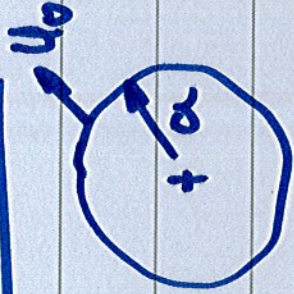


Source * point source



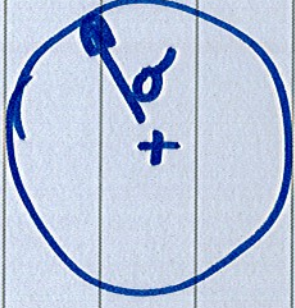
$$kr \ll 1$$

$$\hat{p} = i\rho_0 c \frac{kQ}{4\pi r} e^{-ikr} \quad \checkmark$$

Q = volume velocity

point monopole

$$\lim_{kr \rightarrow 0} I_r = \frac{\mu_0 c k^2 Q^2}{2 (4\pi r)^2}$$



$$Q = \frac{4\pi r^2 U_0}{3}$$

$$I_r \propto a^4$$

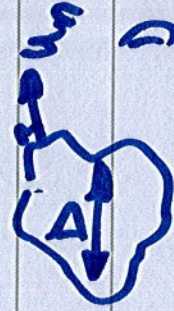
rapid increase in
intensity as source
size increases

- small sources
 \searrow very poor radiators

- Use a point monopole to represent
 any compact source
 that periodically changes volume
 and displace Q volume/s

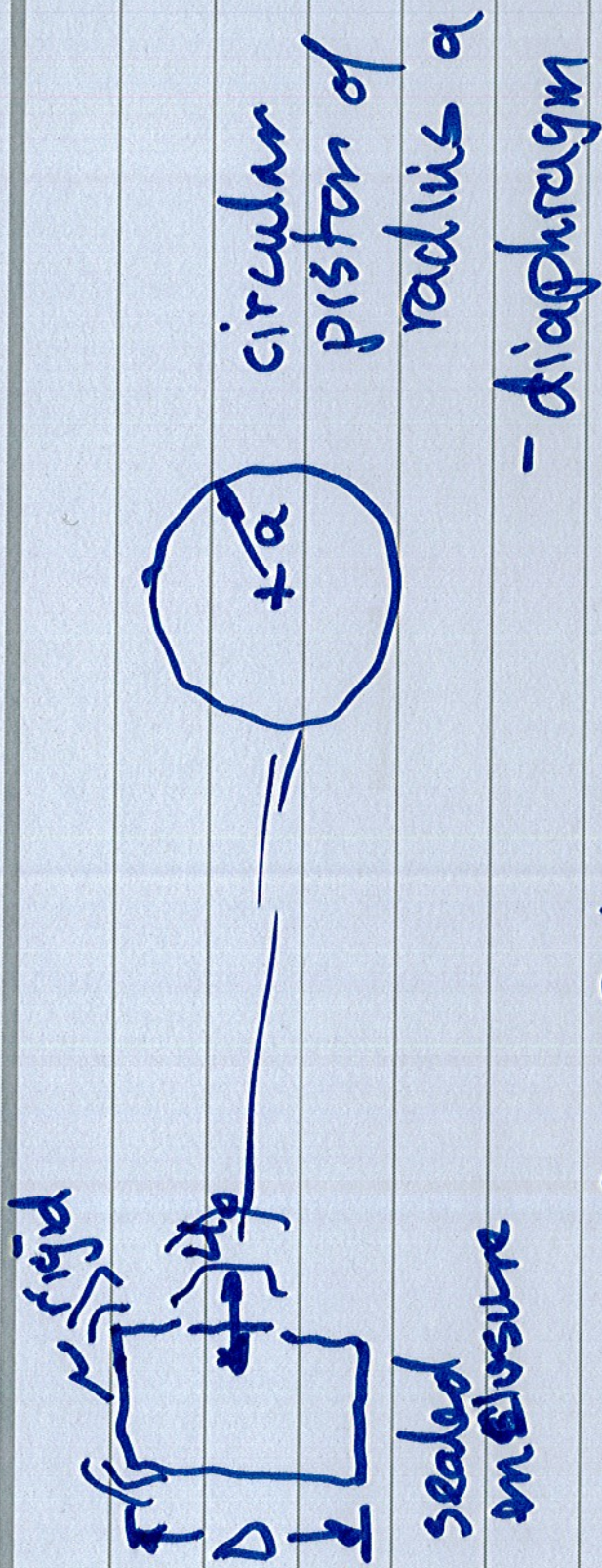
- for a compact source ($D \ll \lambda$)

