

# **Autofrettage: Measuring Residual Stress** in High Performance Fuel Systems

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Cummins Fuel Systems produces high pressure common fuel rail systems for diesel engines. The rails must withstand high cyclic pressures during operation. To increase fatigue resistance, Cummins uses autofrettage (AF) to induce compressive residual stresses in the rails. Cummins wants to reduce the costs associated with common fuel rail systems by determining a cheaper and faster method to assess fuel rail reliability. Four test methods were developed to measure residual stresses in the rails: Vicker's hardness, XRD, residual stress estimation by cutting, and eddy current measurements. The test methods were evaluated by comparing results to expected residual stress values and finite element analysis results to determine feasibility.



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# **Project Background**

#### **Problem Statement**

Cummins fuel rails are autofrettaged (AF) to create residual compressive stresses which strengthen the

### Results

#### Microhardness Test

Student T test determined that hardness values of AF

# Discussion

- Finite Element Analysis
- FEA model estimated
  - depth of residual stress



inner surface and lengthen the fatigue life of the rails.

#### Goal

Determine a faster, cheaper, and preferably nondestructive method to measure residual stresses in

fuel rails due to AF

#### Autofrettage (AF) AF is a strengthening



technique in which internal Photograph of Cummins fuel rail pressure is applied to plastically deform the inner surface of a cylinder, inducing compressive residual stresses near the inner diameter and tensile residual stress near the outer diameter. Finite element



analysis (FEA) modeling provided an estimate of depth and peak residual stress within AF fuel rails.

Schematic of residual stresses due to AF<sup>[1]</sup>

#### Sample Compositions

Mini fuel rails composed of 4 steel alloys

- 38MnSiVS5 (38Mn)
- Metasco MC 25MnCrSiVB6 (25Mn)
- 3. AISI 4140 (4140)



indent (pictured indicated microhardness below) testing was inconclusive.



Best fit lines of average Vicker's Hardness values measured on 4140 AF and NAF, and 25MnCrSiVB6 AF and NAF samples.

#### **Residual Stress Measurement by XRD**

Measurements showed tensile stresses at outer diameter and compressive stress at inner diameter. (tabulated measurements The below) were reasonable compared to the expected compressive residual stress = -690 MPa.

#### **Table 1.** Residual Stress Measurements of AF samples by XRD



Near drilling Far drilling

of 90 µm and peak radial stress of -29 MPa for a 4140 rail

#### Microhardness Test

- Expected hardness gradient increasing from ID to OD not observed
- High standard deviations for each indent led to statistically insignificant results
- The plastically stressed region was approximately equivalent to indent spacing

#### **Residual Stress Measurement by XRD**

- Nondestructive if tensile stresses at OD correlated to compressive stresses at ID
- Results near drilling are less accurate due to increased surface roughness.
- Different amounts of residual stresses in each alloy due to differences in yield stress.

#### Cutting Test

- Indicated presence of residual stresses
- Calculation based on thin tube geometry and linear stress profile gave qualitative results.
- Inaccurate residual stress calculations may occur

# 4. AISI 1045 (1045)



#### **Residual Stress Measurement by XRD**



Measured using  $\sin^2 \psi$ method<sup>[3]</sup> at Cummins Fuel Systems

Tests at outer diameter (OD) (unsectioned), near and far from drilling (sectioned longitudinally)

(1)

**Residual Stress Estimation by Cutting** Cut

	Stress (MPa)	Stress (MPa)	Stress (MPa)
38Mn	364.6 ± 10.0	-447.3 ± 10.0	-351.6 ± 7.6
25Mn	218.8 ± 18.1	-552.5 ± 12.8	-351.3 ± 8.3
4140	315.1 ± 8.6	-423.2 ± 7.8	-437.0 ± 7.8
1045	739.3 ± 9.0	-337.8 ± 9.3	-360.8 ± 7.1

#### **Residual Stress Estimation by Cutting**

AF samples increased in diameter after cutting indicating maximum tensile stress located at outer diameter. NAF samples showed residual stresses <10 MPa, much lower than the stresses for AF samples.

#### Eddy Current Test



 
 Table 2. Residual Stress of AF
 samples by Cutting



1045

# Estimated Sample

125



from heating during cutting and/or measurement



#### Eddy Current Test

- No conclusive pattern was observed in the distribution of results, although results do show thinning for AF rails.
- Rail geometry greatly affects the test results. The ports, welds, and intersection between the ports all have an effect on the recorded impedance values.

# Recommendations

Of the developed techniques, XRD and Estimation by Cutting provided the most useful results. XRD is ideal for providing quantitative measurements nondestructively. Estimation by Cutting provides a rapid, qualitative indication of the presence of residual stresses.

# (ASTM E1928-13)<sup>[4]</sup>

Transverse cross sections cut through thickness as shown.

Compared AF/NAF samples of alloys Surface stress ( $\sigma$ ) calculated by Equation 1<sup>[4]</sup> where E=elastic modulus, D=diameter (before or after cut), µ=Poisson's ratio

$$\sigma = \frac{Et(D_{after} - D_{before})}{2D_{before}D_{after}(1 - \mu^2)}$$

Eddy Current Test Eddy Current Tester: ZETEC MIZ - 10A Probe: ID probe from GE with 6.8mm diameter Impedance change reflects thickness variation in the rail walls, which is affected by residual stresses. Data points at equal spacings from rail end to end

plots, the results are unstable and impedance peaks occur at port positions, which are indicated by vertical lines. AF rails generally showed more points with higher impedance values than NAF rails, but the impedance values were

across the rail and too similar to be conclusive.

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#### **References:**

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