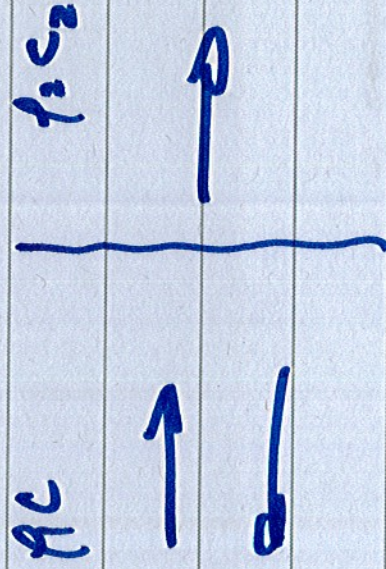


Reflection and Transmission ✓

Midterm Nov 1 Friday

The Atlantic



$f_{c_2} > f_{c_1}$ R +ve

$f_{c_2} < f_{c_1}$ R -ve

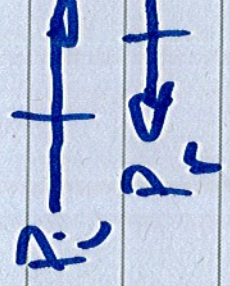
$f_{c_2} \gg f_{c_1}$ $R \rightarrow 1$ $T \rightarrow 2$

$f_{c_2} \ll f_{c_1}$ $R \rightarrow -1$ $T \rightarrow 0$

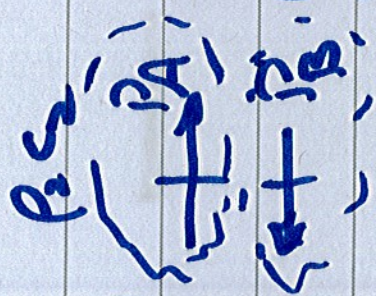
4.2.2

①

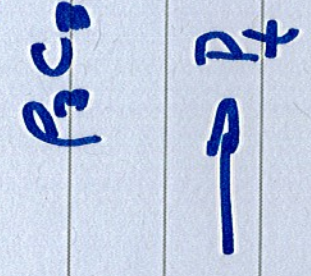
P_C



②



③



$x=L$

$$\frac{d^2 \tilde{P}_1}{dx^2} + k_1^2 \tilde{P}_1 = 0$$

$$k_1 = \frac{\omega}{c_1}$$

$$\tilde{P}_1(x) = P_1 e^{-ik_1 x} + P_2 e^{+ik_1 x}$$

$$\tilde{P}_2(x) = P_A e^{-ik_2 x} + P_B e^{+ik_2 x}$$

$$\tilde{P}_3(x) = P_T e^{-ik_3 x}$$

$$\frac{d^2 \tilde{P}_2}{dx^2} + k_3^2 \tilde{P}_3 = 0$$

$$k_3 = \frac{\omega}{c_3}$$

B.C.'s

$$\text{at } x=0 \quad \tilde{P}_1 = \tilde{P}_2 \quad (1)$$

$$\tilde{U}_1 = \tilde{U}_2 \quad (2)$$

$$\text{at } x=L \quad \tilde{P}_2 = \tilde{P}_3 \quad (3)$$

$$\tilde{U}_2 = \tilde{U}_3$$

$$(1) \quad P_c + P_r = P_A + P_B \quad \div P_i$$

$$\boxed{I + R = A + B}$$

$$R = \frac{P_c}{P_i} \quad A = \frac{P_A}{P_i} \quad B = \frac{P_B}{P_i}$$

$$(2) \quad I - R = \frac{1}{s_{21}} (A - B)$$

$$s_{21} = \frac{P_{32}}{P_{11}} \quad T = \frac{P_4}{P_1}$$

$$(3) \quad A e^{-ik_2 L} + B e^{+ik_2 L} = T e^{-ik_3 L}$$

$$(4) \quad A e^{-ik_2 L} - B e^{+ik_2 L} = \frac{T}{s_{32}} e^{-ik_3 L}$$

$$s_{32} = \frac{P_{33}}{P_{22}}$$

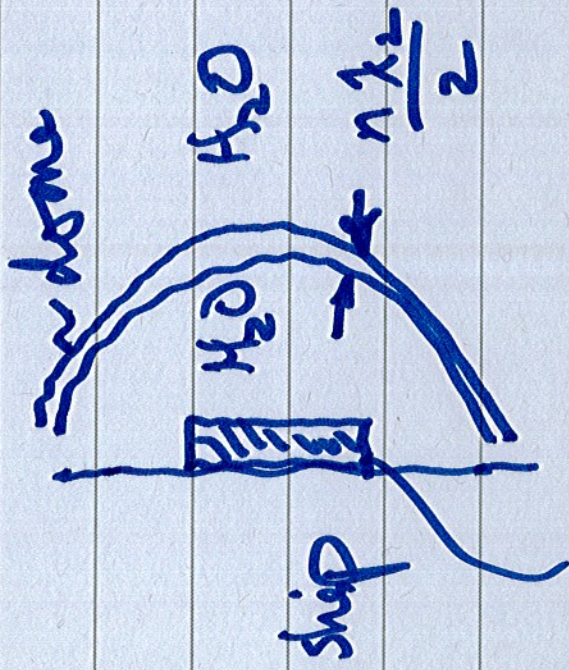
$$R = \frac{\left(1 - \frac{\rho_{12}}{\rho_{23}}\right) \cos k_2 L + j \left(\frac{\rho_{12}}{\rho_{23}} - \frac{\rho_{13}}{\rho_{23}}\right) \sin k_2 L}{\left(1 + \frac{\rho_{12}}{\rho_{23}}\right) \cos k_2 L + j \left(\frac{\rho_{12}}{\rho_{23}} + \frac{\rho_{13}}{\rho_{23}}\right) \sin k_2 L}$$