The sound radiation does
 not depend on the spatial
 distribution of the source
 velocity



$$Q = \int \text{volume} \left[\frac{m^3}{s} \right]$$

$$D \ll \lambda$$



$$Q = \pi a^2 U_0$$

so long as $D \ll \lambda$

replace the l/s by a point monopole.

$$P(r) = j \rho c k Q \frac{e^{-ikr}}{4\pi r} \quad \left. \begin{array}{l} \text{free} \\ \text{field} \end{array} \right\}$$

$$W = \rho c k^2 \frac{Q^2}{8\pi}$$

5.3.2 Simple Volume Source

Any source that displaces Φ m³/s and is small compared to a wavelength radiates like a point monopole

$$\oint \mathbf{F} \cdot \mathbf{u}_n \quad Q = \int u_n ds$$



perfect cube

$$Q = \frac{u_0 a^2}{3}$$

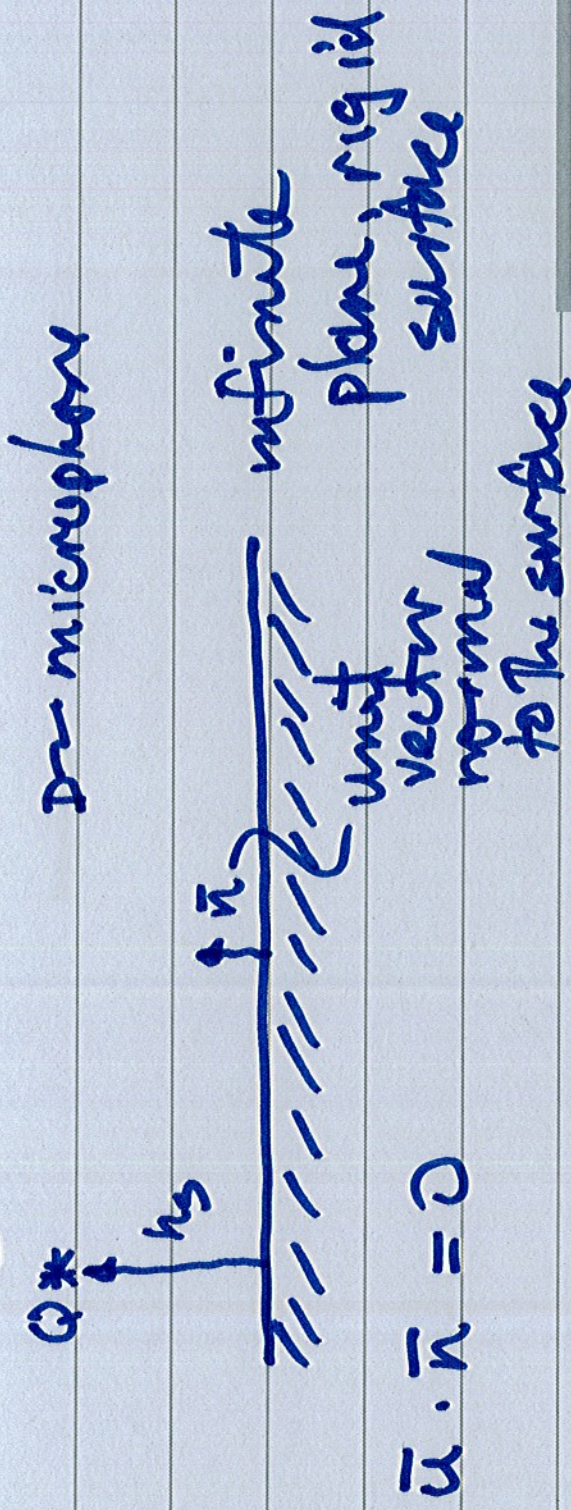
$$a \ll \lambda$$

- some sources do not exhibit
a volume change

