

Creep Compliance and Tensile Strength of Hot-Mix Asphalt for Wearing Courses in Missouri

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Thermal Cracking Module

Level 1 Inputs

- ***Creep Compliance determined at -20, -10, and 0°C (-4, 14, and 32°F, respectively)***
- ***Creep Compliance determined at 1, 2, 5, 10, 20, 50, and 100 seconds at each temperature***
- ***Tensile Strength determined at -10°C***
- Aggregate and mixture Coefficient of Thermal Contraction (mix CTC can be calculated from other properties)
- Mixture VMA

Results

Input Summary

Thermal Cracking

- Level 1
- Level 2
- Level 3

Average tensile strength at 14 °F (psi):

388.87

Import

Export

Loading Time sec	Creep Compliance (1/psi)		
	Low Temp (°F)	Mid Temp (°F)	High Temp (°F)
	-4	14	32
1	4.68382e-007	6.91144e-007	9.33833e-007
2	5.09039e-007	7.97027e-007	1.16513e-006
5	5.68252e-007	9.62291e-007	1.56107e-006
10	6.17578e-007	1.10971e-006	1.94772e-006
20	6.71187e-007	1.27972e-006	2.43015e-006
50	7.49261e-007	1.54507e-006	3.25596e-006
100	8.143e-007	1.78178e-006	4.06242e-006

Compute mix coefficient of thermal contraction.

Mixture VMA (%):

18.6

Aggregate coefficient of thermal contraction:

1e-006

...

Mix coefficient of thermal contraction (in/in/°F):

OK

Cancel

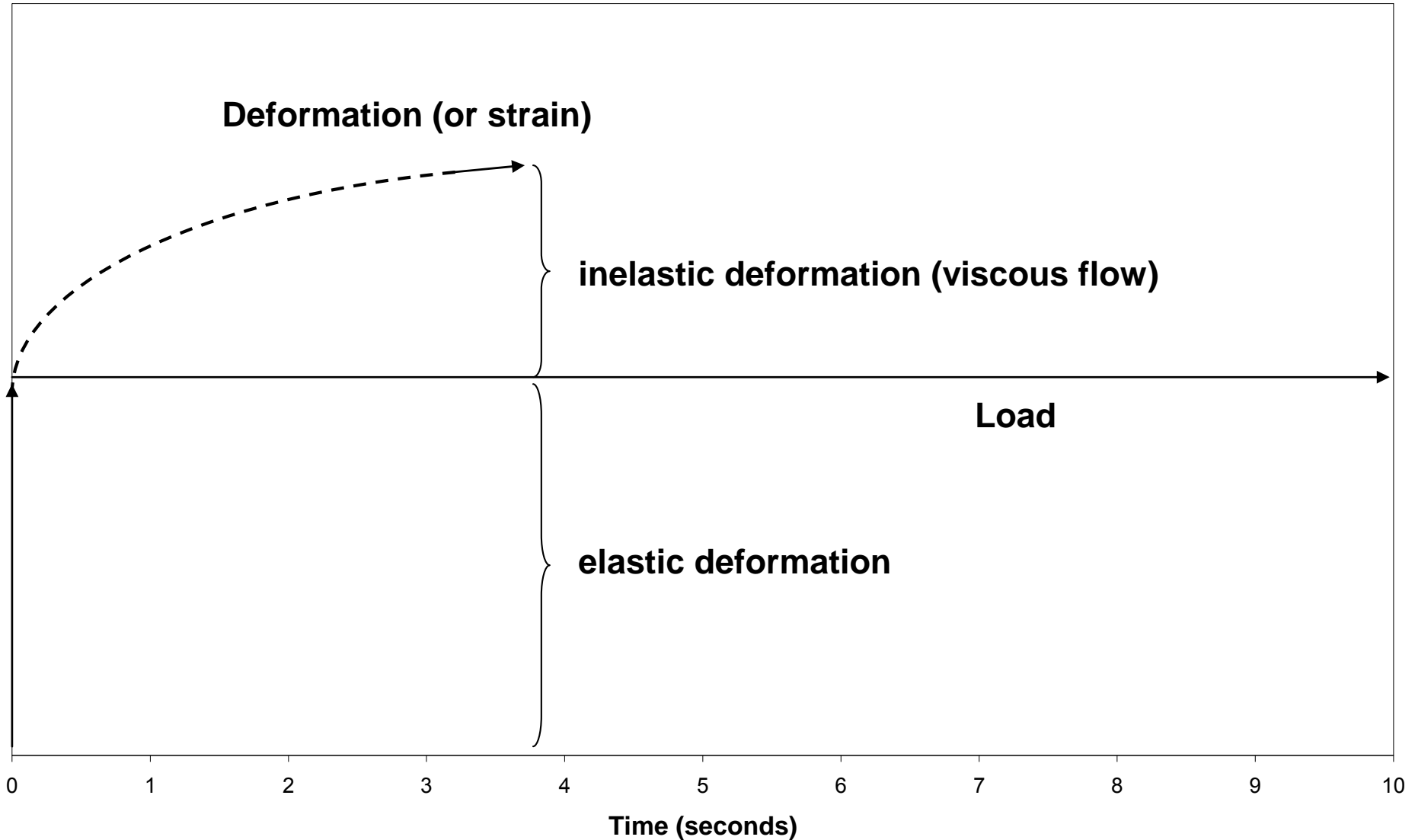
AASHTO T 322 Basics

- Indirect Tensile (IDT) method
- Maximum Aggregate Size ≤ 38 mm
- Specimens 38 to 50 mm high (thick) and 150 ± 9 mm in diameter
- Creep Compliance: “Zero or rebalance the electronic measuring system and apply a static load of fixed magnitude ($\pm 2\%$) without impact to the specimen for 100 ± 2 seconds.”(Sec. 11.4)
- Tensile Strength: “After the creep tests have been completed at each temperature, determine the tensile strength by applying a load to the specimen at a rate of 12.5 mm of ram (vertical) movement per minute.” (Sec 11.5)

