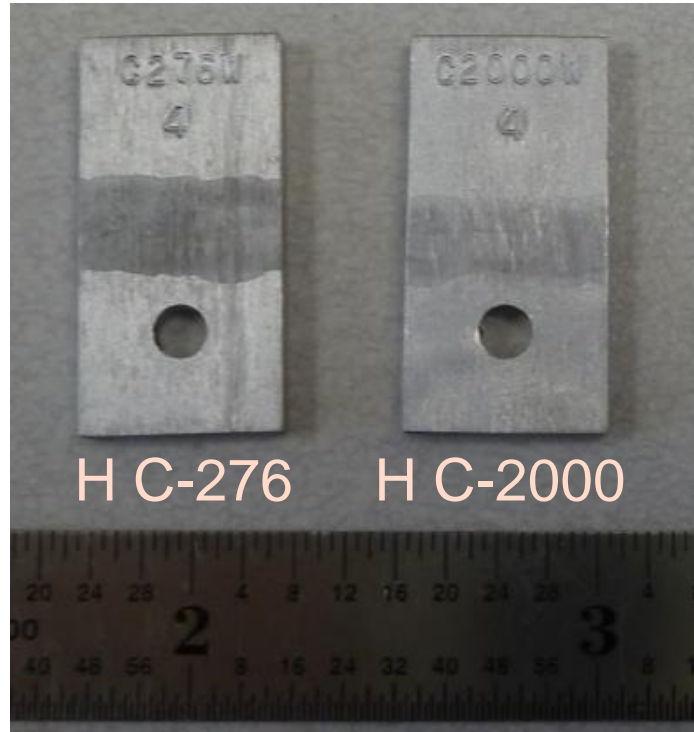
# Coupon Testing was Performed to Quantify Corrosion Rate

End of test → Agitator and reactor surfaces had significant visible corrosion



# Coupon Testing was Performed to Quantify Corrosion Rate

Coupons had visible surface damage and corrosion rate was extremely high



$$\text{Corrosion Rate} = \frac{\text{Weight Loss}}{\text{Density} \times \text{Surface Area} \times \text{Time}}$$

(Calculation assumes uniform corrosion rate)

Coupon	Initial weight (g)	Final weight (g)	% change in weight	<b>Corrosion rate (MPY)*</b>
H C-276	8.1130	8.0330	0.99%	<b>144.4</b>
H C-2000	7.6087	7.5070	1.34%	<b>193.1</b>

# Coupon Testing Repeated Without Acetonitrile

Test conditions:

2.1 wt% starting material, 4 eq.  $\text{SO}_2\text{Cl}_2$ , rest DCM

80 °C and 370 psi for 25 hours

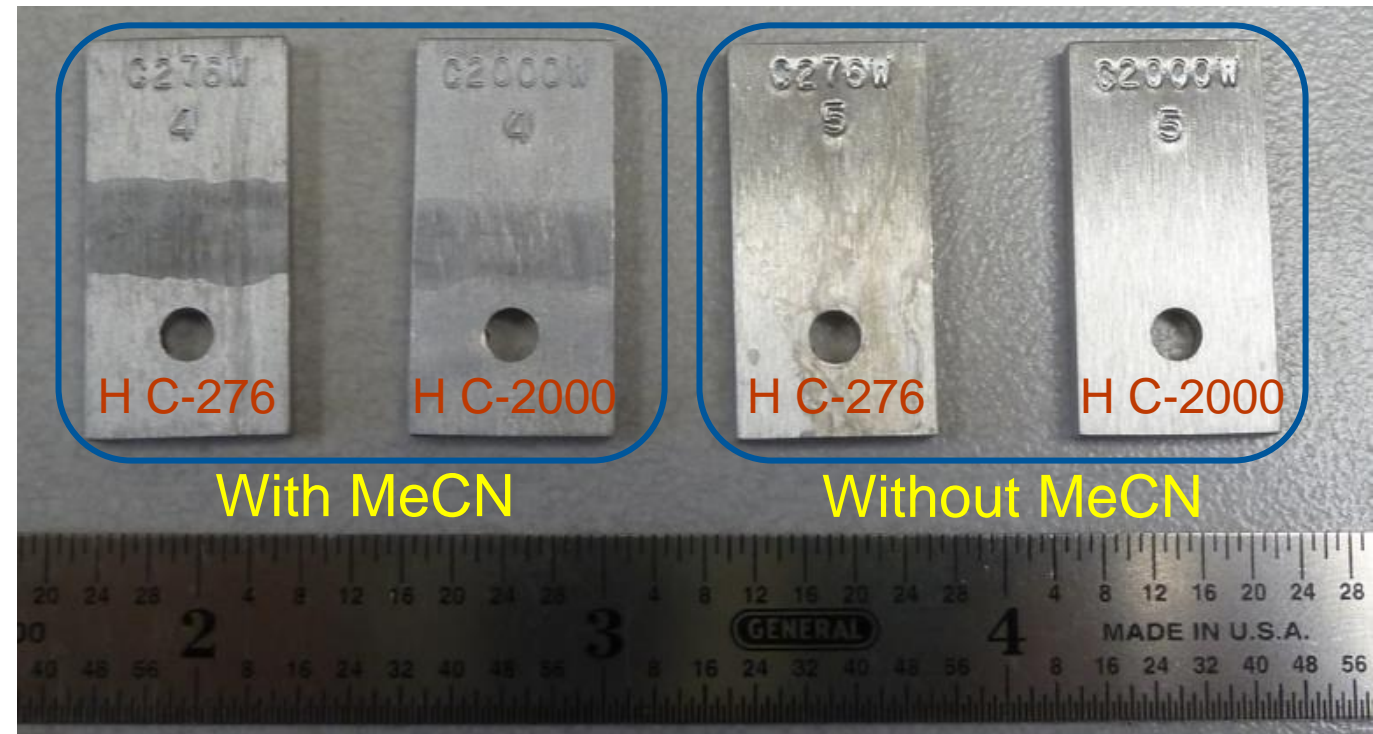
# Coupon Testing Repeated Without Acetonitrile

