

$$f_e = F_e e^{j\omega t}$$

steady-state response
 - system responds at the
 driving frequency

$$\tilde{x} = \frac{F_e e^{j\omega t}}{j\omega (R_m + j(\omega m - \frac{s}{\omega}))}$$

zero at the natural freq
 - large response
 - resonance

1.3.3 Mechanical Impedance

$$\begin{aligned} \text{Defin } \hat{Z}_m &= \frac{\text{complex driving force}}{\text{steady state complex velocity at the driven point}} \\ &= \frac{F}{\dot{x}} \end{aligned}$$

Damped SDOF

$$\begin{aligned} \hat{Z}_m &= \frac{F e^{j\omega t}}{R_m + j(\omega m - \frac{s}{\omega})} \\ &= R_m + j(\omega m - \frac{s}{\omega}) \end{aligned}$$

$$\hat{z}_m = R + jX$$

mechanical
resistance

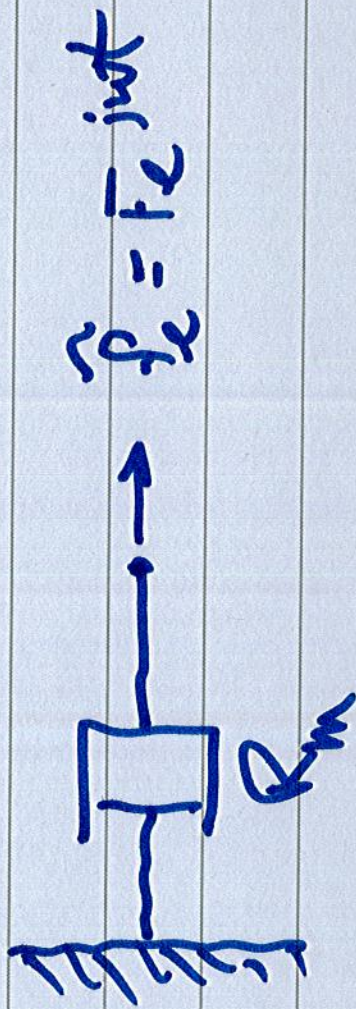
mechanical
reactance

$$R = \operatorname{Re}\{\hat{z}_m\}$$

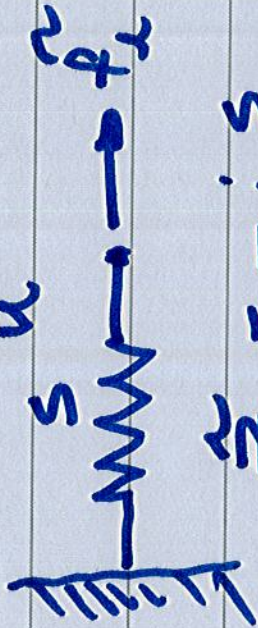
$$X = \operatorname{Im}\{\hat{z}_m\}$$

$$R = R_m$$

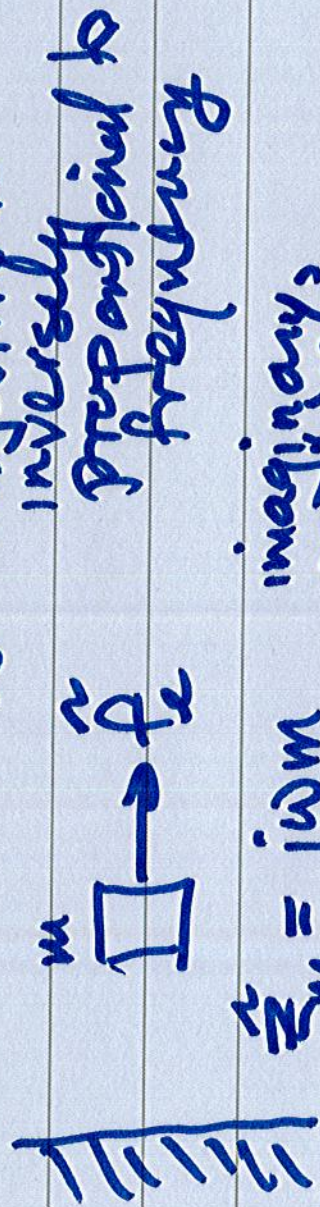
$$X = \left(\omega m - \frac{s}{\omega}\right)$$



