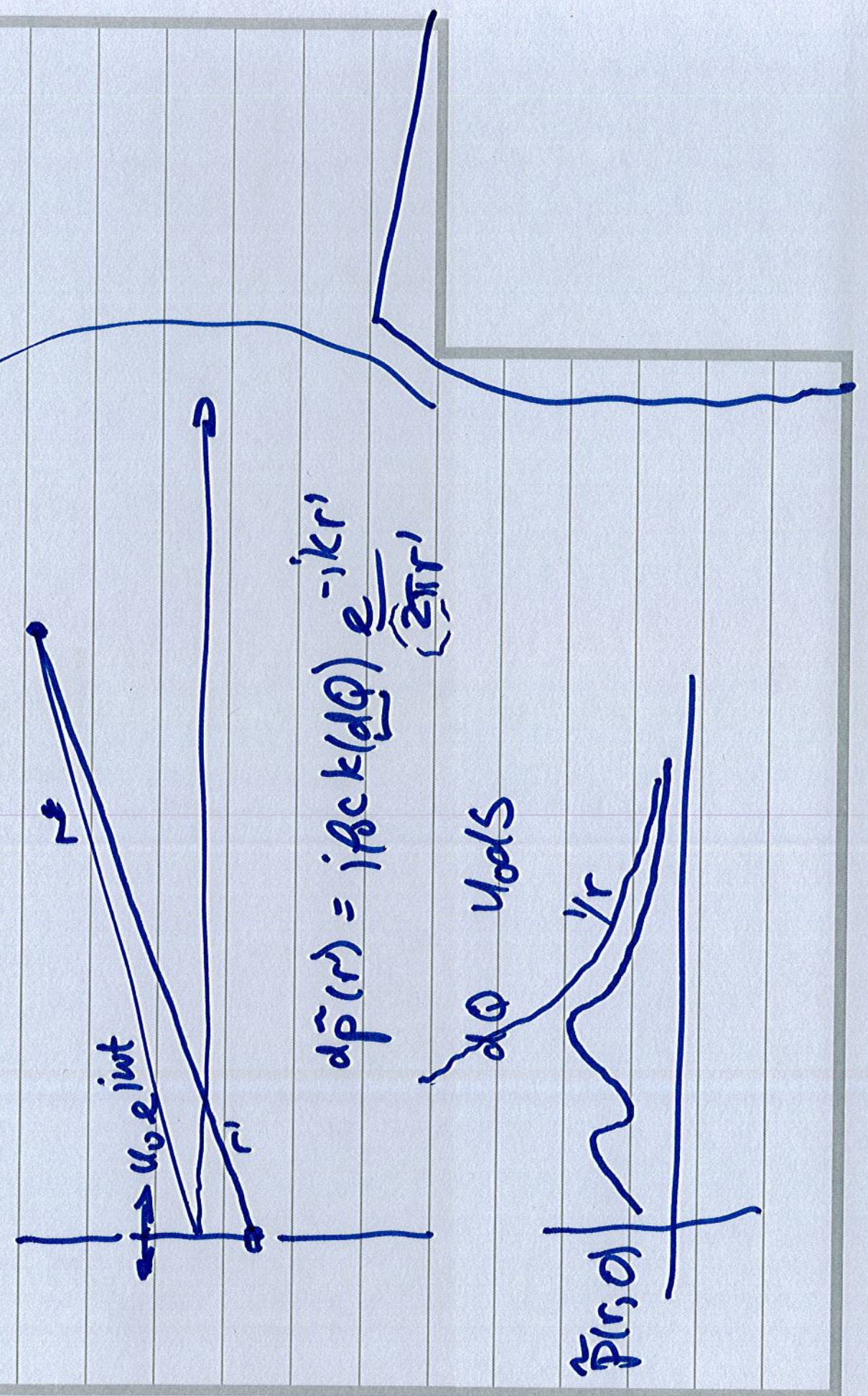


Piston in a beaffle



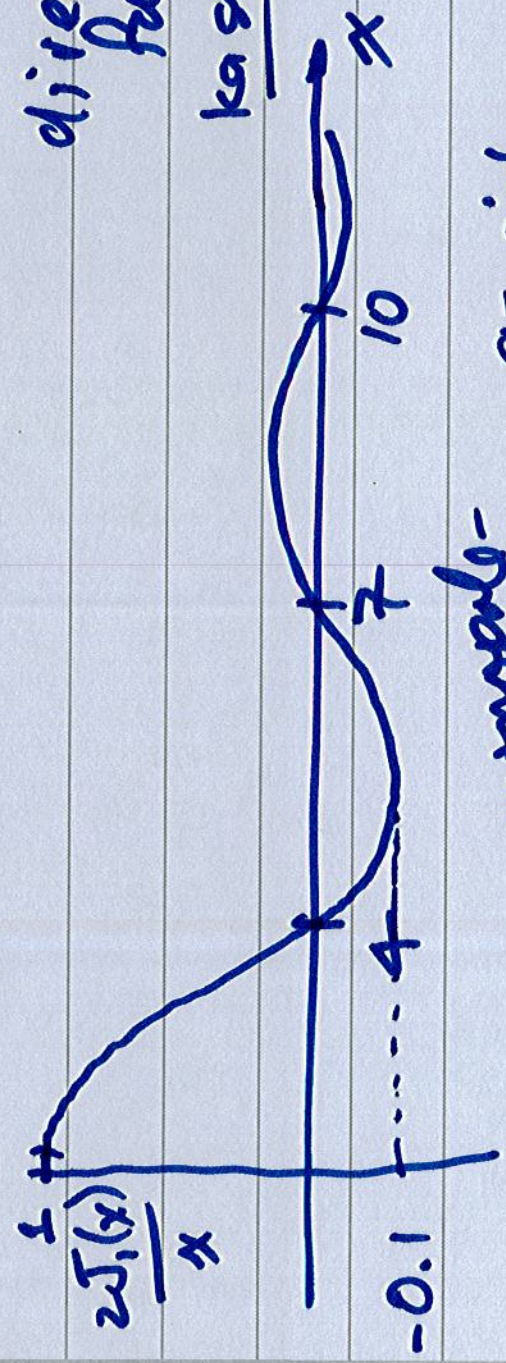
Farfield



$$\hat{P}(r, \theta) = j \frac{\mu_0 c}{2} U_0 \left(\frac{a}{r}\right) e^{-jkr} \left[2 \frac{J_1(ka \sin \theta)}{ka \sin \theta} \right]$$

directivity factor

$$ka \sin \theta = x$$



if $ka \ll 1$ \sim monopole-like case.