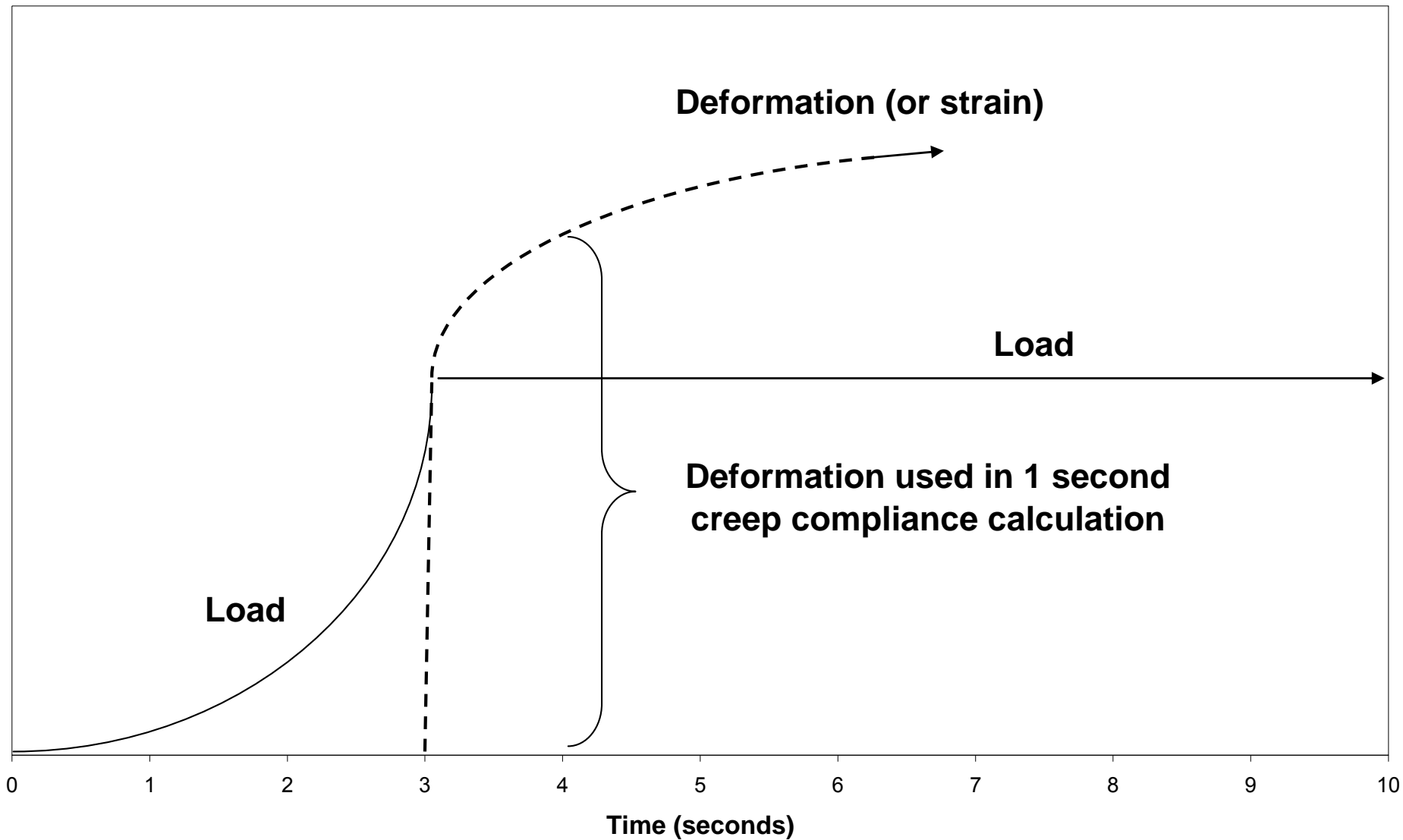


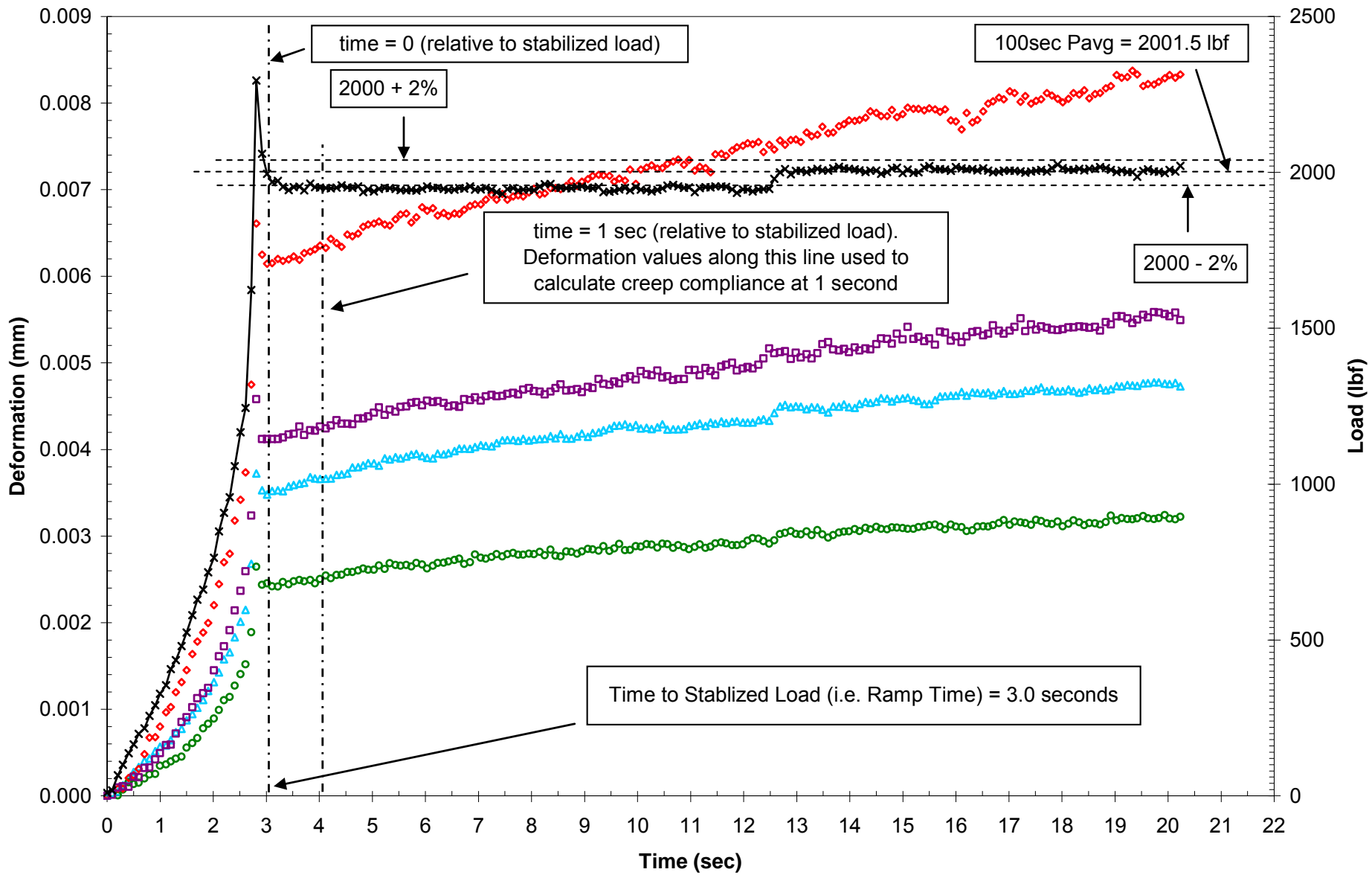


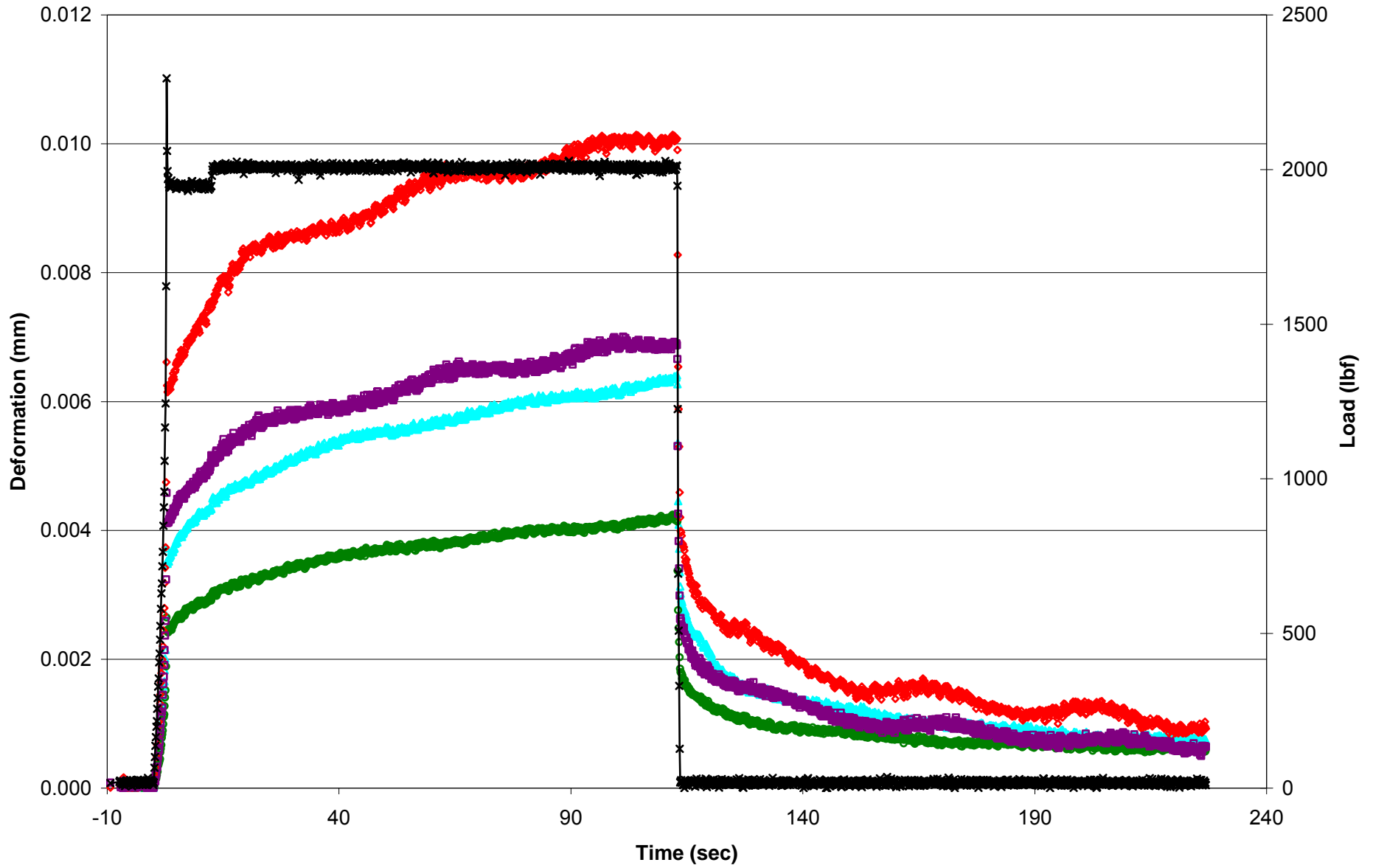
True Creep Load Profile: Instantaneous