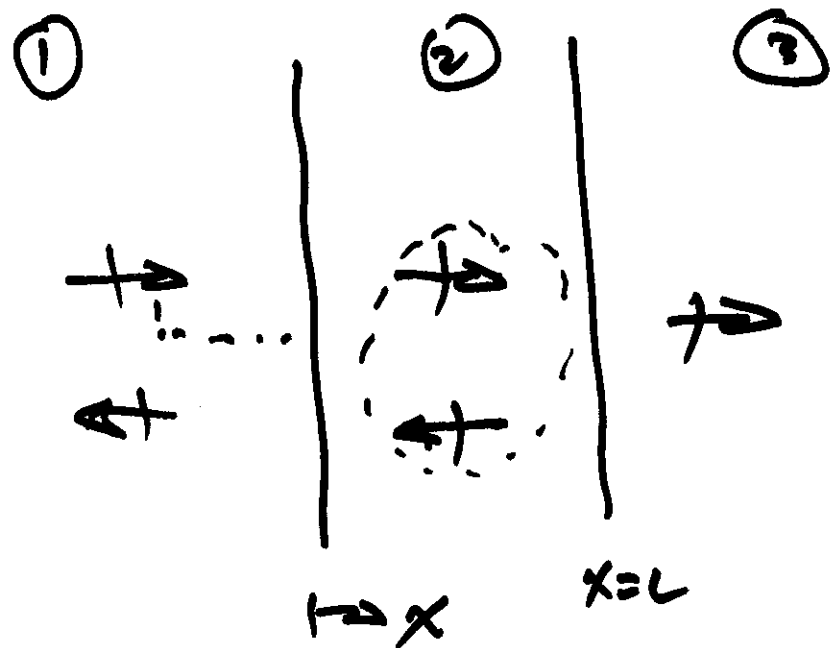


$$R = \frac{\zeta_{21} - 1}{\zeta_{21} + 1}$$

$$T = \frac{2 \zeta_{21}}{\zeta_{21} + 1}$$

$$\zeta_{21} = \left(\frac{p_2 c_2}{p_1 c_1} \right)$$



Boundary Conditions

at $x=0$

$$\hat{p}_1(0) = \hat{p}_2(0) \quad (1)$$

$$u_{1n}(0) = u_{2n}(0) \quad (2)$$

at $x=L$

$$\hat{p}_2(L) = \hat{p}_3(L) \quad (3)$$

$$u_{2n}(L) = u_{3n}(L) \quad (4)$$

$$(1) \quad P_i + P_r = P_A + P_B \quad \div P_i$$

$$\boxed{1 + R = A + B} \quad \checkmark$$

$$R = \frac{P_r}{P_i}$$

$$A = \frac{P_A}{P_i}$$

$$B = \frac{P_B}{P_i}$$

$$(2) \quad 1 - R = \frac{1}{S_{21}} (A - B) \quad \checkmark$$

$$T = \frac{P_t}{P_i}$$

$$(3) \quad A e^{-jk_2 L} + B e^{+jk_2 L} = T e^{-jk_3 L} \quad \checkmark$$

$$(4) \quad A e^{-jk_2 L} - B e^{+jk_2 L} = \frac{T}{S_{32}} e^{-jk_3 L} \quad \checkmark$$

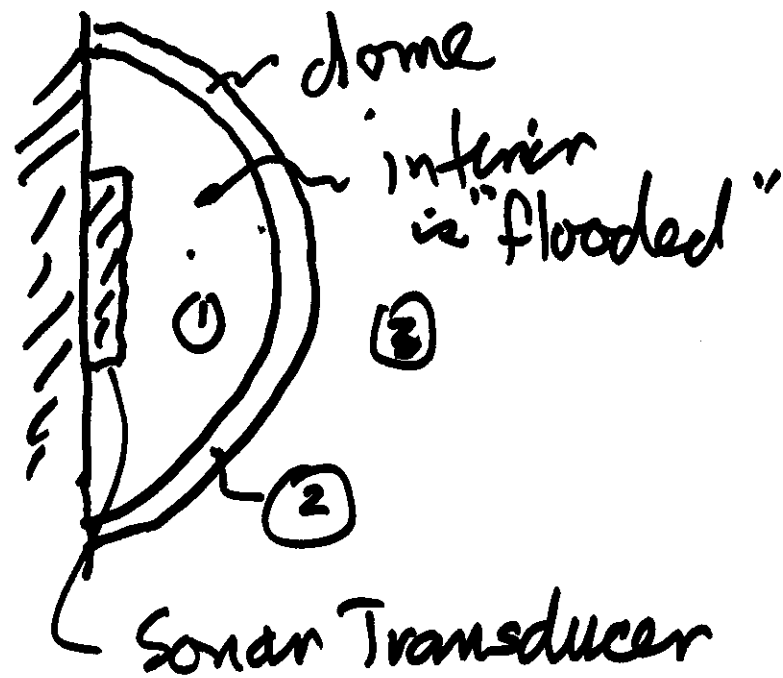
$$S_{21} = \frac{\rho_2 c_2}{\rho_1 c_1}$$

