

**Abstract:** Ductile iron (DI) is a cast ferrous alloy that can be used for engine components. Several DI grades were tested, including ASTM A439 D5S, SiMo 5-1, SiMo with Vanadium additions (SiMo+V), and SAE J2582. A SiMo 5-1 alloy was designed and cast in the SMART Foundry in Lambertus Hall. This study determined the oxidation resistance of various grades of DI through oxidation testing at 760°C and 850°C for 500 hours and observing the change using microscopy techniques. SiMo+V had the smallest oxide growth at 760°C and ranked second to ASTM A439 D5S at 850°C. At both temperatures, ASTM A439 D5S experienced significant spallation of the positive oxide layer.

This work is sponsored by Caterpillar,  
Lafayette, IN



## Background

### Caterpillar Engines – Exhaust Systems

- Used in stationary systems and class 9 vehicles
- Sustained and cyclic high temperatures
- DI is common for high stress and thermal exposure [1]

### Ductile Iron

- Strong, ductile, unique microstructure
- Commonly have a ferritic or austenitic matrix
- Different grades of DI control oxidation through carbide production, eutectic adjustments, and matrix transition temperatures [2]
- Ni promotes an austenitic matrix
- Mo, Si, and V form carbides

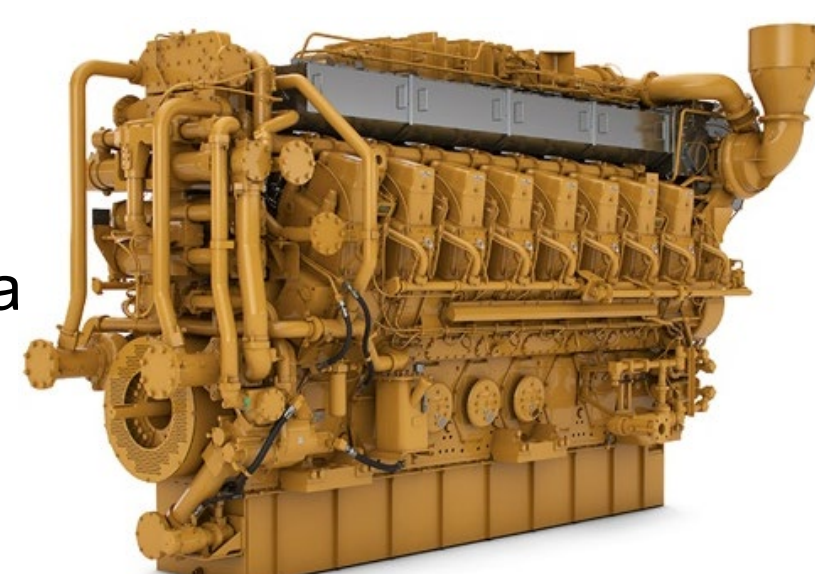


Figure 1. CAT G3600 Engine.

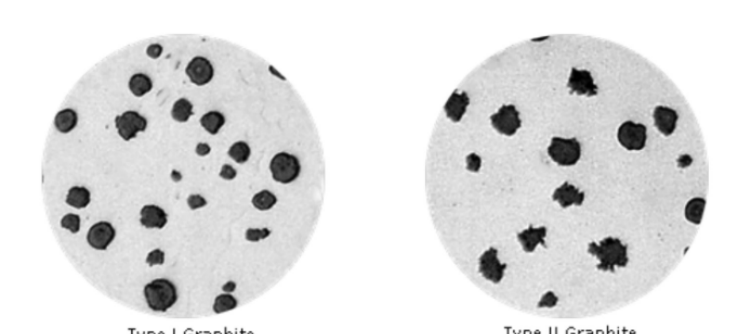


Figure 2. Graphite nodule morphology characteristic to DI. [3]

### Oxidation

- Oxidation is expected to follow a logarithmic growth with active and passive layer formation over time [4]
- Layer growth is expected to level off with time - "protective oxide"
- Although most oxidation is expected in the first 500 hours, industry standard test for new material validation is 1,000 hours [4, 5]

### Objectives

- Evaluation and characterization of four high temperature cast iron materials (ASTM A439 D5S, SiMo 5-1, SiMo+V, SAE J2582) to understand material properties and process impacts on castings for gas engine applications
- Compare oxidation resistance between as-cast and machined surfaces
- Design of a SiMo 5-1 alloy to be cast in the Caterpillar SMART Foundry in Lambertus Hall

## Materials & Methods

### Materials

- Materials studied include Ni-based ASTM A439 D5S, SiMo+V, SiMo 5-1, and SAE J2582

Table 2. Material composition of three of the materials studied, balanced with iron [6, 7, 8].