Loading/Unloading



Assumed Creep Load: Non-Instantaneous Loading

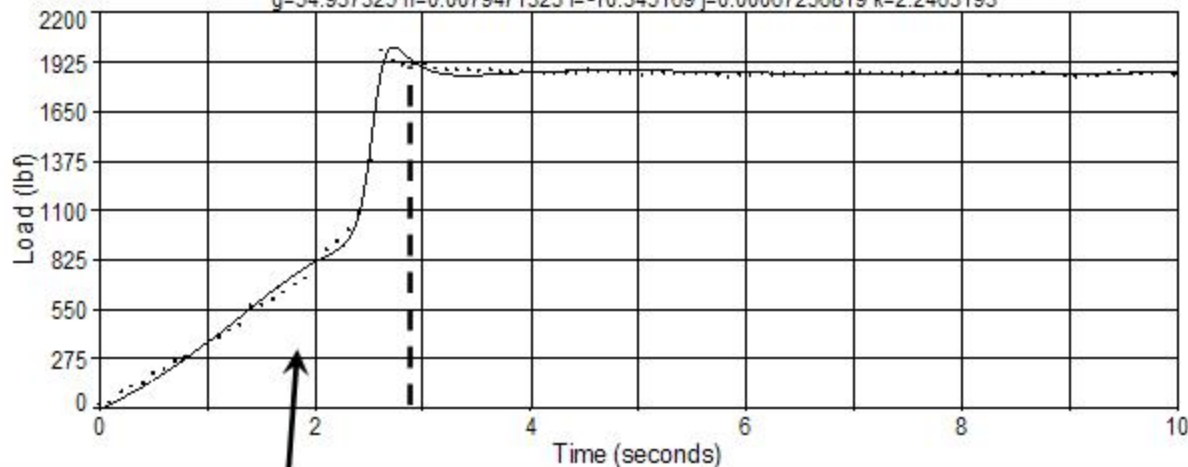






Load vs Time (First 10 seconds only)