$$\hat{z}_m = \frac{\hat{f}_e}{\hat{u}} = R_m \quad \text{real and positive}$$



$$\hat{z}_m = -j \frac{S}{\omega} \quad \text{imaginary, negative \& inversely proportional to frequency}$$



$$\hat{z}_m = j\omega m \quad \text{imaginary, positive, proportional to freq}$$

1.3.4 Mechanical Resonance Response

Defn: Occurs when the imaginary of the input mechanical impedance force to zero

$$\text{Im} \{ \hat{Z}_m \} = 0$$

$$\hat{Z}_m = R_m + j(\omega m - \frac{s}{\omega})$$

$$\text{Im} \{ \hat{Z}_m \} = \omega m - \frac{s}{\omega}$$

$$\omega m - \frac{s}{\omega} = 0$$

$$\omega^2 = \frac{s}{m}$$

ω_0 - undamped
natural freq
of the system

Resonance occurs when the system is driven at the undamped natural frequency

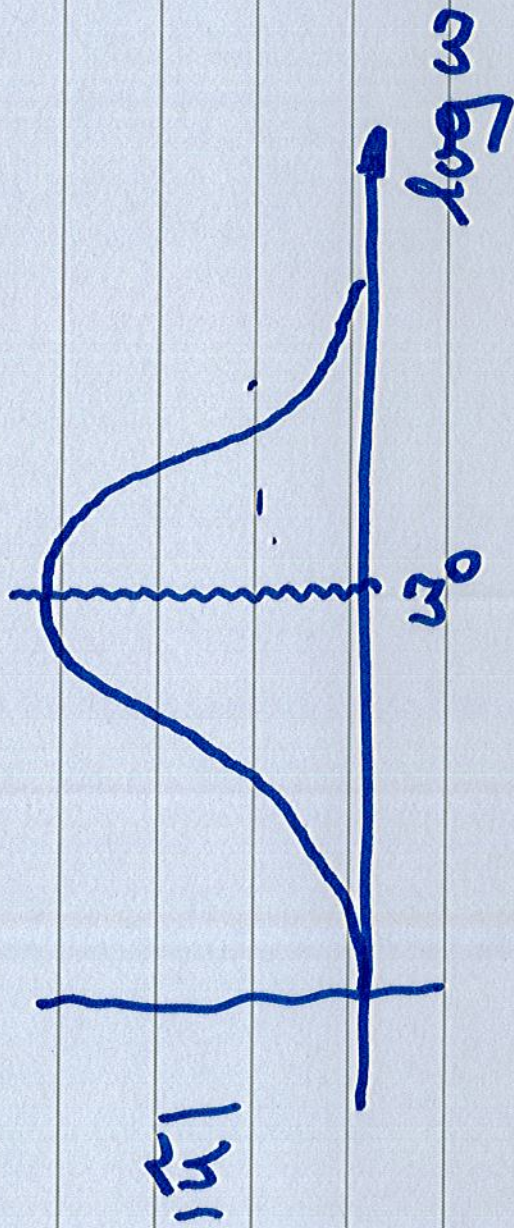
$$\tilde{u} = \frac{F_0 \text{ just}}{R_m + j(\omega m - \frac{s}{\omega})} \quad \left. \vphantom{\frac{F_0 \text{ just}}{R_m + j(\omega m - \frac{s}{\omega})}} \right\} = 0 \text{ when}$$