Test conditions:

2.1 wt% starting material, 4 eq. SO<sub>2</sub>Cl<sub>2</sub>, rest DCM

80 °C and 370 psi for 25 hours

Condition	Coupon	Corrosion rate (MPY)*
No MeCN	H C-276	1.6
No MeCN	H C-2000	1.9
MeCN present	H C-276	144.4
MeCN present	H C-2000	193.1

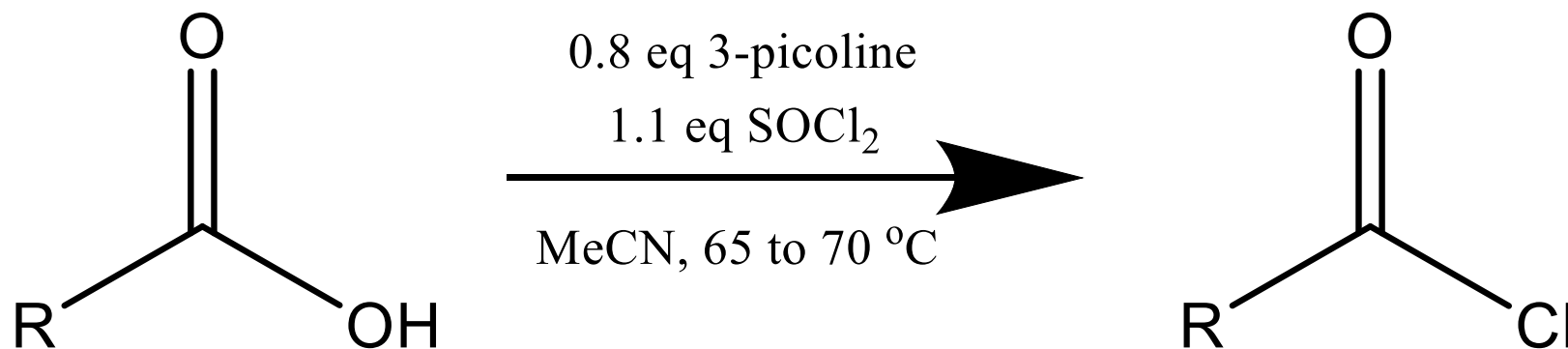


Corrosion rate was ~100x lower; no noticeable damage to reactor



## Case Study 2: Another Example of High Corrosion in Chemistry with Acetonitrile

Acid chloride formation reaction:



Coupon testing was performed over 2 weeks at 20 °C and 70 °C as part of scale-up preparations

# Case Study 2: Another Example of High Corrosion in Chemistry with Acetonitrile

H C-276 at 20 °C

Before

Mass: 17.9738 g



After

Mass: 17.7754 g



Coupon cleaning

Corrosion rate = 11.8 mpy

H C-276 at 70 °C

Before

Mass: 17.9969 g



After

Mass: 17.1059 g



Coupon cleaning

Corrosion rate = 59.1 mpy

# Case Study 2: Another Example of High Corrosion in Chemistry with Acetonitrile

H C-22 at 20 °C

Before

Mass: 17.8526 g



After

Mass: 17.6497 g



Coupon cleaning

Corrosion rate = 15.8 mpy

H C-22 at 70 °C

Before

Mass: 17.9969 g



After

Mass: 17.1059 g



Coupon cleaning

Corrosion rate = 74.8 mpy

# Evidence for Acetonitrile being the Root Cause of Corrosivity

Coupon tests were performed with mixtures of chlorinating agents and solvents

No other reagents (including ag intermediates) were included

## **Coupons:**

- 1) Hastelloy B3
- 2) Hastelloy C-2000
- 3) Hastelloy C-276
- 4) Inconel 600
- 5) Monel 400
- 6) Nickel 200
- 7) Stainless Steel 316