\otimes fan] not volume
 \oplus un baffled l/s] ~~not~~ sources

5.3.3 Reflection at a hard surface

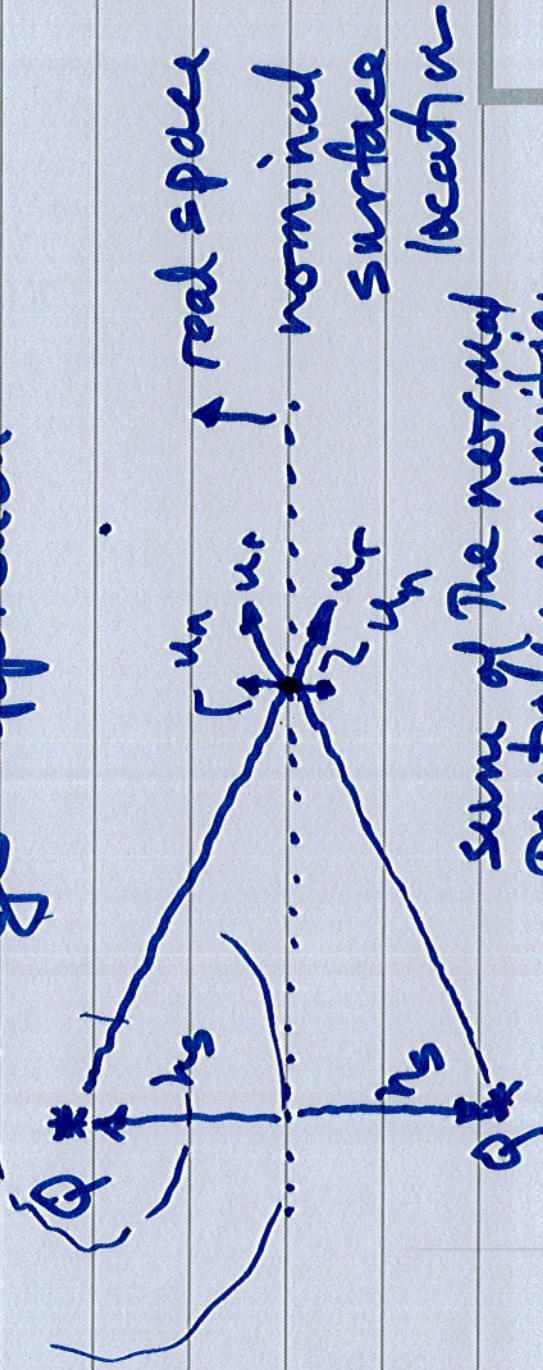
5.3.3.1 Single Reflection



zero normal particle velocity

Equivalent system in free space
which satisfies the b.c.

- image approach

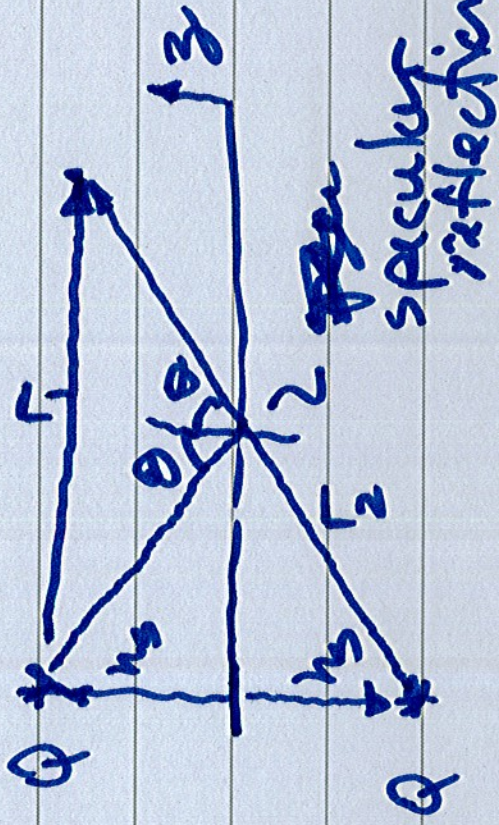


sum of the normal
particle velocities

$\vec{u} \cdot \vec{n} = 0$
is satisfied

surface location

This image source arrangement
is mathematically equivalent to the
real case in region above the surface.



solution
 applies
 in the
 region
 $z \geq 0$

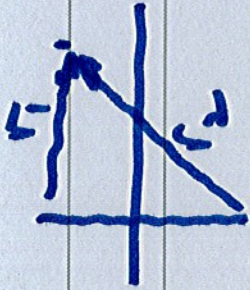
$$\vec{P}_t = \vec{P}_1 + \vec{P}_2$$

$$\vec{P}_t = j\beta c k Q \frac{e^{-ikr_1}}{4\pi r_1} + j\beta c k Q \frac{e^{-ikr_2}}{4\pi r_2}$$