Grade	C (wt%)	Si (wt%)	Mn (wt%)	Mo (wt%)	V (wt%)	Cr (wt%)	Ni (wt%)
SiMo 5-1	-	4.80 - 5.20	-	0.80 - 1.10	-	-	-
SiMo+V	3.20 - 3.80	4.00 - 5.00	-	0.75 - 1.20	0.60 max	-	-
ASTM A439 D5S	2.00 Max	4.00 - 6.00	0.50 - 1.50	-	-	1.50 - 2.50	34.00 - 36.00
SAE J2582	3.00 - 3.80	3.50 - 4.50	0.10 - 0.50	0.51 - 0.70	-	-	-

### Homogenization Treatment

- To reduce microsegregation in the castings, all bars were homogenized in Carbolite furnace

Table 3. Heat treatment schedules, cooled in air.

Type	Soak Time	Soak Temperature	Cooling Rate	Cool to
SiMo 5-1	1 hr	770 - 820°C	~102 minutes	650°C
SiMo+V	2 hr	771 - 820°C	~102 minutes	650°C
ASTM A439 D5S	1 hr	620 - 650°C	~102 minutes	310°C
SAE J2582	4 hr	790°C	~80 minutes	370°C

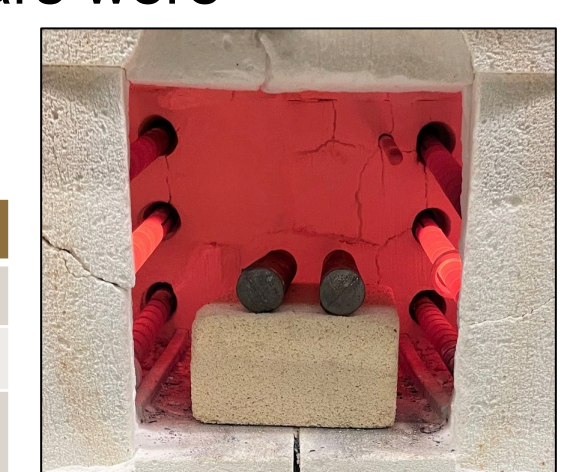


Figure 1. Homogenization Treatment of Bars.

### Sectioning

- Bars were sectioned after heat treat to create samples for oxidation and tensile testing

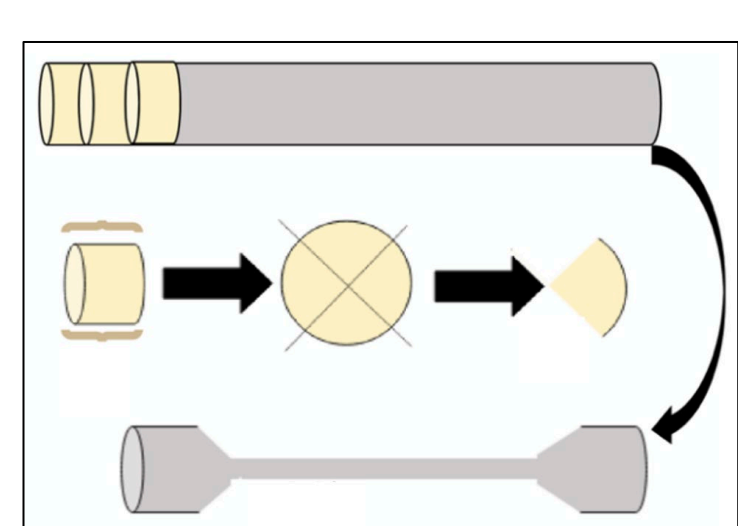


Figure 2. Sectioning diagram.



Figure 3. Oxidation Testing.

