

Snell's Law $\theta_r = \theta_i$

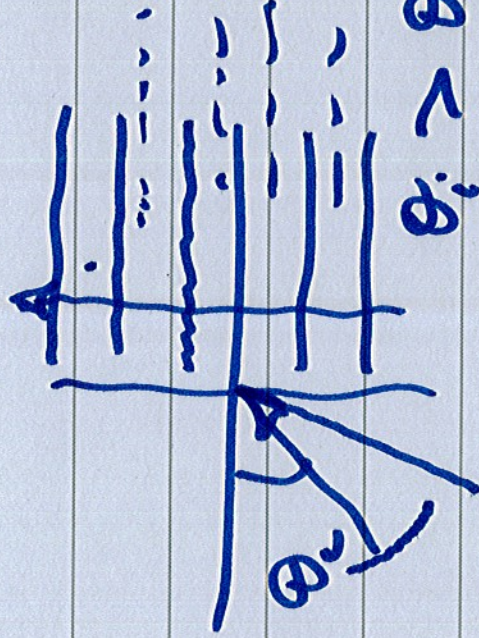
$$\frac{\sin \theta_t}{\sin \theta_i} = \frac{c_1}{c_2}$$

$$R = \frac{c_2 - c_1}{c_2 + c_1} \frac{\sin \theta_i}{\sin \theta_i}$$

$$= \frac{c_2 \cos \theta_i - c_1 \cos \theta_i}{c_2 \cos \theta_i + c_1 \cos \theta_i}$$

$$R = \frac{\epsilon_2 \cos \theta_i - \sqrt{1 - \left(\frac{\epsilon_2}{\epsilon_1}\right)^2} \sin^2 \theta_i}{\epsilon_2 \cos \theta_i + \sqrt{1 - \left(\frac{\epsilon_2}{\epsilon_1}\right)^2} \sin^2 \theta_i}$$

$$\epsilon_2 = \frac{\epsilon_2 c_1}{c_2}$$

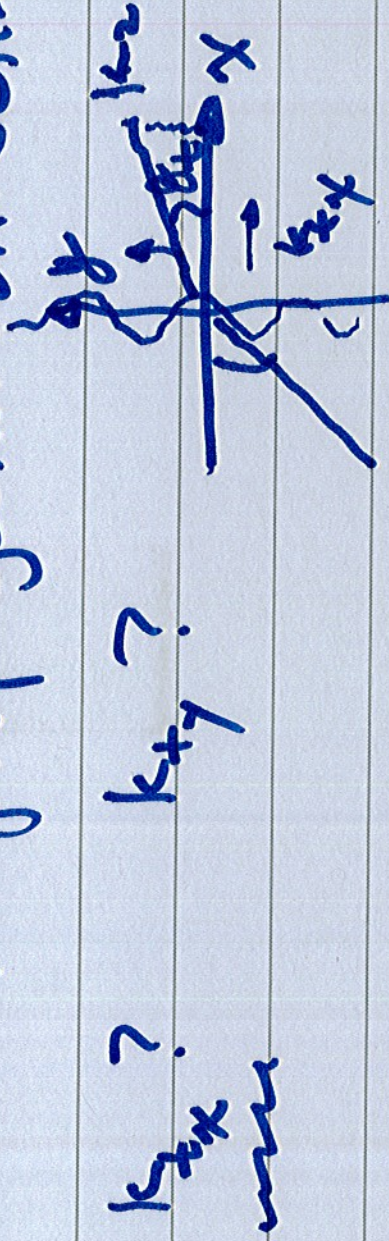


$$= 0$$

$R \rightarrow 1$ Total Reflection

$\theta_i > \theta_c$ what happens

what is the propagation direction



$$k_{1y} = k_2 \sin \theta_2 = k_1 \sin \theta_1$$

because of
pressure continuity

forcing
spatial
pattern

real number

$$k_{tx} = k_2 \cos \theta_4 \quad \cos^2 \theta_4 + \sin^2 \theta_4 = 1$$

even if θ_4 is complex

$$k_{tx} = \pm k_2 \sqrt{1 - \sin^2 \theta_4}$$

$$= \pm k_2 \sqrt{1 - \left(\frac{c_2}{c_1}\right)^2 \sin^2 \theta_i}$$

$$\geq 1$$

$$= \pm \sqrt{-1} k_2 \sqrt{\left(\frac{c_2}{c_1}\right)^2 \sin^2 \theta_i - 1}$$

$$c_2 > c_1$$

+ve number

when $\theta_i > \theta_c$

$$k_{tx} = \pm j\gamma \quad \gamma = k_2 \sqrt{\left(\frac{c_2}{c_1}\right)^2 \sin^2 \theta_i - 1}$$