$$S_{32} = \frac{\rho_3 c_3}{\rho_2 c_2}$$

$$S_{32}$$

$$R = \frac{\left(1 - \frac{\rho_1 c_1}{\rho_3 c_3}\right) \cos \underline{k_2 L} + j \left(\frac{\rho_2 c_2}{\rho_3 c_3} - \frac{\rho_1 c_1}{\rho_2 c_2}\right) \sin \underline{k_2 L}}{\left(1 + \frac{\rho_1 c_1}{\rho_3 c_3}\right) \cos k_2 L + j \left(\frac{\rho_2 c_2}{\rho_3 c_3} + \frac{\rho_1 c_1}{\rho_2 c_2}\right) \sin k_2 L}$$

$$k_2 L = \frac{2\pi L}{\lambda_2} = 2\pi \left(\frac{L}{\lambda_2}\right) \quad \text{non-dimensional layer depth}$$



Sonar Dome problem

$$R = 0 \quad (T = 1)$$

objective \rightarrow perfect transmission

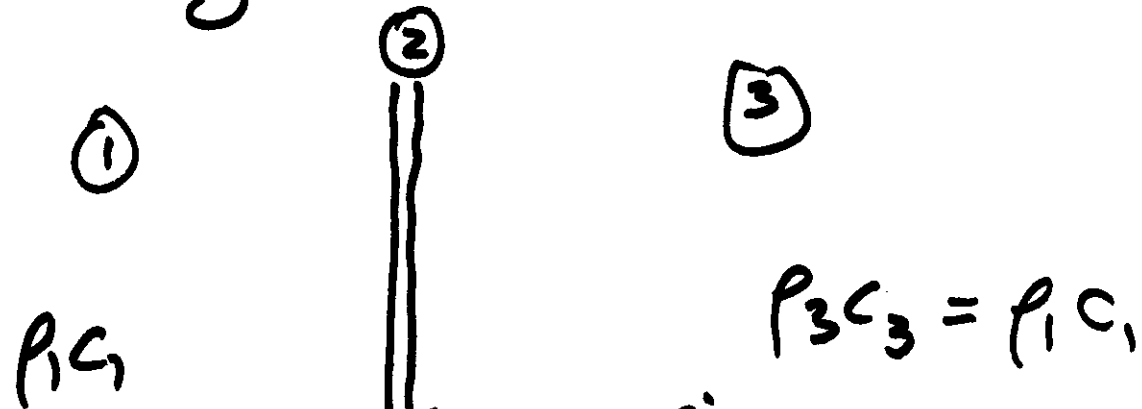
dome thickness must be an integral number of half wavelengths

choose $k_2 L = n\pi \quad \Rightarrow \quad L = n \left(\frac{\lambda_2}{2} \right)$

$$\left. \begin{array}{l} \sin k_2 L \rightarrow 0 \\ \cos k_2 L \rightarrow 1 \end{array} \right\} + \quad \rho_1 c_1 = \rho_3 c_3$$

$$R = 0 \quad |T| = 1$$

Thin, heavy barrier case



very thin compared to a wavelength,
limp, heavy

$$k_2 L \ll 1$$

$$\rho_2 c_2 \gg \rho_1 c_1$$

$$\sin k_2 L \rightarrow k_2 L \quad \cos k_2 L \rightarrow 1$$

$$\text{when } k_2 L \ll 1$$

$$R \rightarrow \frac{\left(1 - \frac{\rho_1 c_1}{\rho_3 c_3}\right) 1 + i \left(\frac{\rho_2 c_2}{\rho_3 c_3} - \frac{\rho_1 c_1}{\rho_2 c_2}\right) k_2 L}{\left(1 + \frac{\rho_1 c_1}{\rho_3 c_3}\right) 1 + i \left(\frac{\rho_2 c_2}{\rho_3 c_3} + \frac{\rho_1 c_1}{\rho_2 c_2}\right) k_2 L}$$