### Oxidation Testing

- Oxidation formation was tested at 760°C and 850°C in air using a Thermo Scientific furnace
- Oxidation tests were conducted for about 500 hours each to capture the majority of oxidation growth
- Each sample was weighed and measured with calipers before and after oxidation testing

### Scanning Electron Microscopy (SEM) & Elemental Analysis (EDX)

- Each sample was mounted in epoxy or Bakelite and polished using a Buehler Automet 250 autopolisher
- SEMs used: Apreo 2s at HARF and Whistler, and a Teneo Volumscope at Whistler
- Elemental analysis conducted on the Apreo 2s at Whistler. For EDX samples were sputter coated with a 10 nm layer of Platinum

### Metallography

- Samples were repolished for optical imaging using a Leco polishing wheel and 3 µm diamond paste
- 2% Nital was used to etch for 10 seconds
- Images taken using an Olympus BX41M optical microscope

## Discussion & Results

### Oxidation Testing Results

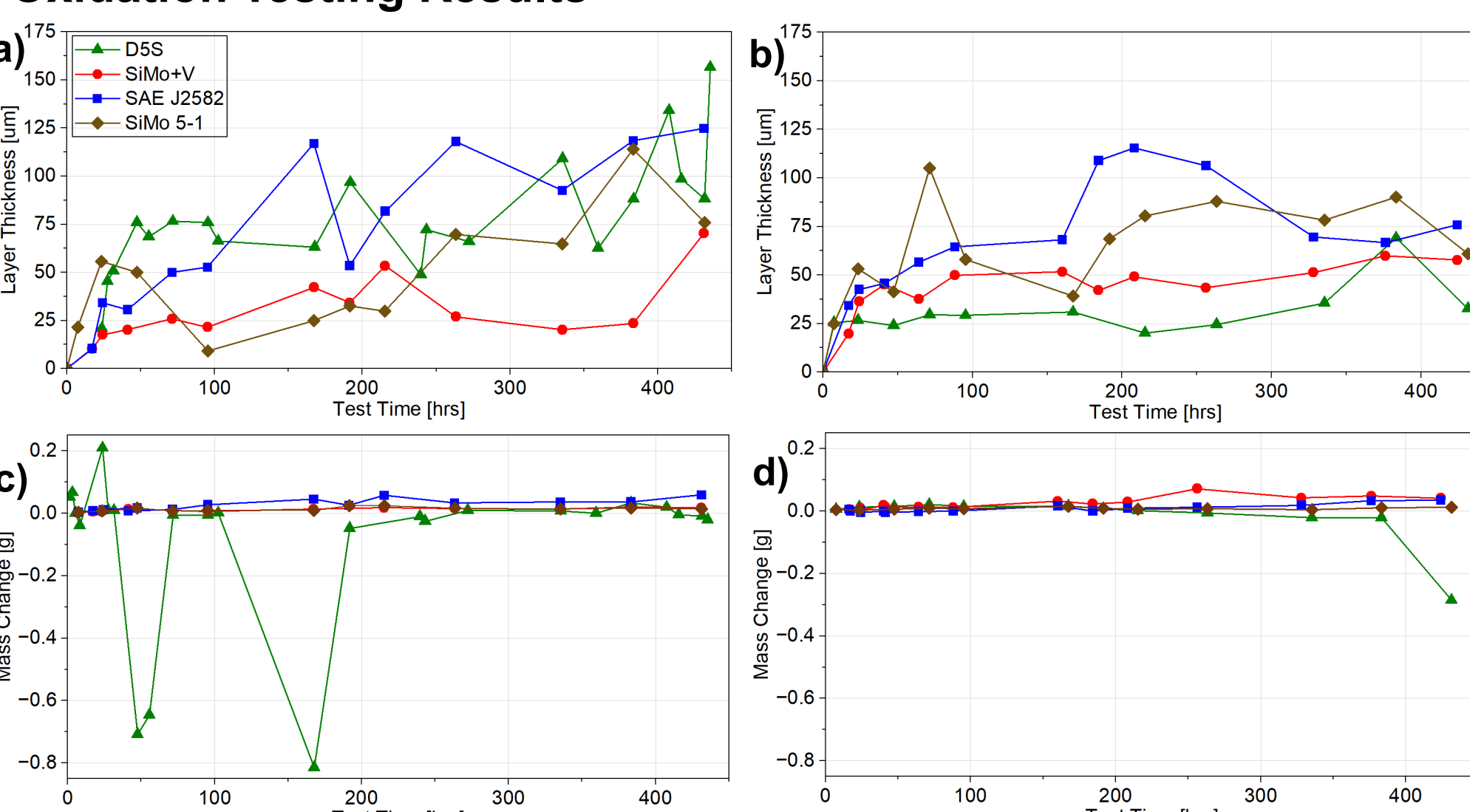


Figure 3. Oxidation testing results over time including negative layer thickness at a) 760°C and b) 850°C and mass change at c) 760°C and d) 850°C.