$$k_2 L = \frac{2\pi}{\lambda_2} L = 2\pi \left(\frac{L}{\lambda_2}\right)$$

non-dimensional layer depth

$R \rightarrow 0$ when $\rho_{12} = \rho_{23}$

when $\sin k_2 L = 0$



Sonar Dome Case

sonar
transducer

$R \rightarrow 0$ $|T| \rightarrow 1$ perfect transmission

$r_{11} = \beta_3 c_3$ choice

$$\sin kt_2 \rightarrow 0 \quad kt_2 = n\pi$$

$$L = n \left(\frac{\lambda_2}{2} \right)$$

Thin, heavy barrier case

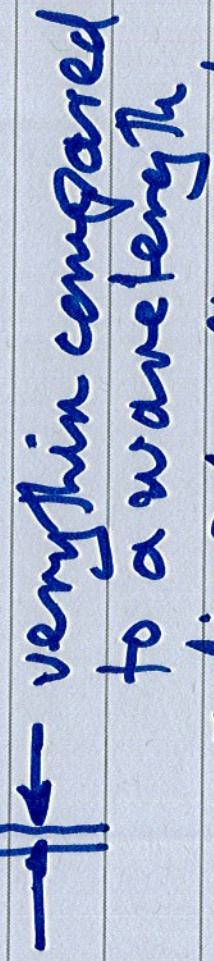
③

②

①

ρc_1

$\rho c_3 = \rho c_1$



very thin compared to a wavelength
 - limp (no flexural stiffness)
 - heavy

$k_2 L \ll 1$

$\sin k_2 L \approx k_2 L$

$\cos k_2 L \approx 1$

$\rho c_3 \gg \rho c_1$ heavy

$$R = \frac{\left(1 - \frac{\rho_{c1}}{\rho_{c3}}\right) 1 + j \left(\frac{\rho_{c2}}{\rho_{c3}} - \frac{\rho_{c1}}{\rho_{c3}}\right) k_2 L}{\left(1 + \frac{\rho_{c2}}{\rho_{c3}}\right) 1 + j \left(\frac{\rho_{c2}}{\rho_{c3}} + \frac{\rho_{c1}}{\rho_{c3}}\right) k_2 L}$$

$$R = \frac{j \frac{\rho_{c2} \omega}{\rho_{c3}} \frac{\omega}{\rho_2} L}{2 + j \frac{\rho_{c2} \omega}{\rho_{c3}} \frac{\omega}{\rho_2} L} \quad (\rho_2 L) = m_s \quad \text{mass/unit area}$$

$$\rho_{c1} = \rho_{c3} = \rho_c \quad \left\{ R = \frac{j \omega m_s}{2 \rho_c + j \omega m_s} \right.$$

Physical parameter
= mass/unit area

$$\omega \rightarrow \infty \quad R \rightarrow 1 \quad \omega \rightarrow 0 \quad R \rightarrow 0$$

$$M_s \rightarrow \infty \quad R \rightarrow 1 \quad (T \rightarrow 1) \quad \begin{array}{c} \rightarrow \\ \parallel \\ \rightarrow \end{array} \begin{array}{c} R \\ \rightarrow \\ T \end{array}$$

$$T = \frac{2e^{ik_2L}}{\left(1 + \frac{\rho_{c1}}{\rho_{c3}}\right) \cos k_2L + j\left(\frac{\rho_{c2}}{\rho_{c3}} + \frac{\rho_{c1}}{\rho_{c2}}\right) \sin k_2L}$$

(i) Sonar $k_2L = n\pi$

$$\sin k_2L \rightarrow 0$$

$$\cos k_2L \rightarrow 1$$

$$\rho_{c1} = \rho_{c3}$$

perfect

$$T \rightarrow \frac{2e^{+ik_2L}}{\pm 2} \quad |T| \rightarrow 1$$

transmission
accepted for
phase shift

(ii) Thin ~~to~~ heavy barrier

$$f_{c1} = \beta_3 c_3 \quad \frac{\beta_3 c_2}{\beta_1 c_1} \gg 1 \quad k_2 L \ll 1$$

$$T \rightarrow \frac{2 e^{+ik_3 L}}{2 + j \left(\frac{\beta_3 c_2}{\beta_3 c_3} \right) k_2 L} \quad k_1 = k_3 = k \quad f_{c1} = \beta_3 c_3 = f_0 c \quad f_{c2} = m_s$$

$$T = \frac{2 \beta_0 c e^{+ikL}}{2 \beta_0 c + j \omega m_s}$$

Thin, heavy barrier - below the critical frequency

$\omega \rightarrow 0 \quad 1/T \rightarrow 1$
high freq $\omega m_s \gg 2 \beta_0 c$

In the high frequency region

$$|T| = \frac{zbc}{\omega ms}$$

mass law

$$|T| \propto \frac{1}{ms}$$

$$|T| \propto \frac{1}{f}$$

"limp" \rightarrow flexural stiffness is negligible

Sheet of AL 0.05" limp below 10 kHz

Transmission Loss

$$TL = 10 \log_{10} \frac{1}{|T|^2} \quad \text{dB}$$

$$|T| \downarrow \quad \uparrow \quad TL \uparrow$$