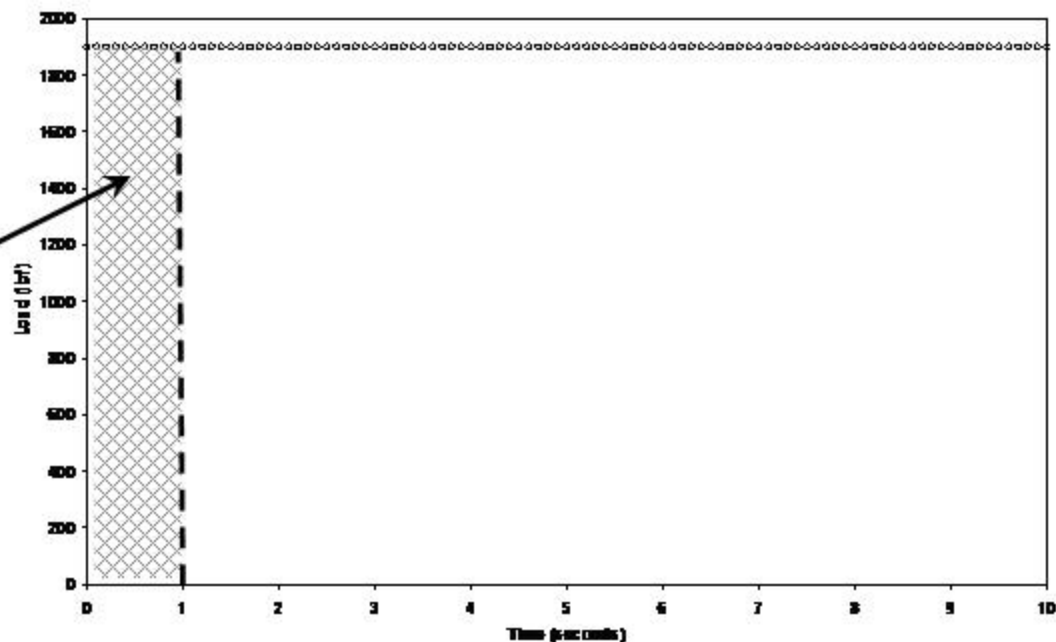
Rank 1 Eqn 7909 $y=(a+cx+ex^2+gx^3+ix^4+kx^5)/(1+bx+dx^2+fx^3+hx^4+jx^5)$ [NL]
 $r^2=0.99803154$ DF Adj $r^2=0.99778549$ FitStdErr=29.270661 Fstat=4512.4118
 $a=-6.9628778$ $b=-1.0752231$ $c=287.17329$ $d=0.45821031$ $e=-220.30919$ $f=-0.098969075$
 $g=54.937325$ $h=0.0079471323$ $i=-10.345169$ $j=0.00067256819$ $k=2.2463193$



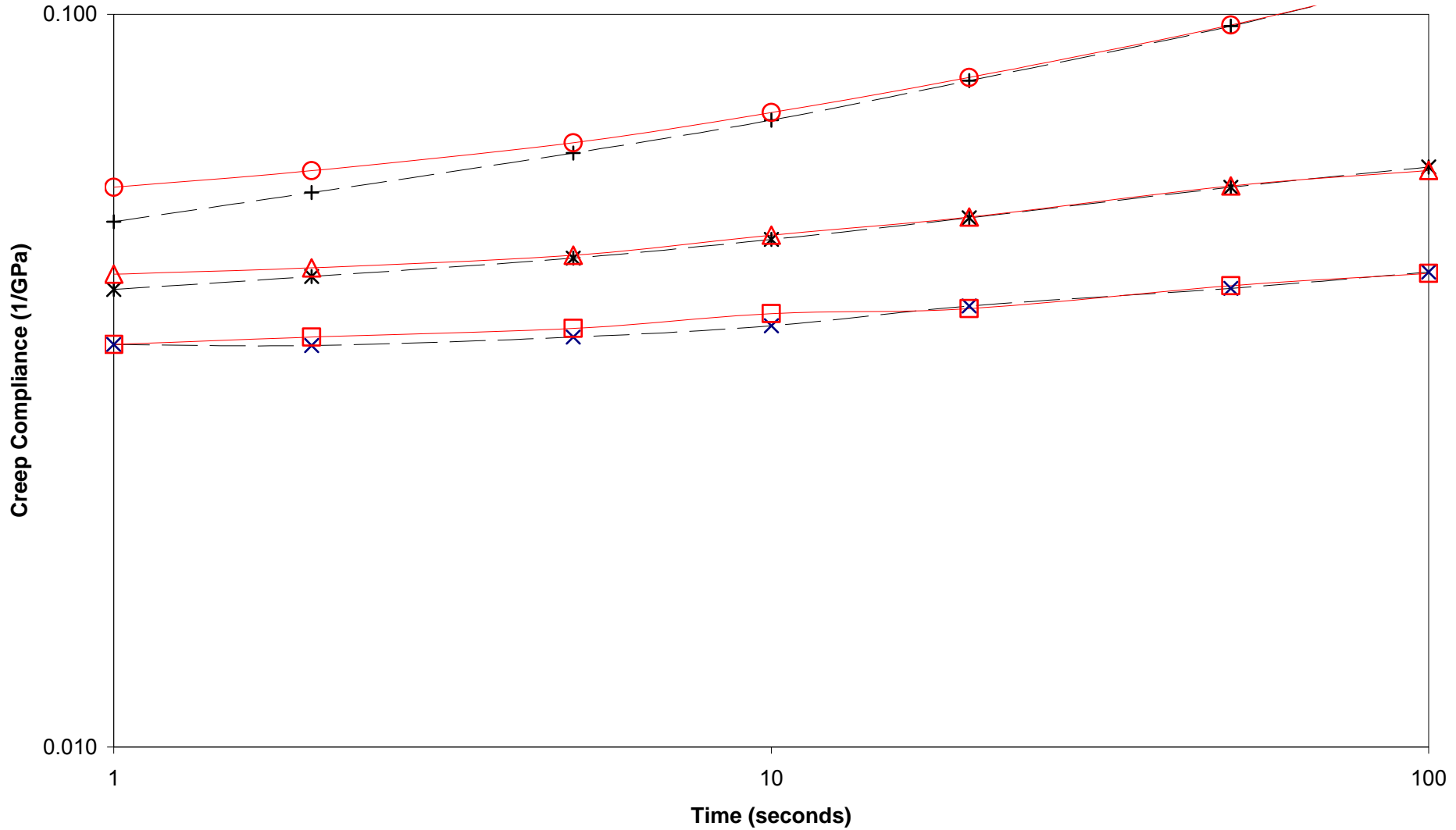
Based on integration of the fitted equation (Eqn 7909), the area under the load-time curve (up to 2.85 sec) is equal to area under the curve of a 1 second true creep load (below).