- Negative oxide layer growth over time for the cast surface of each alloy is graphed in Fig. 3. Using a T-test, there was no statistically significant difference in the oxide layer thickness between the cast and cut surface of ASTM A349 D5S at 760°C and J2582 and SiMo 5-1 at 850°C

### Scanning Electron Microscopy

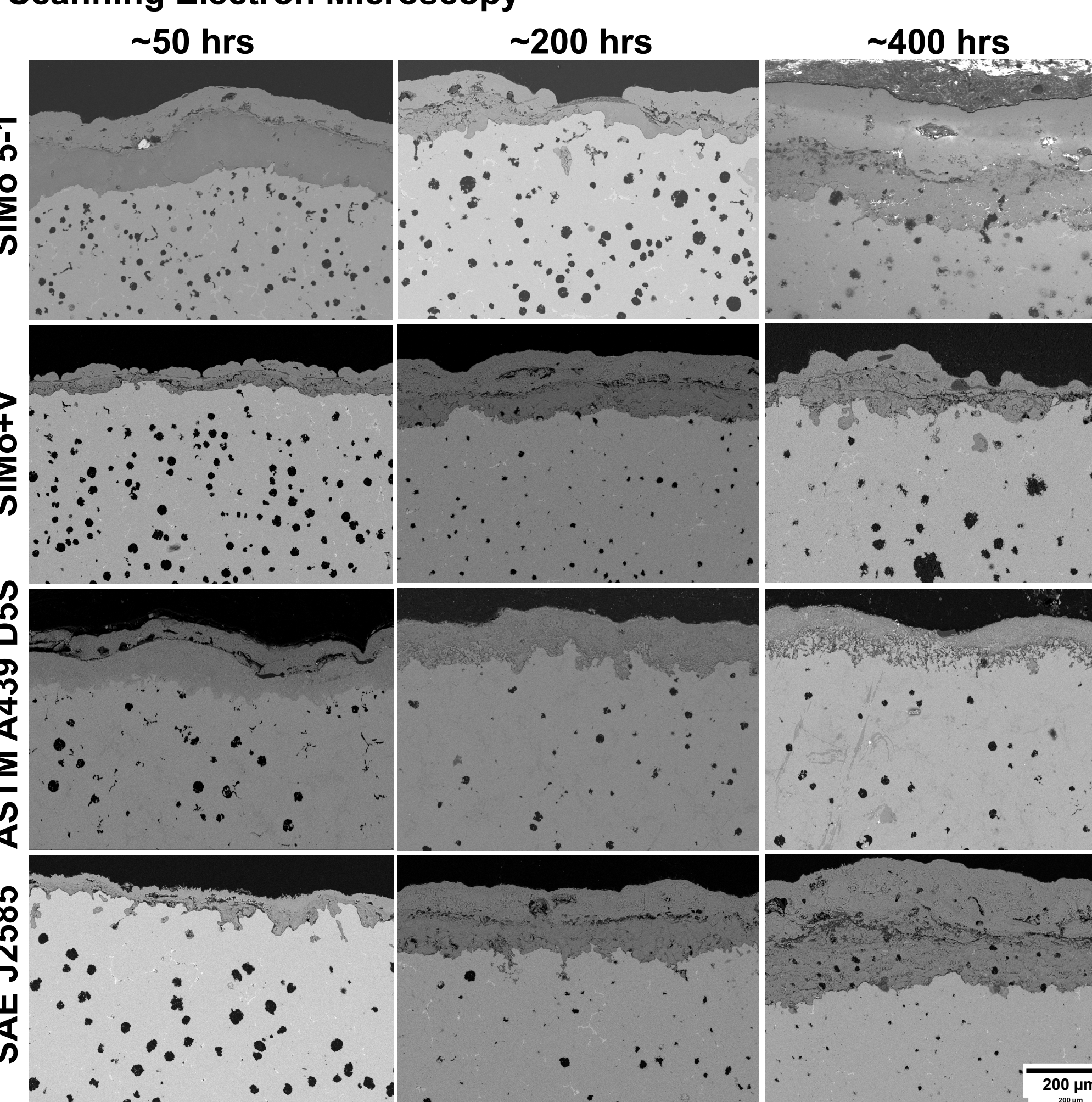


Figure 4. Oxide layers on the cast edge of SiMo 5-1, SiMo+V, ASTM A439 D5S and SAE J2582. Tested in air at 760°C. Spallation occurred on ASTM A439 D5S samples so only the negative layer is visible at ~200 hrs and ~400 hrs.