Sound field in region ②

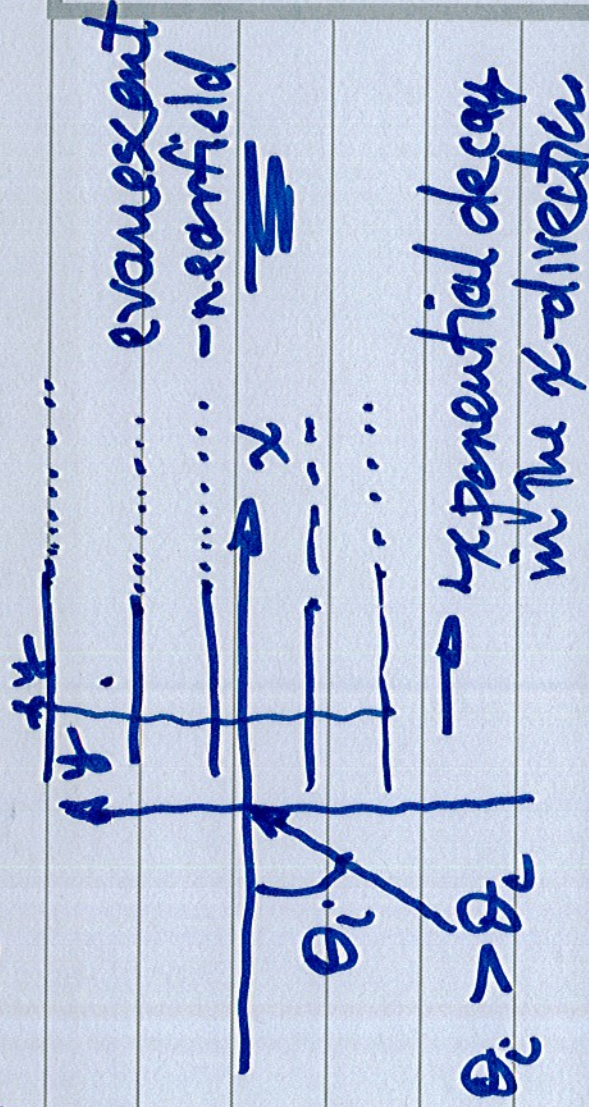
$$\hat{p}_e = P_0 e^{-ik_x x} e^{-i\omega t} \quad k_y = \text{real number}$$

$$e^{-j(\pm j\gamma)x} \quad \text{propagation}$$

exponential growth or decay

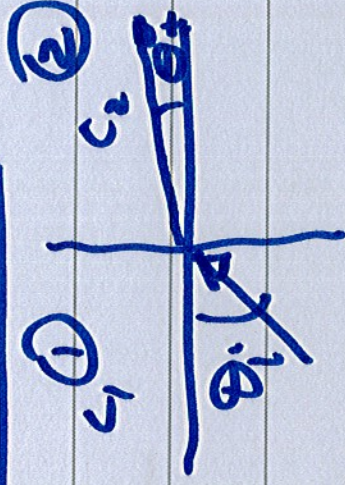
$$e^{+\gamma x} \quad e^{-\gamma x}$$

discard
infinite
region ②



Consequences of Snell's Law

1. From Snell's Law



when $\frac{c_2}{c_1} < 1$

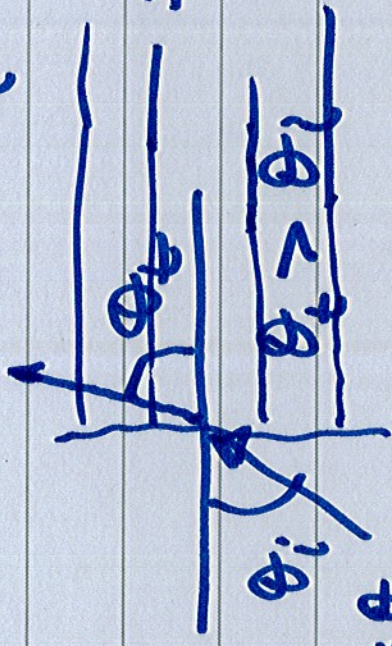
$$\sin \theta_t < \sin \theta_i$$

$$\theta_t < \theta_i$$

"sound refracts towards the normal"