Areas are equal; 1900 lbf-sec

True Creep Load Profile



Comparison of Calculation Methods 07-123 (BP1)



—x— EqArea-20 —□— Orig-20 —*— EqArea-10 —△— Orig-10 —+— EqArea0 —○— Orig0

Plant-Produced Mixes

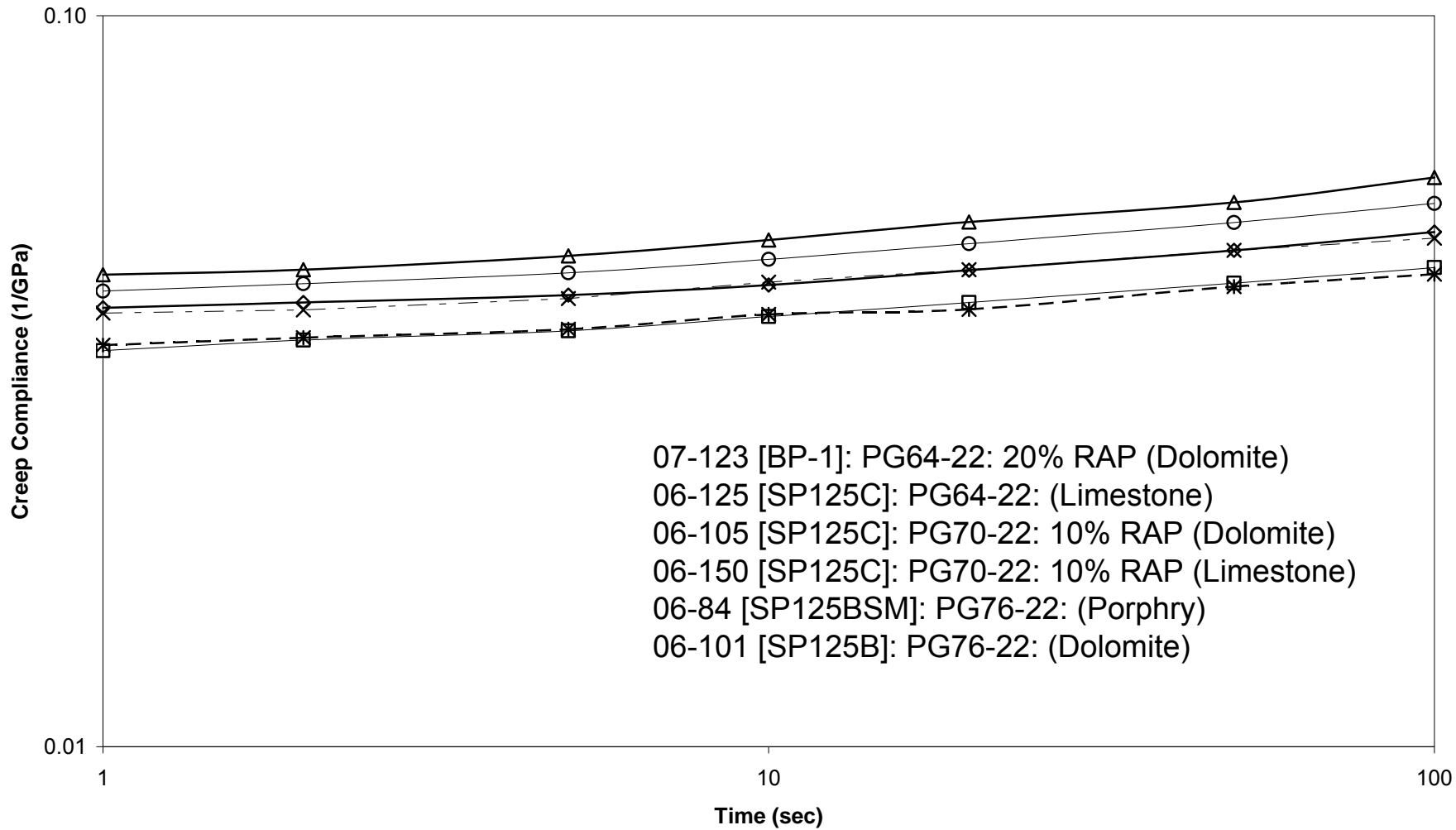
Table 1: HMA Mixes and Target % Air Voids

HMA Mix Type	MoDOT ID [Description] % RAP** (Aggregate Type)	Virgin PG Binder Grade	No. Replicate Tests		
			4% Voids	6.5% Voids	9% Voids
Superpave	06-101 [SP125B] (Dolomite)	76-22 (modified)	3*	3*	3*
Superpave	06-150 [SP125C] 10% RAP (Limestone)	70-22 (modified)	3*	3*	3*
Superpave	06-125 [SP125C] (Limestone)	64-22	3*	3*	3*
Superpave	06-105 [SP125C] 10% RAP (Dolomite)	70-22 (modified)		3	
Superpave (Stone Matrix)	06-84 [SP125BSM] (Porphyry)	76-22 (modified)	3*	3*	3*
Marshall	07-123 [BP-1] 20% RAP (Dolomite)	64-22		3	

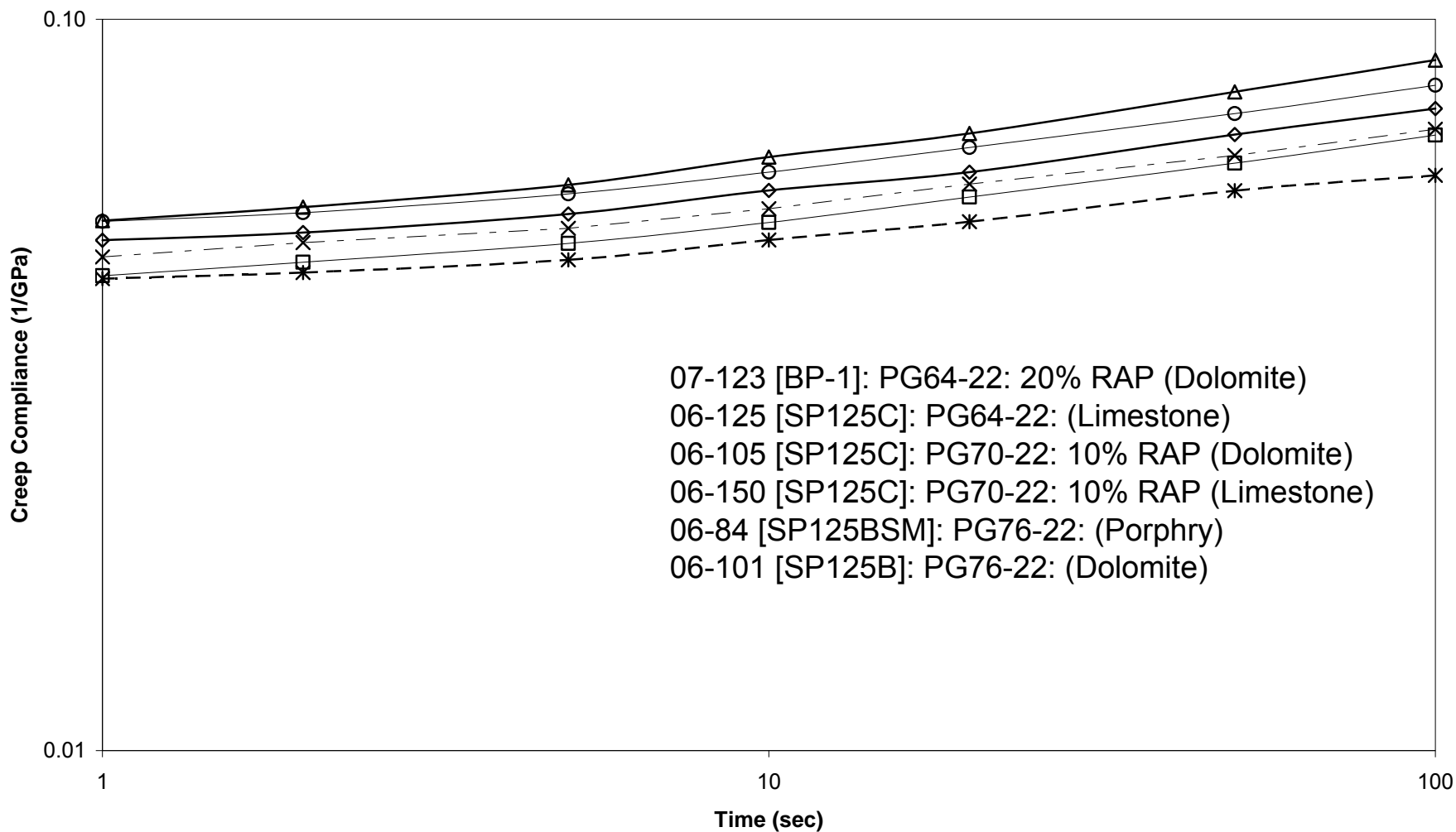
*Additional IDT strength testing at 4.4 and 21°C (40 and 70°F, respectively)