### Elemental Analysis

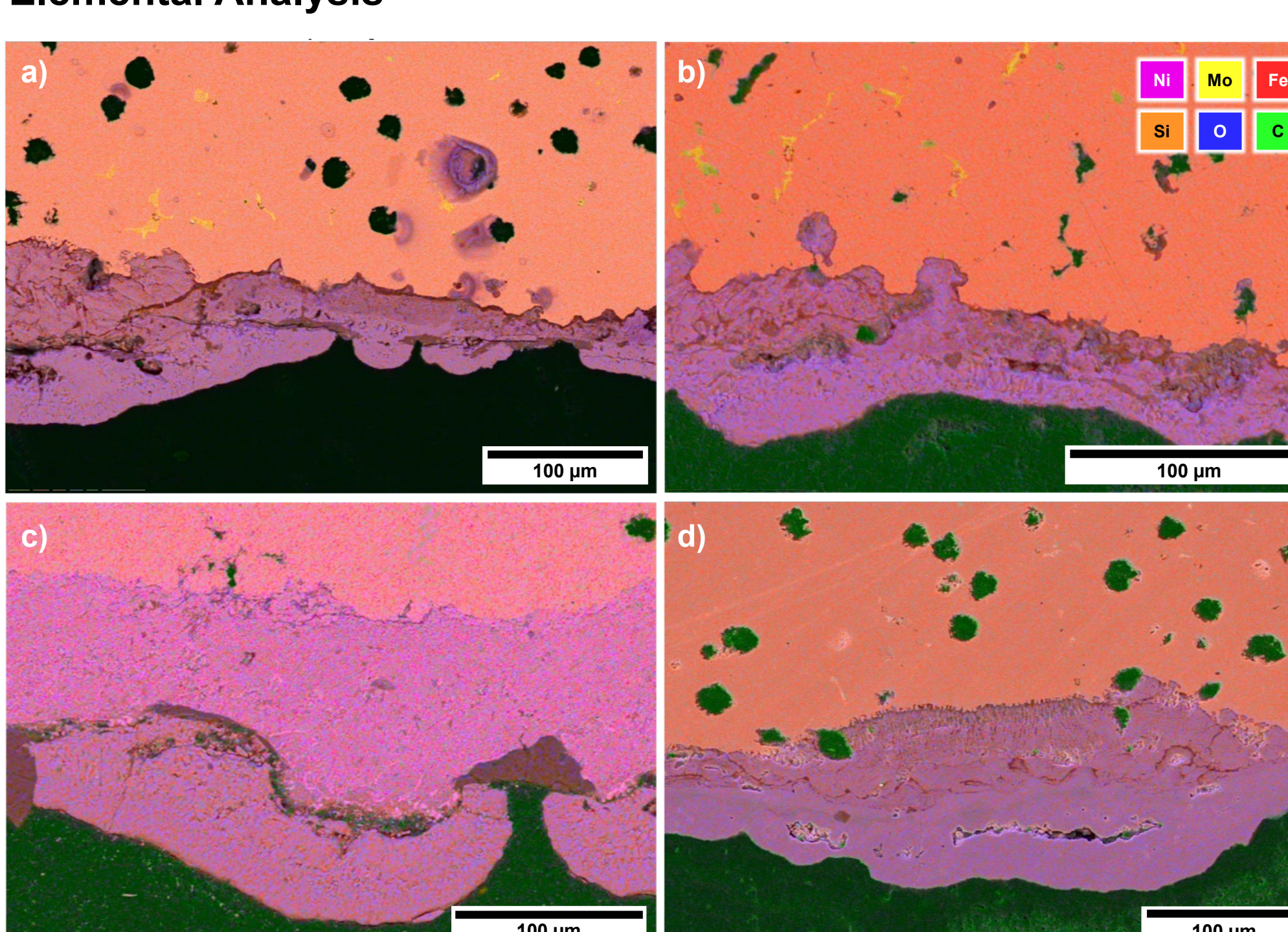


Figure 5. EDX maps of the cast surface oxide layers of a) SiMo 5-1, b) SiMo+V, c) ASTM A439 D5S and d) SAE J2582 at ~95 hrs in an oxidation test in air at 760°C.