$$\omega = \omega_0$$

drive at the natural freq

velocity \rightarrow maximum

$$\phi \approx \tilde{z}_m \text{ is purely real} = R_m$$



≡ frequency ranges of interest

(i) $\omega < \omega_0$

(ii) $\omega \approx \omega_0$

(iii) $\omega > \omega_0$

$$\tilde{Z}_m = R_m + i(\omega m - \frac{s}{\omega})$$

(i) $\omega < \omega_0$

stiffness controlled region

$$\tilde{Z}_m \approx -i \frac{s}{\omega}$$

$$\tilde{x} \approx \left(\frac{F}{s}\right) e^{i\omega t}$$

$|\tilde{x}|$ is independent of frequency

(ii) near resonance

$$\omega \approx \omega_0$$

$$\tilde{Z}_m \approx R_m$$

$$\tilde{x} \approx \frac{F e^{i\omega t}}{j\omega R_m}$$

$$\vec{u} = j\omega \vec{x} \approx \frac{F e^{j\omega t}}{R_m}$$

$$\vec{z}_m = R_m + j(\omega m - \frac{F}{\omega})$$

$|\vec{u}| \approx \frac{F}{R_m}$ independent of frequency

~~stiff~~ "damping controlled region"

(iii) $\omega > \omega_0$ "mass controlled region"

$$\vec{z}_m \approx j\omega m$$

$$\vec{a} = j\omega \vec{u} \approx \left(\frac{F}{m}\right) e^{j\omega t}$$

acceleration is independent of frequency



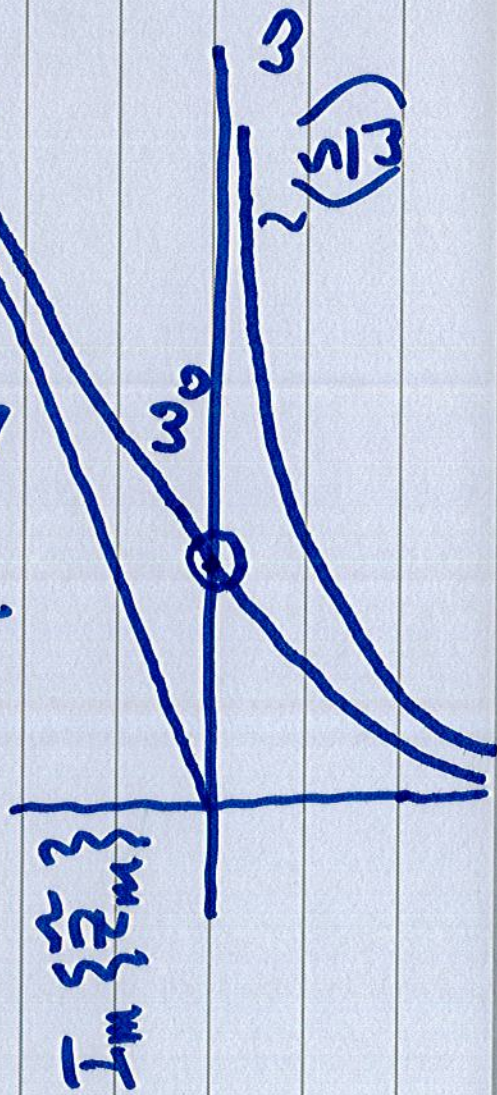
transducers are designed to operate in one of these regions

$$\tilde{Z}_m \approx j\omega m$$

- imag
- positive
- proportional to frequency

$$\tilde{Z}_m \approx -j \frac{s}{\omega}$$

- imag
- negative
- inversely prop. to freq.



$$Z_m = \frac{F}{U} \quad U = \frac{F}{Z_m}$$

can predict the response to any force if the impedance is known (from measurement or analysis) and if the system is linear