**Recycled Asphalt Pavement

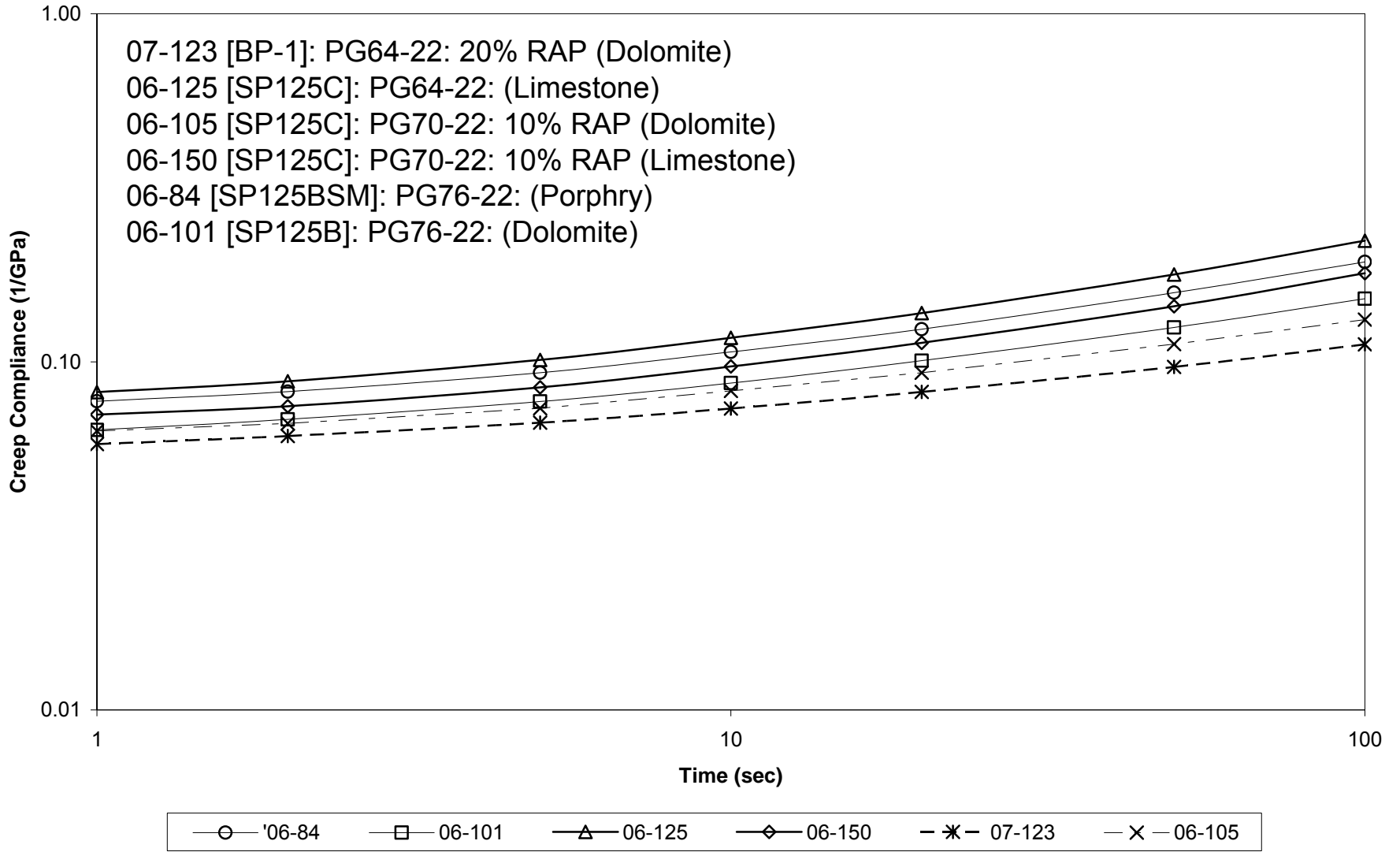
6.5% Voids: -20 deg C



6.5% Voids: -10 deg C



6.5% Voids: 0 deg C

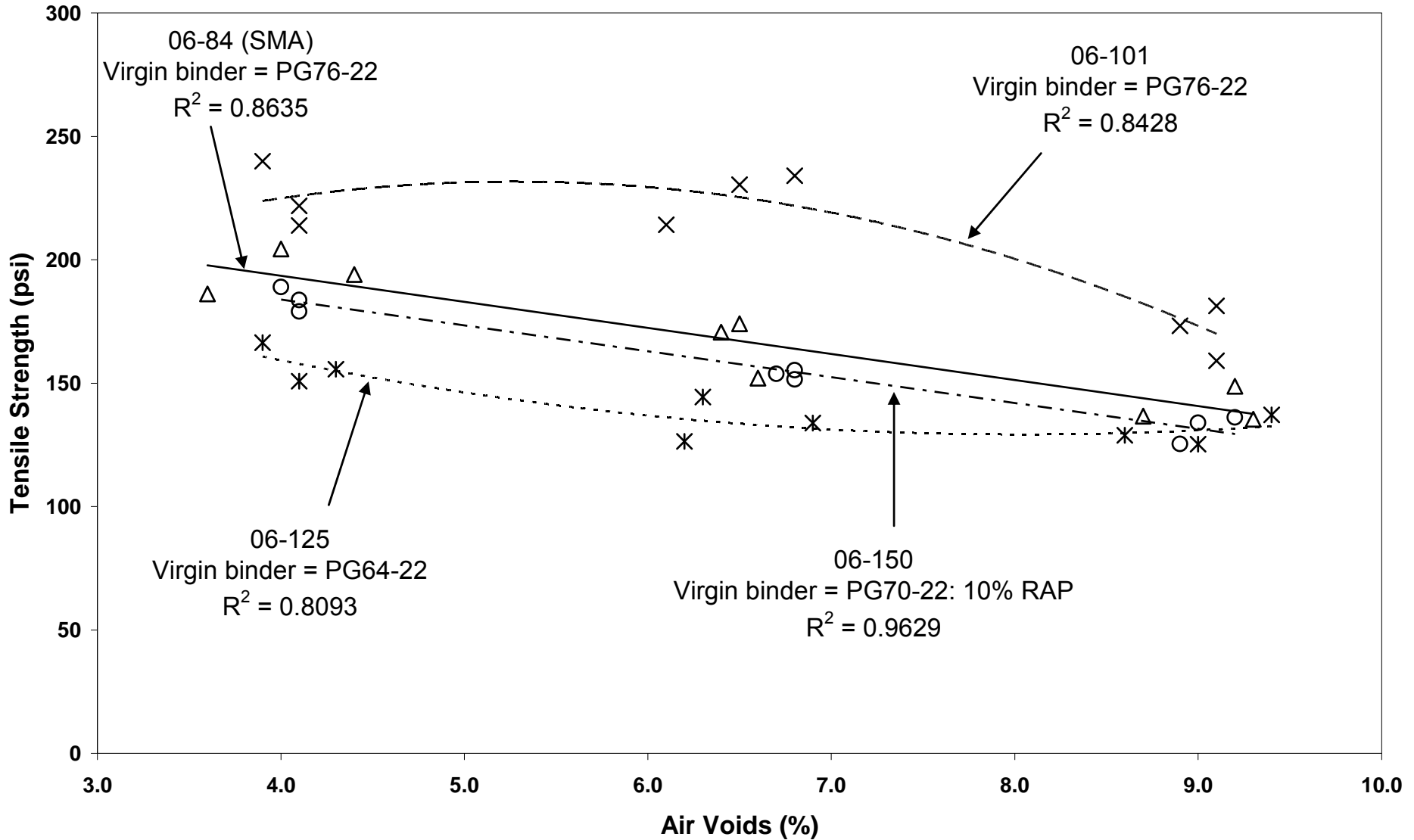


Temp (deg C)	Time (sec)	06-125 (Voids = 4%)		06-125 (Voids = 6.5%)		06-125 (Voids = 9%)	
		D(t) (1/psi)	D(t) (1/Gpa)	D(t) (1/psi)	D(t) (1/Gpa)	D(t) (1/psi)	D(t) (1/Gpa)
-20	1	2.5035E-07	0.03631	3.0510E-07	0.04425	3.3867E-07	0.04912
	2	2.5648E-07	0.03720	3.0997E-07	0.04496	3.4573E-07	0.05014
	5	2.6933E-07	0.03906	3.2352E-07	0.04692	3.5754E-07	0.05186
	10	2.8235E-07	0.04095	3.4009E-07	0.04933	3.7427E-07	0.05428
	20	2.9128E-07	0.04225	3.6010E-07	0.05223	3.9264E-07	0.05695
	50	3.1535E-07	0.04574	3.8300E-07	0.05555	4.1835E-07	0.06068
	100	3.2748E-07	0.04750	4.1431E-07	0.06009	4.4649E-07	0.06476
-10	1	3.3791E-07	0.04901	3.6567E-07	0.05304	4.1683E-07	0.06046
	2	3.4928E-07	0.05066	3.8180E-07	0.05538	4.2892E-07	0.06221