2. if $c_2 > c_1$

$$\sin \theta_t = \frac{c_2}{c_1} \sin \theta_i$$



sound refracts away from

the normal

$\theta_i = \theta_c$

maximum possible real θ_t is $\pi/2$

def'n of θ_c $\sin \theta_c = \frac{c_1}{c_2}$

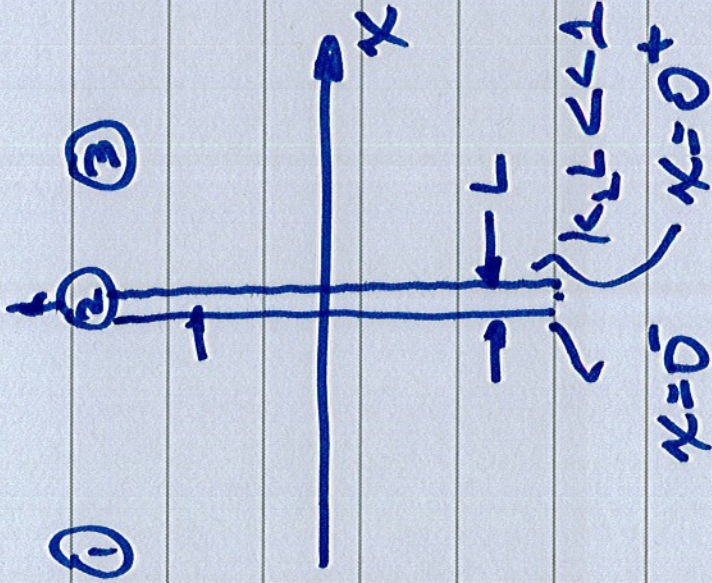
$$\sin \theta_t = 1$$

3. If $\theta_i > \theta_c$

Exponential decay into the second medium

θ_t is then complex

4.3.2 Reflection and Transmission at a Thin, limp panel



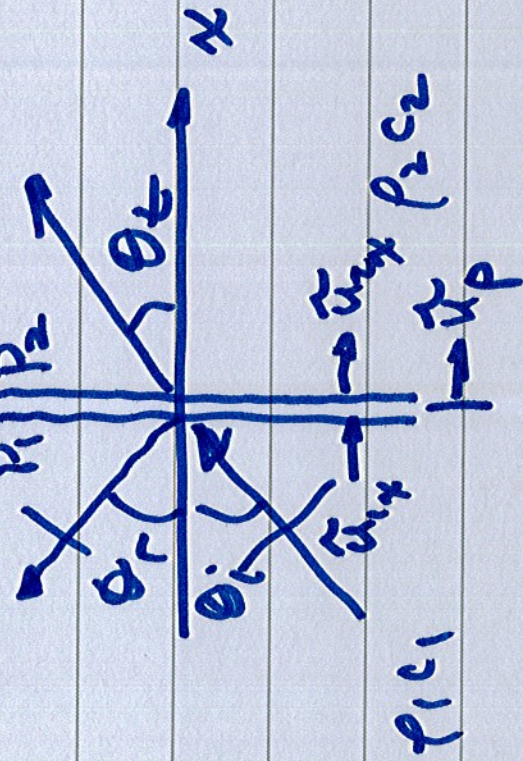
① no flexural stiffness

- no wave propagation within the panel in the x-direction - panel does not compress in the x-direction

- no free wave propagation possible in region ② in the y-direction

local reaction
 - only consider solid body transverse motion

① ②



same medium on both sides

$$p_1 = p_2 \quad c_1 = c_2$$

m_s - mass/unit area

u_p - transverse velocity of the panel

- panel in limf - no free wave prop in the y-direction

① region

$$\tilde{A}_1 = P_i e^{-i(k_x x + k_y y)} + P_r e^{-i(k_x x - k_y y)}$$

$$\theta_i = \theta_r = \theta_t$$

$$k_x = k \cos \theta_i$$

$$k_y = k \sin \theta_i$$

$$k = \frac{\omega}{v}$$

$$\tilde{u}_1 = \frac{P_i}{\rho c} \cos \theta_i e^{-i(k_x x + k_y y)}$$

$$- \frac{P_r \cos \theta_i}{\rho c} e^{-i(k_x x - k_y y)}$$

$$P_i = P_r = P_c$$

in region ②

$$\tilde{P}_2 = P_t e^{-i(k_x x + k_y y)}$$

$$\tilde{u}_2 = \frac{P_t}{\rho c} \cos \theta e^{-i(k_x x + k_y y)}$$