1.4 Superposition

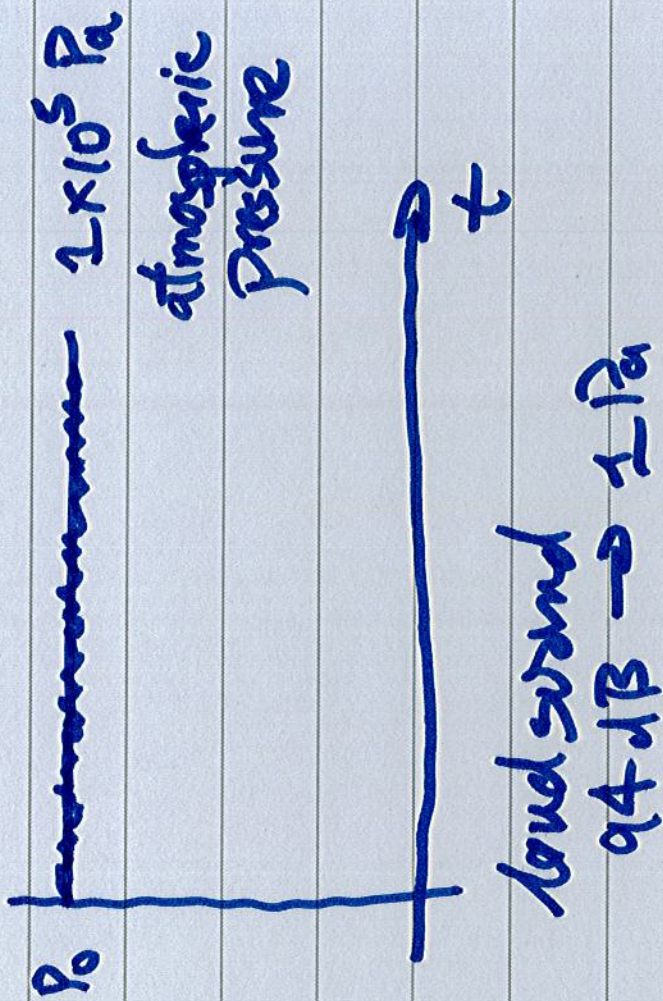
"linear" acoustics

"linear" vibration

- small amplitude
fluctuations in
sound pressure or
velocity

* linear systems,
small amplitudes

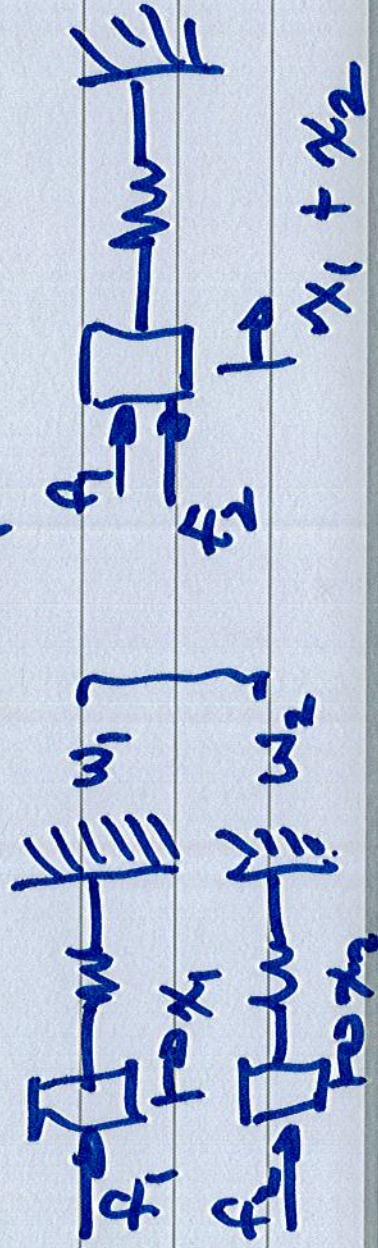
- output of a linear system
is linearly proportional to
the input



- double the force - response doubles
- linear system responds at the forcing frequency

$$F e^{j\omega t} \rightarrow \hat{A} e^{j\omega t} = \hat{x}$$

- response to two or inputs is the linear sum of the individual responses



- convenient to break up input forces into individual frequency components (frequency analysis)

- find the response to each frequency component

- sum up individual responses to give the total response