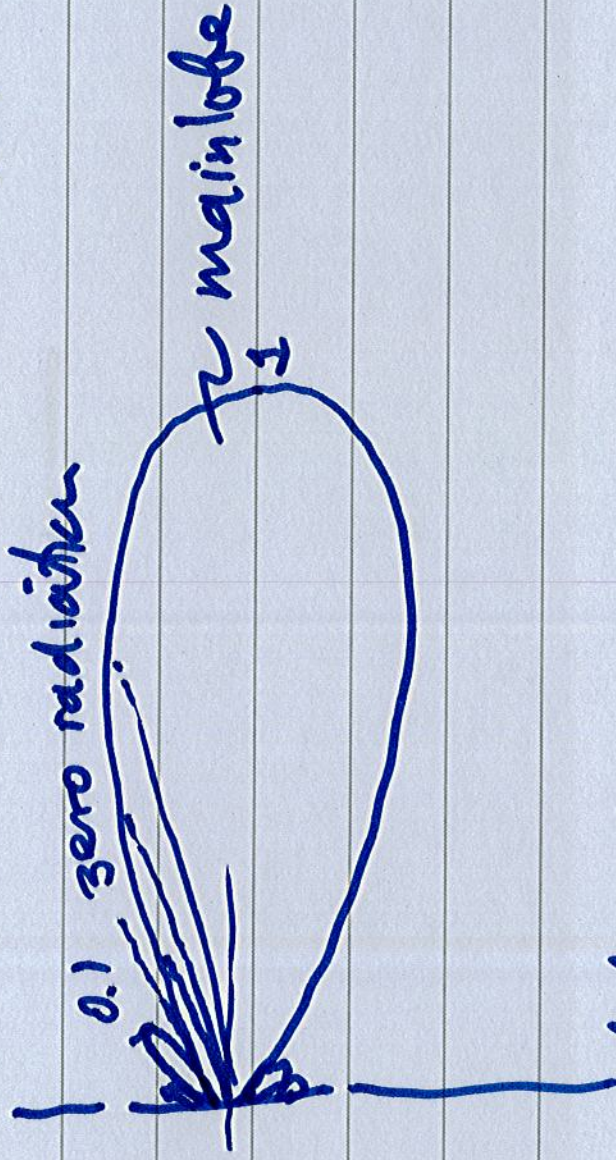
$a =$ piston radius

directivity factor ≈ 1 for all angles

$k = \frac{\omega}{c}$
 $\theta =$ polar angle

3

$ka > 1$ we have possibility of
sidelobes & nulls

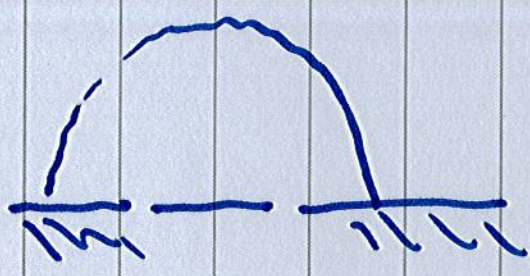


main lobe becomes narrower
as the frequency increases

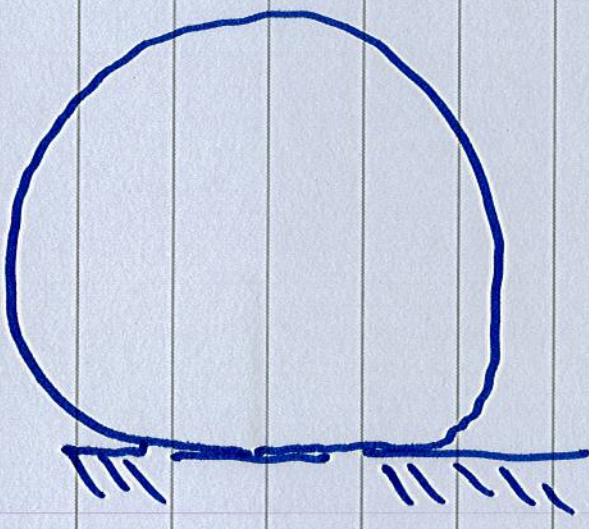
$$ka \sin \theta = \frac{\pi}{2}$$

$ka \gg$ highly directional radiation

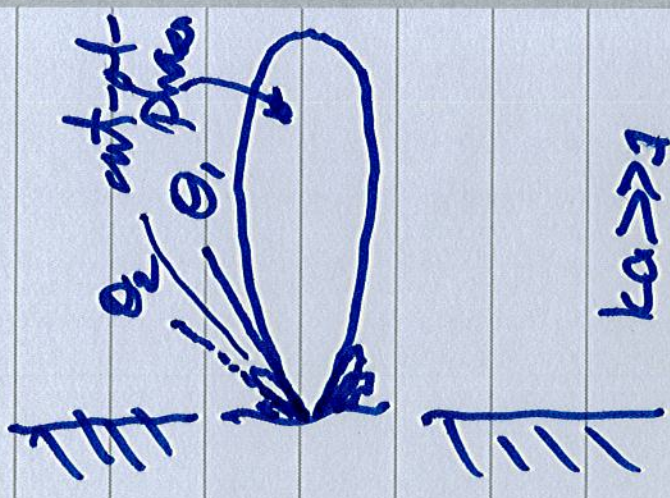
$ka \ll 1$ omnidirectional radiation



$ka \ll 1$



$ka \approx 4$



$ka \gg 1$

zeros of the Bessel function \rightarrow AS

$\theta_1 =$ angle of first

First minimum happens null

when $ka \sin \theta_1 = j_{11} \approx$ first zero of the Bessel function $J_1(j_{11}) = 0$

$J_1(j_{12}) = 0$ $ka \sin \theta_2 = j_{12}$ $J_1(j_{11}) = 0$

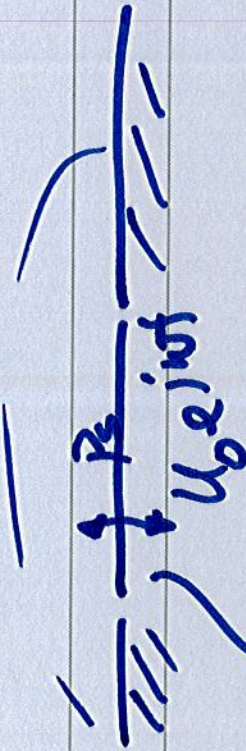
5
at high freqs $ka \gg 1$ j_1 is
reached at progressively smaller
angles