Table 4. Composition of the negative oxide layer of the cast surface of four alloys after ~95 hrs at 760°C.

Element	SiMo 5-1	SiMo +V	D5S	SAE J2582
Fe	51.7%	55.1%	28.2%	65.3%
O	26.8%	21%	14.3%	17%
C	13.7%	-	16.9%	11.8%
Si	7.0%	12.1%	4.7%	5.4%
Ni	-	-	34%	-

Table 5. Composition of the positive oxide layer of the cast surface of four alloys after ~95 hrs at 760°C.

Element	SiMo 5-1	SiMo +V	D5S	SAE J2582
Fe	63.1%	71%	59.1%	70.5%
O	26.1%	19.7%	27.3%	18.7%
C	10.2%	-	12.9%	10.8%
Si	0.1%	0.3%	0.1%	-
Ni	-	-	0.6%	-

## Discussion & Results, Cont.

### Metallography

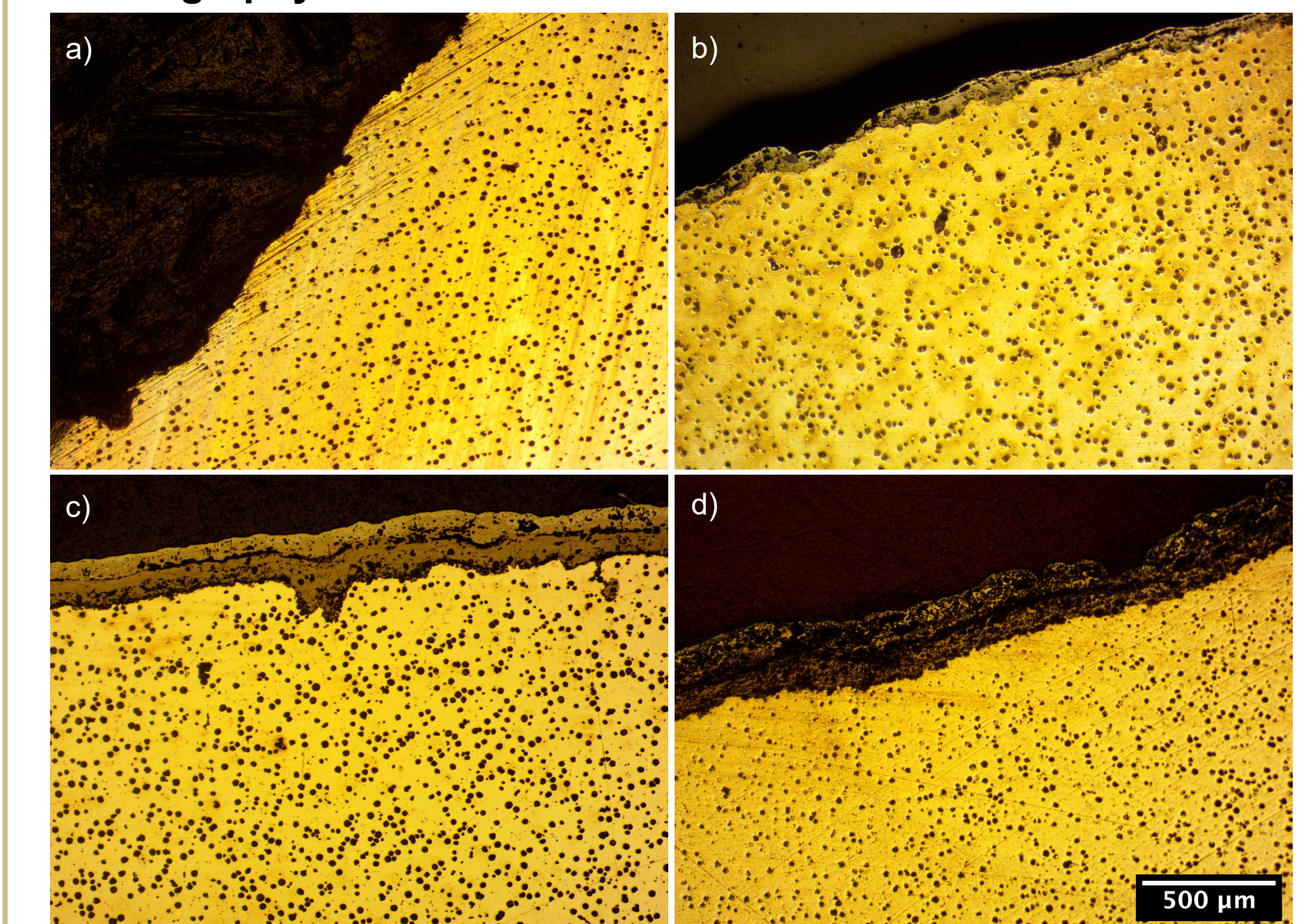


Figure 6. Oxidation Layer development on cast edge during testing at 760C in air after a) heat treat b) 23 hours c) 167 hours d) 383 hours. Etched with 2% Nital.

- The oxide layer appears to have a bilayer that progressively grew throughout the test (refer to Fig. 3 for layer growth measurements)
- The nodules present were rated as ASTM A247 Type I and II for all materials tested for the duration of the oxidation test

## Future Work

### Recommendations

- Understand differences between cut and cast oxide layer growth mechanism
- Continue working with the MET and Purdue SMART Foundry to cast SiMo 5-1 DI
- Characterize other austenitic ductile iron to determine whether spallation of oxide layer is a characteristic feature of austenitic grades

### Future Work

- Continue casting SiMo 5-1 alloy in the Purdue SMART Foundry. Work was completed to design the alloy, initial charge, and mold. The expected range of the carbon equivalent is 4.3% - 5.2%



Figure 7. SiMo 5-1 DI pour in the SMART Foundry completed with MET.

Table 6. Designed chemistry of SiMo 5-1 alloy for casting.

Element	Targets
C	2.80% - 3.00%
Si	4.50% - 6.50%
Ni	<0.30%
Cr	<0.15%
Mo	0.75% - 1.25%
Cu	<0.30%
S	<0.01%
P	<0.05%