## **Chlorinating agents:**

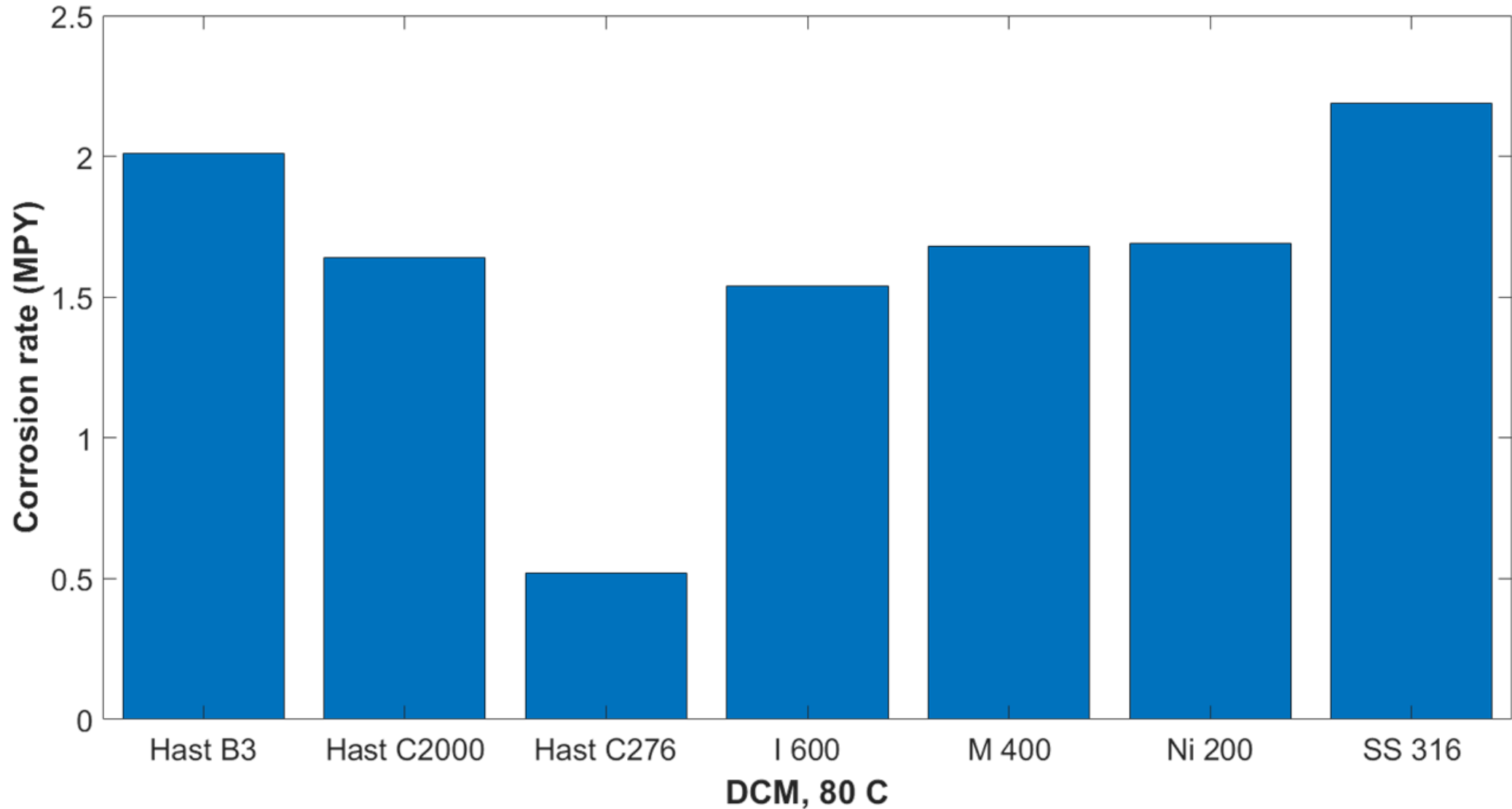
- 1) Sulfuryl Chloride
- 2) Thionyl Chloride
- 3) Oxalyl Chloride