↑
 direct

↑
 reflected

$$\vec{E} = i \rho_0 c \frac{kQ}{4\pi r_1} e^{-ikr_1} \left[\frac{1}{r_1} + \left(\frac{r_1}{r_2} \right) e^{-ik(r_2 - r_1)} \right]$$



reflected
component

$\left(\frac{r_1}{r_2} \right) =$ relative spherical spreading attenuation
 $(r_2 - r_1)$ path length difference

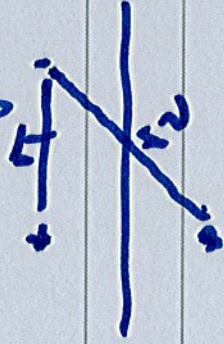
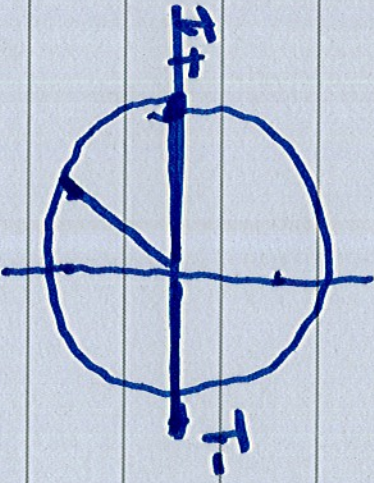
$k(r_2 - r_1) =$ phase difference between direct + reflected signals

$$0 \leq \left(\frac{r_1}{r_2}\right) \leq 1$$

reflected sound is
attenuated w/rt

The direct sound
due to spherical
spreading

$$e^{-jk(r_2-r_1)}$$



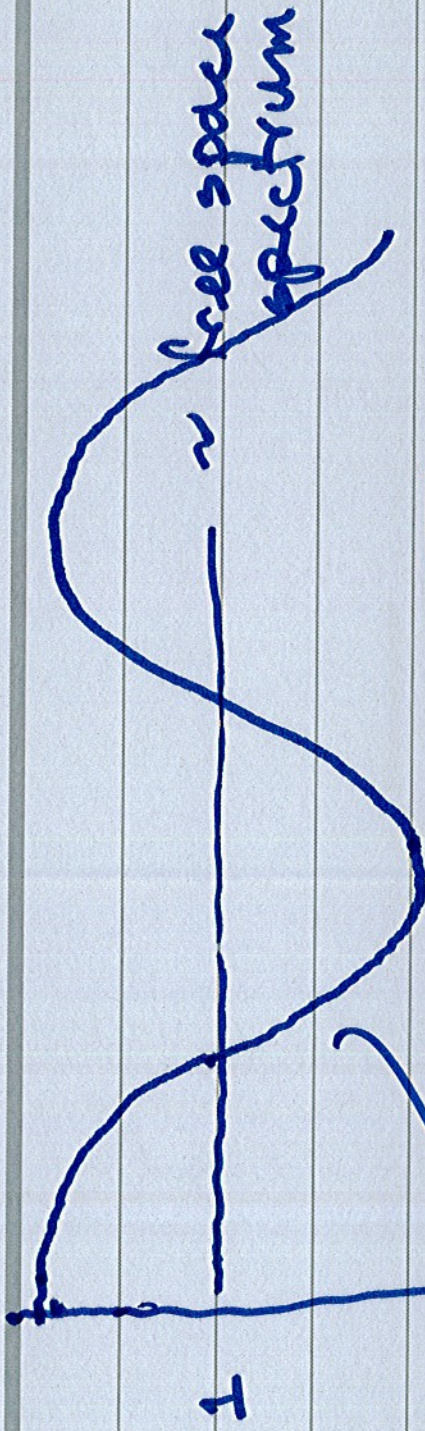
$$k(r_2-r_1) = 0, 2\pi, 4\pi \quad e^{-jk(r_2-r_1)} = 1$$

$$\frac{2\pi}{\lambda}(r_2-r_1) = 2\pi$$

$$(r_2-r_1) = \lambda \quad \text{approximate maximum}$$

$$k(r_2-r_1) = \pi, 3\pi, 5\pi, \dots$$

$$e^{-jk(r_2-r_1)} = -1 \quad (r_2-r_1) = \lambda/2, 3\lambda/2, \dots \quad \text{minimum}$$



magnitude of
the ripple
depends on $\left(\frac{r_1}{r_2}\right)$

Effect of a single reflector
is to add a ripple to the
received spectrum.