## Acknowledgements

The authors would like to thank the Mechanical Engineering Technology (MET) Capstone team (Tiansu Chu, Ilya Kachuro, Jack Klopfenstein, Evan Steinmetz, and Blake Strawsma) and the MET staff and faculty (Prof. Tyler Blowers, Prof. Xiaoming Wang, and Clayton Kibbey) and graduate students Nathan Gehmlich and Donovan Simonton.

## References

- ASM International Handbook Committee, "Ductile Iron Applications," in *ASM Handbook, Volume 01 - Properties and Selection: Irons, Steels, and High-Performance Alloys*, pp. 33-41, 1990.
- Davis, J.R. (2001). *Alloying - Understanding the Basics*. ASM International.
- ASTM International. (2024). Standard Test Method for Visual Evaluation of Graphite in Iron Castings (ASTM A247-24). ASTM International. <https://doi.org/10.1520/A0247-24A247-24>
- Stawarz, M., & Nuckowski, P. M. (2020). Effect of Mo Addition on the Chemical Corrosion Process of SiMo Cast Iron. *Materials*, 13(7), 1745. <https://doi.org/10.3390/ma13071745>
- G.A. Celik, F. Kahriman, S.H. Atapek, S. Polat, "Characterization of the high temperature oxidation behavior of iron based alloys used as exhaust manifolds," in *MATEC Web of Conferences*, vol. 188, 2018, doi: <https://doi.org/10.1051/mateconf/201818802001>
- SAE International. (2017). J2582: Automotive Ductile Iron Castings for High Temperature Applications (SAE J2582, Issued 2001-12; Revised 2004-06; Stabilized 2018-01; Superseding J2582 JUN2004). SAE International.
- ASTM International. (2023). Standard Specification for High-Silicon Molybdenum Ferritic Iron Castings (ASTM A1095-15 (Reapproved 2023)). ASTM International. <https://doi.org/10.1520/A1095-15R23>
- ASTM International. (2022). Standard Specification for Austenitic Ductile Iron Castings (ASTM A439/A439M-18 (Reapproved 2022)). ASTM International. <https://doi.org/10.1520/A0439M-18R22>