## **Solvents:**

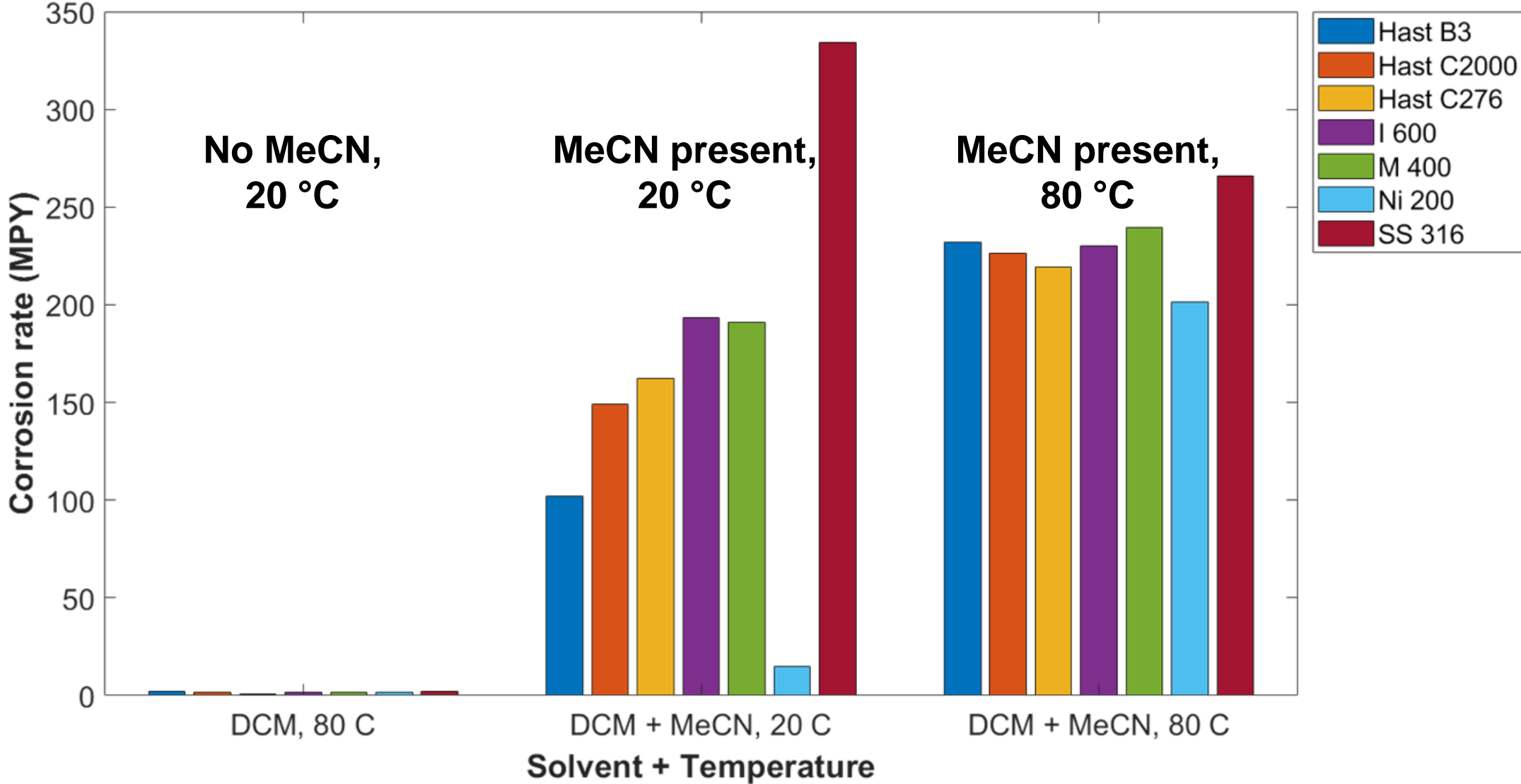
- 1) Dichloromethane (DCM)
- 2) DCM:MeCN 4:1 mix