	5	3.7034E-07	0.05371	4.0938E-07	0.05938	4.5714E-07	0.06630
	10	3.9875E-07	0.05783	4.4683E-07	0.06481	4.9356E-07	0.07159
	20	4.2747E-07	0.06200	4.8141E-07	0.06982	5.3069E-07	0.07697
	50	4.7736E-07	0.06924	5.4865E-07	0.07957	5.9145E-07	0.08578
	100	5.2629E-07	0.07633	6.0627E-07	0.08793	6.4465E-07	0.09350
0	1	5.3193E-07	0.07715	5.6385E-07	0.08178	6.7142E-07	0.09738
	2	5.6947E-07	0.08260	6.0557E-07	0.08783	7.1841E-07	0.10420
	5	6.3890E-07	0.09266	6.9872E-07	0.10134	8.1813E-07	0.11866
	10	7.1948E-07	0.10435	8.0840E-07	0.11725	9.3953E-07	0.13627
	20	8.2759E-07	0.12003	9.5273E-07	0.13818	1.0931E-06	0.15854
	50	1.0377E-06	0.15051	1.2298E-06	0.17837	1.3791E-06	0.20002
	100	1.2568E-06	0.18228	1.5379E-06	0.22305	1.6955E-06	0.24591

COMPARISON OF CREEP COMPLIANCE VALUES OF THE 06-125 MIX (PG64-22, NO RAP) TO LEVEL 3 TYPICAL VALUES (UNITS OF 1/GPa)