"beam" width becomes narrower

Public Address systems

- many h.f. drivers - pointing
in various directions to
ensure uniform coverage
- small number of large
low frequency drivers

s.4.1.2 Radiation Impedance



force exerted on the radiator by the sound field
source velocity

$$Z_r =$$

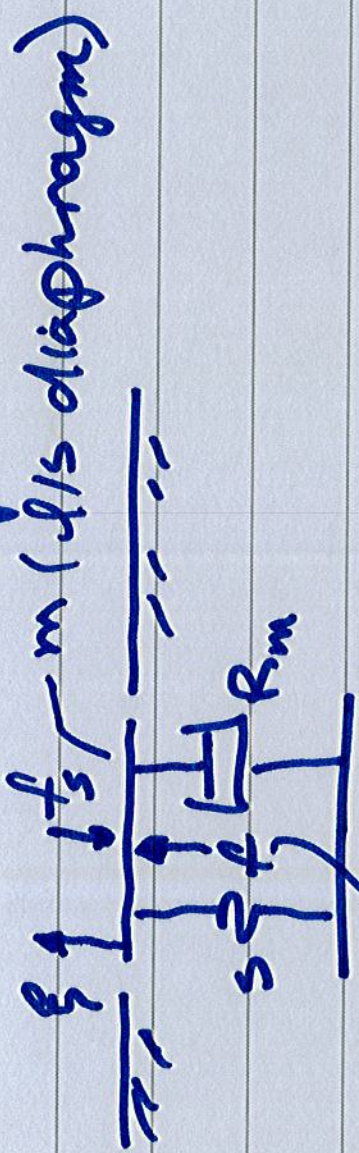
rigid piston

total force acting on piston

$$Z_r = \frac{\int_s P_{\text{surface}} ds}{u_0}$$

u_0 rigid piston velocity

loudspeaker - finite internal mechanical impedance



force generated by the voice coil.

Equation of Motion

$$f - f_s = m \frac{d^2 \xi}{dt^2} + R_m \frac{d\xi}{dt} + s \xi$$

Assume harmonic motion $e^{j\omega t}$

$$u = j\omega \xi \quad \text{diaphragm velocity}$$

$$f - f_s = j\omega m u + R_m u + \frac{s}{j\omega} u \sim Z_m$$

$$= \left[R_m + j \left(\omega m - \frac{s}{\omega} \right) \right] u$$

in vacuo mechanical
impedance of the L/S

$$f = f_s + z_m u$$

$$= (z_r + z_m) u \quad z_r = \frac{f_s}{u}$$

↑ radiation impedance
in vacuo mechanical impedance

$$u = \frac{f}{z_r + z_m}$$

l/s response is determined by both mechanical & radiation impedance

$$Z_r = R_r + jX_r$$

resistance reactance

Power delivered by the piston to
the sound field

$$\Pi = \frac{1}{T} \int_0^T \operatorname{Re}\{f_s\} \operatorname{Re}\{u\} dt$$

harmonic case

$$\Pi = \frac{1}{2} \operatorname{Re}\{f_s u^*\}$$

$$Z_r = \frac{f_s}{u}$$

$$f_s = Z_r u$$

$$\overline{\Pi} = \frac{1}{2} R_e \{ z_r u u^* \}$$

$$= \frac{|u|^2}{2} R_e \{ z_r \}$$

R_r radiation resistance

$$= \left\{ \frac{|u|^2}{2} \right\} R_r$$

mean square velocity
of the piston

Circular Piston

$$R_r = \pi a^2 \rho c R_1(zka)$$

$$X_r = \pi a^2 \rho c X_1(zka)$$

Circular rigid
piston in
an infinite
rigid baffle.

$$R_1(x) = 1 - 2 \frac{J_1(x)}{x}$$

$$X_1(x) = \frac{4}{\pi} \left[\frac{x}{3} - \frac{x^3}{3 \cdot 5} + x^5 \dots \right]$$

13