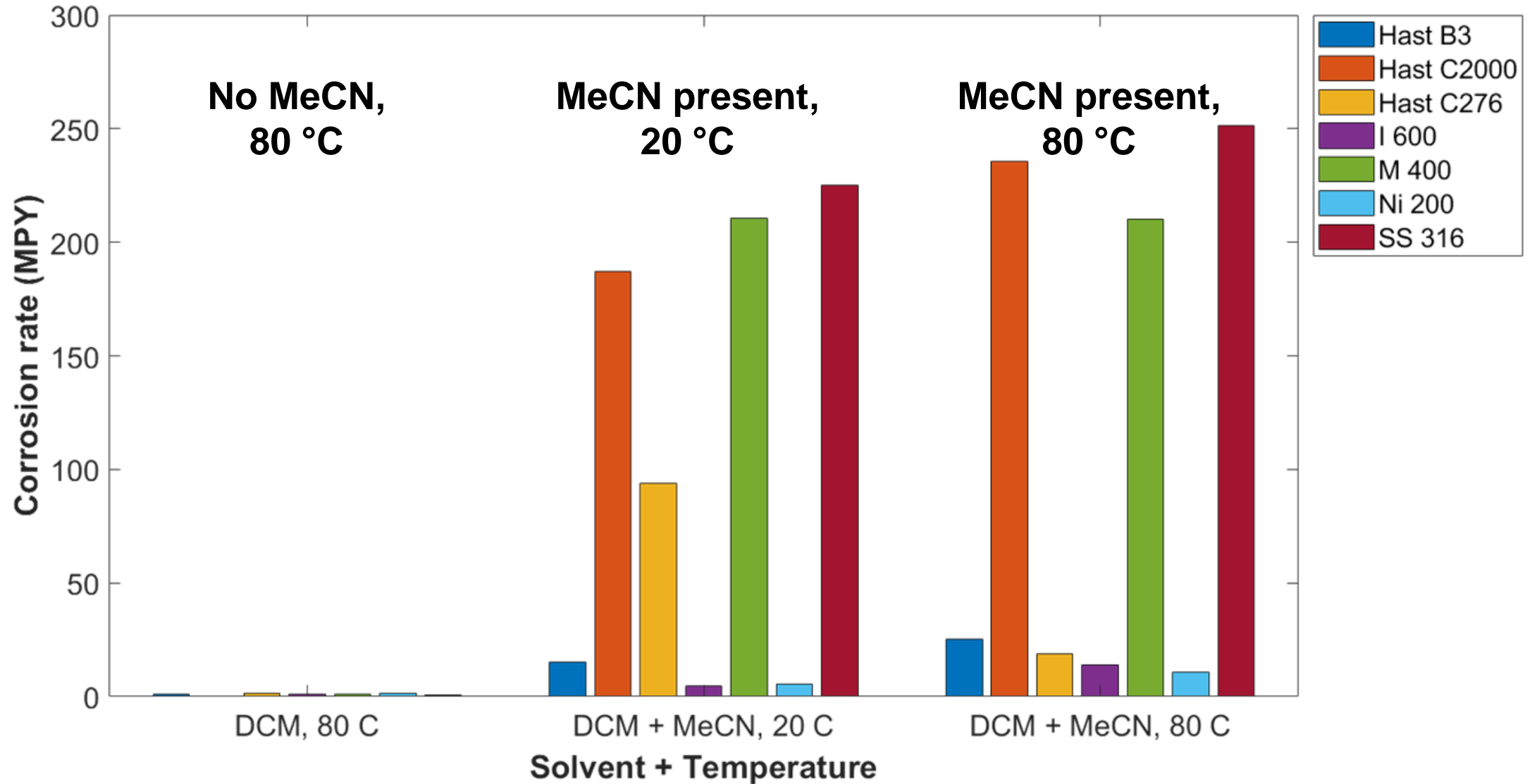
# Corrosion Rates for Sulfuryl Chloride + DCM (80 °C)