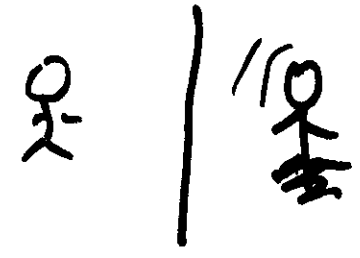
$$R \approx \frac{i \frac{\rho_2 c_2}{\rho_3 c_3} \frac{\omega}{v_2} L}{2 + i \frac{\rho_2 c_2}{\rho_3 c_3} \frac{\omega}{v_2} L}$$

$\rho_2 L = \text{mass/unit area of the "barrier"}$
 $= m_s$

$$\rho_1 c_1 = \rho_3 c_3 = \rho_0 c \quad]$$

characteristic impedance of the ambient fluid

$$R = \frac{j\omega m_s}{2\rho_0 c + j\omega m_s}$$

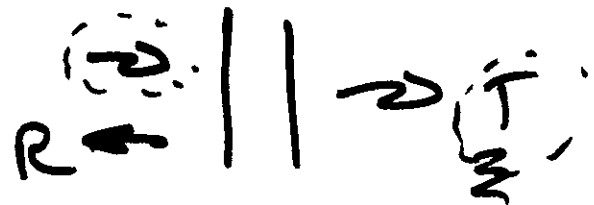


for a thin, heavy barrier

$$\omega \rightarrow 0 \quad R \rightarrow 0 \quad (T \rightarrow 1)$$

$$\omega \rightarrow \infty \quad R \rightarrow 1$$

Normal Incidence Transmission Coefficient



$$T = \frac{2 e^{jk_3 L}}{\left(1 + \frac{\rho_1 c_1}{\rho_3 c_3}\right) \cos k_2 L + j \left(\frac{\rho_2 c_2}{\rho_3 c_3} + \frac{\rho_1 c_1}{\rho_2 c_2}\right) \sin k_2 L}$$

(i) Sonar Case:

$$k_2 L = n\pi$$

$$\sin k_2 L \Rightarrow 0$$

$$\cos k_2 L \Rightarrow 1$$

$$\rho_1 c_1 = \rho_3 c_3$$

$$T = \frac{2e^{ik_3L}}{\pm 2}$$

$$|T| = 1$$

perfect transmission except for
a phase change

(ii)

Thin, heavy barrier

$$\rho_1 c_1 = \rho_3 c_3 \quad \frac{\rho_2 c_2}{\rho_1 c_1} \gg 1$$

$$k_2 L \ll 1$$

$$T = \frac{2 e^{jk_3 L}}{2 + j \left(\frac{\rho_2 c_2}{\rho_3 c_3} \right) k_2 L}$$

$$k_1 = k_3 = k$$

$$\rho_1 c_1 = \rho_3 c_3 = \rho_0 c$$

$$\rho_2 L = m_s$$

$$T = \frac{2 \rho_0 c e^{jkL}}{2 \rho_0 c + j \omega m_s}$$

$$k = \frac{\omega}{c} \text{ air}$$

Thin, limp barrier

$$\omega \rightarrow 0 \quad |T| \rightarrow 1$$

"high frequency" $\omega m_s \gg \rho_0 c$

$$\boxed{|T| \Rightarrow \frac{2\rho c}{\omega m_s} \quad \text{mass law}} \quad]$$

$|T| \propto \frac{1}{\omega}$ barrier performance increases directly with mass & frequency
 $|T| \propto \frac{1}{m_s}$

limp \rightarrow flexural stiffness
 is assumed to be negligible
 sheet of AL 0.005"