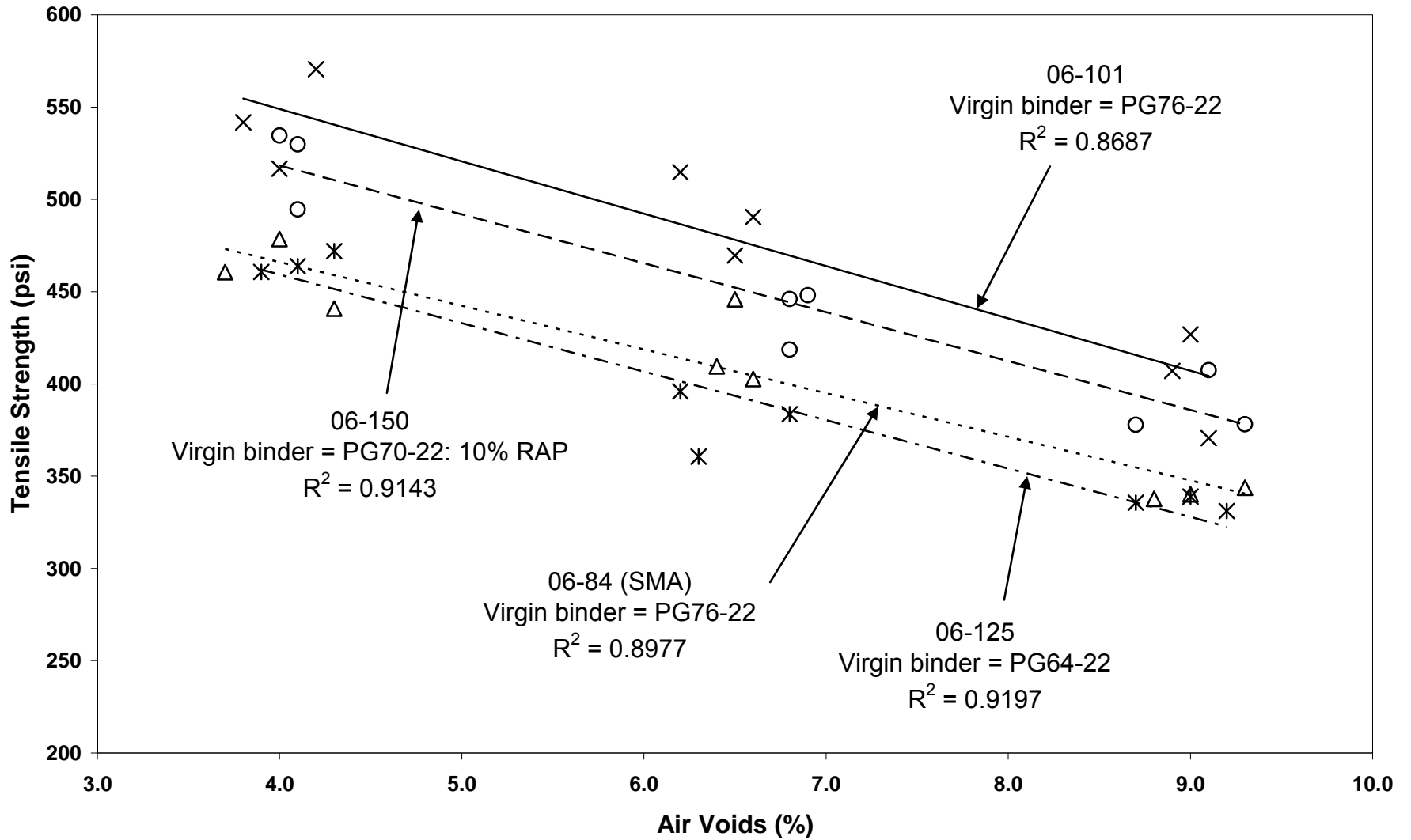
	Time	-20C	-10C	0C
AC-20	1	0.030	0.035	0.062
Pen 60-70	2	0.032	0.039	0.068
PG 64-22	5	0.035	0.043	0.080
	10	0.037	0.047	0.091
	20	0.039	0.051	0.108
	50	0.041	0.057	0.137
	100	0.045	0.059	0.163

Tensile Strength: 21°C (70°F)

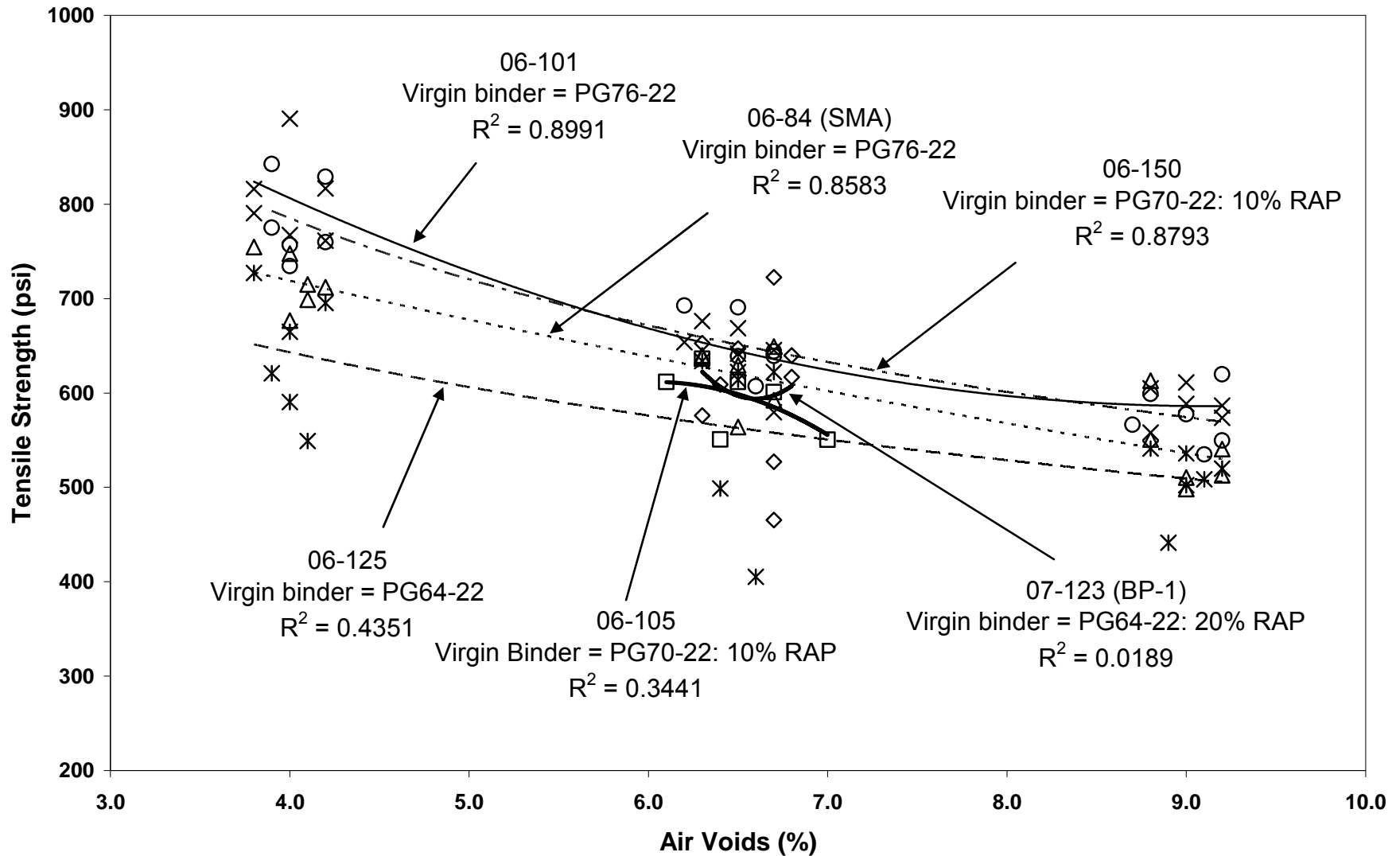


△ '06-84	× 06-101	* 06-125	○ 06-150
— Linear ('06-84)	- - - Poly. (06-101)	- - - Linear (06-150)	- · - · Poly. (06-125)

Tensile Strength: 4.4°C (40°F)



Tensile Strength: -10°C (14°F)



△ '06-84	× 06-101	* 06-125	○ 06-150
◇ 07-123	□ 06-105	--- Log. (06-125)	— Poly. (06-101)
..... Poly. ('06-84)	--- Power (06-150)	— Poly. (06-105)	— Poly. (07-123)