# Corrosion Rates for Sulfuryl Chloride

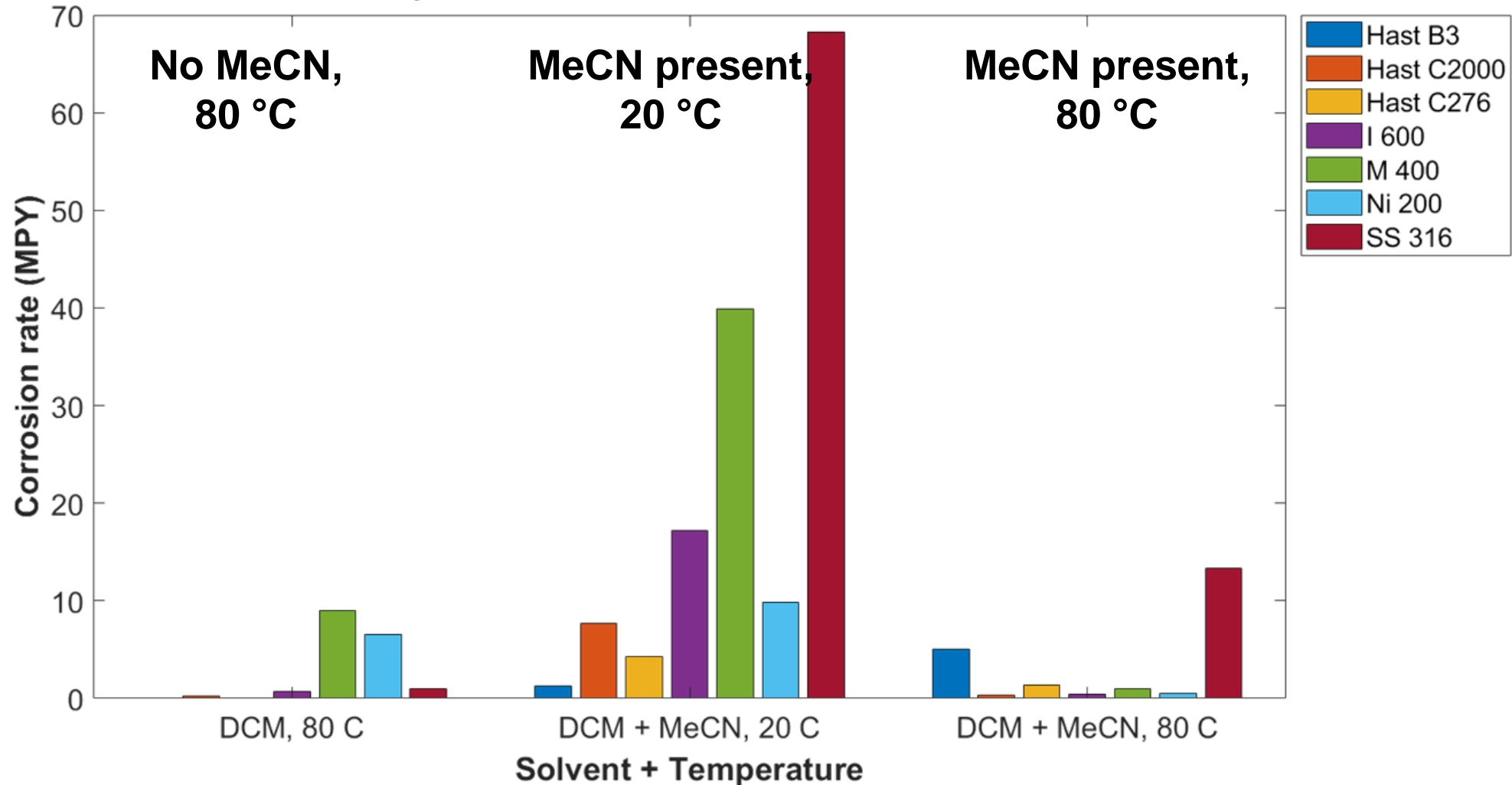


# Corrosion Rates for Thionyl Chloride



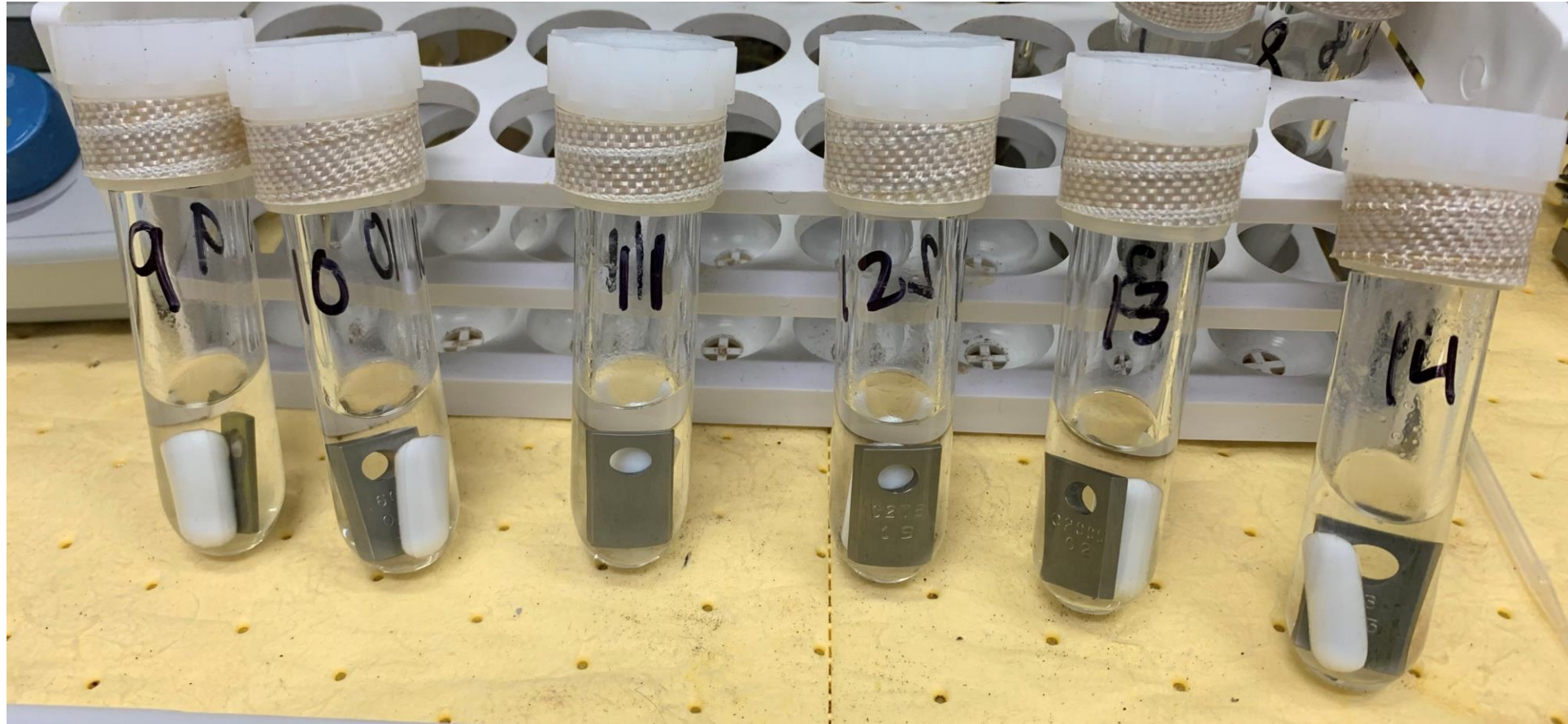
# Corrosion Rates for Oxalyl Chloride

Oxalyl chloride behaves differently from sulfuryl or thionyl chloride  
Further investigation needed to understand mechanism



# Representative Images at End of Coupon Tests

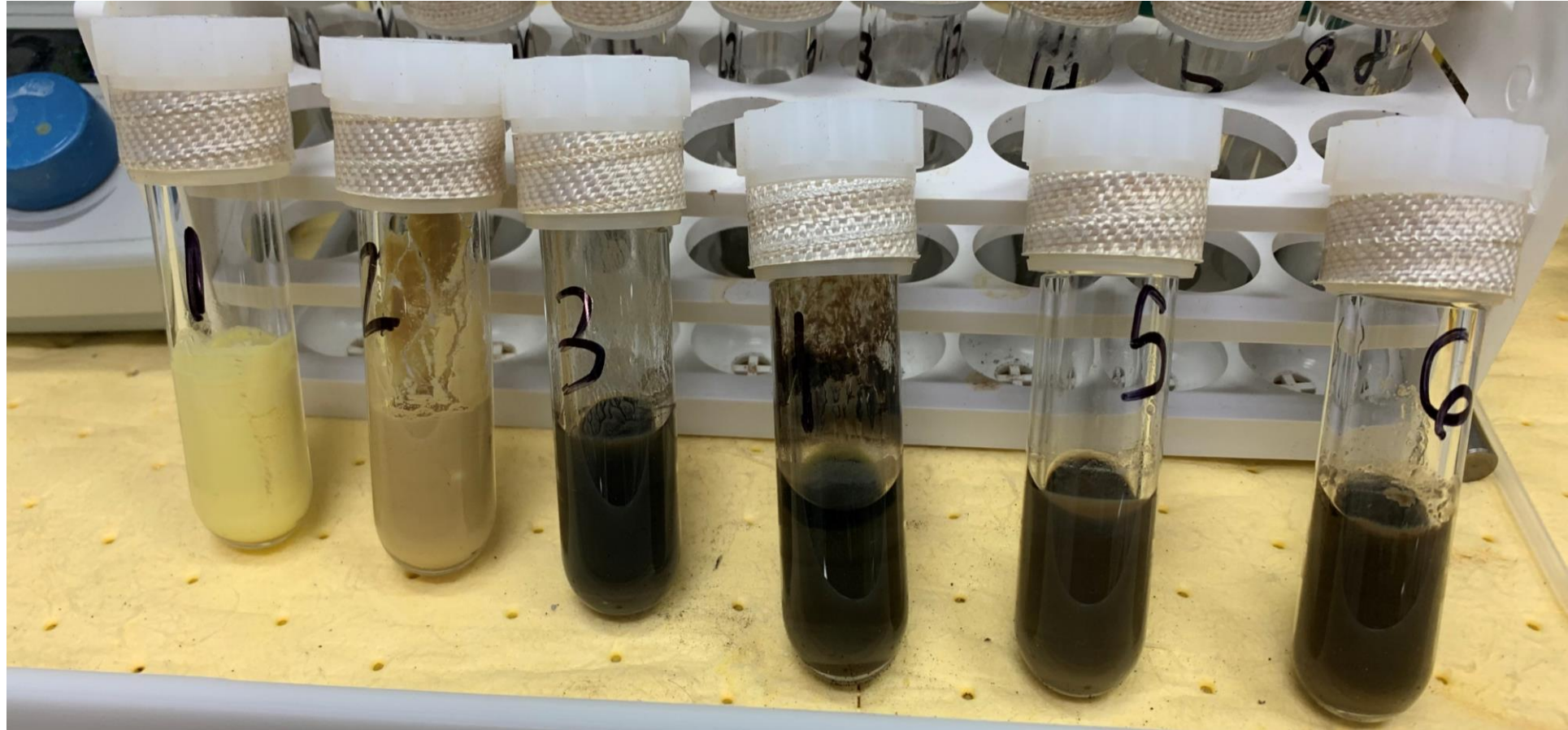
Low corrosion conditions





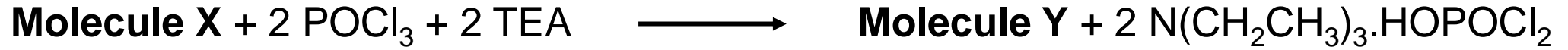
# Representative Images at End of Coupon Tests

High corrosion conditions



Acetonitrile is not the only reagent that can cause unexpectedly high corrosion in resistant alloys

# Case Study 3: POCl<sub>3</sub> Chlorination



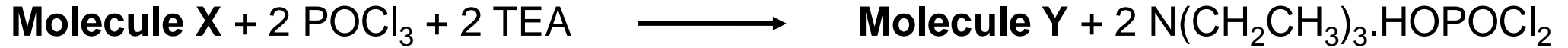
The base, triethylamine (TEA), catalyzes POCl<sub>3</sub> chlorinations

TEA also suppresses over-chlorination of Molecule X

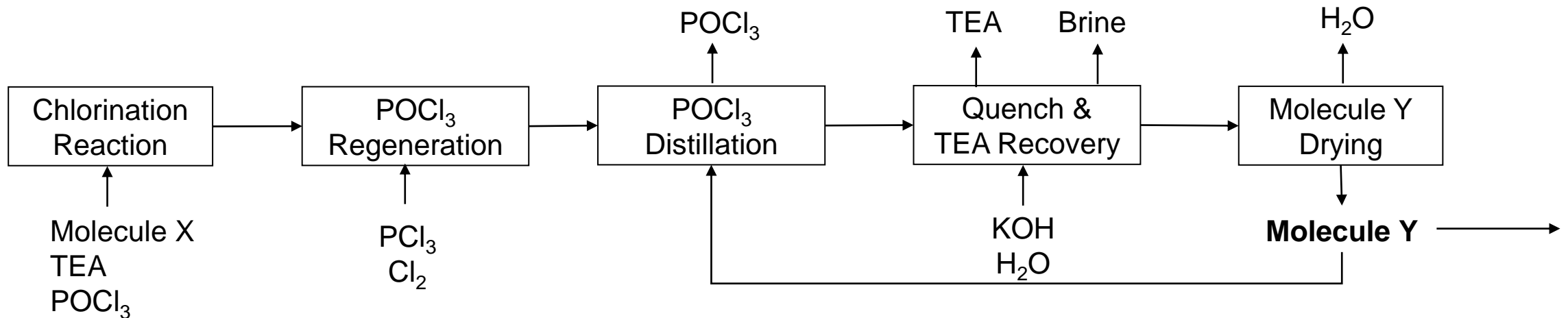
Both POCl<sub>3</sub> and TEA are regenerated at the end of the reaction

# Case Study 3: POCl<sub>3</sub> Chlorination

## POCl<sub>3</sub> Chlorination



## POCl<sub>3</sub> Regeneration



# Materials of Construction Surprise

Process was planned to be scaled up in a Hastelloy C reactor in pilot plant

- Reactor had been used for similar  $\text{POCl}_3$  reaction with good results



# Materials of Construction Surprise

Process was planned to be scaled up in a Hastelloy C reactor in pilot plant

- Reactor had been used for similar  $\text{POCl}_3$  reaction with good results

Coupon testing performed at 75 °C few months before startup

Reaction	Corrosion Rate (MPY)*
$\text{POCl}_3$ Chlorination	27
$\text{POCl}_3$ regeneration	482
$\text{POCl}_3$ Chlorination w/o TEA	< 1

TEA•HCl presumably formed “super acid” in  $\text{POCl}_3$  → attacked Hastelloy C

# Conclusions

Acetonitrile combined with certain chlorinating agents can severely corrode resistant alloys, even at room temperature

Other reagents can also form “super-acids” that can corrode resistant alloys

Mechanism of severe corrosion is not completely understood → Difficult to predict when it will occur

Perform thorough corrosion testing before scale-up to avoid unpleasant surprises

# Acknowledgements



Jay Devaraj



Paul Speakman



Aaron Shinkle



Kelsi Goshinsky



Ajit Mishra



John Doyle



Abraham Schuitman



Greg Whiteker



Ron Leng



David Clouse



Matthias Ober



Matthew Bolten

# Additional Slides

# Reactivity of Sulphuryl Chloride in Acetonitrile with the Elements †

Alfred A. Woolf

*Department of Science, Bristol Polytechnic, Bristol BS16 1QY, UK*

---

Sulphuryl chloride in MeCN reacts with all but the most refractory elements to give mainly solvated chlorides at or below 300 K in contrast with  $\text{SO}_2\text{Cl}_2$  alone which requires at least twice this temperature. There is evidence for an ionic mechanism based on analogy, thermochemistry, transport measurements and additive effects. The instability of these solutions leading to polymerization, together with its inhibition, is described. Sulphur dioxide formed in reactions seldom plays a reductive role apart from influencing formation of the mixed-valence  $\text{Ti}_4\text{Cl}_6$ . Semiquantitative kinetic measurements in different solvents emphasize the uniqueness of MeCN. For most elements attack is diffusion controlled across surface films giving a parabolic dependence on time which can be linearized if film growth is prevented by changing the solvent mix. The varied nature of these surface films vitiates any simple relation between rate and periodicity. Some applications are indicated.

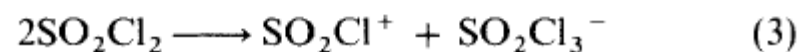
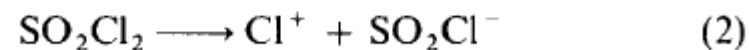
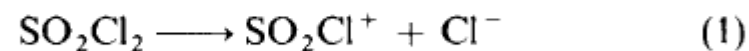


## Reactivity of Sulphuryl Chloride in Acetonitrile with the Elements †

Alfred A. Woolf

*Department of Science, Bristol Polytechnic, Bristol BS16 1QY, UK*

The enhanced reactivity of  $\text{SO}_2\text{Cl}_2$  in MeCN, comparable with that of  $\text{N}_2\text{O}_4$  in organic solvents towards metals,<sup>20</sup> suggests an ionic mechanism. The extent of ionization is minute, and not detectable in Raman or NMR spectra of fresh solutions, but the presence of ions is detectable from the conductivity increase. Possible gas-phase ionizations (1)–(3) can be compared.



J. CHEM. SOC. DALTON TRANS. 1991

