

1. The diameters of some shafts and holes to be assembled were measured and the results are given in the table below.

	1	2	3	4	5	6	7	8	9	10	average	std
Shaft	9.86	9.94	9.91	9.92	9.79	9.89	9.91	9.86	10.01	9.93	9.902	0.058
Hole	10.01	10.11	10.04	10.12	10.05	10.06	10.11	10.07	10.06	10.08	10.071	0.035

Unit: mm

- (a) Express the dimensional tolerance of the shafts and holes using the bilateral and unilateral notations. For the unilateral notation, use 0 as the lower tolerance limit for the holes and 0 as the upper tolerance limit for the shafts. (Hint: they must represent the same ranges)

Bilateral

shafts: 9.902 ± 0.174 ,
holes: 10.071 ± 0.105 ,

Unilateral

shafts: $10.076^0_{-0.348}$,
holes: $9.966^{+0.315}_0$,

- (b) For the manufacturing process making the shafts, assuming USL = 10.00 and LSL = 9.80, determine the process capability C_p and C_{pk} .

$$C_{pk} = \frac{10.2 - 9.7}{6 \times 0.058} = 1.44$$

$$C_{pk} = \frac{\min(|10.2 - 9.902|, |9.7 - 9.902|)}{3 \times 0.058} = \frac{\min(0.298, 0.202)}{3 \times 0.058} = 1.16$$

- (c) This problem is related to surface roughness. The surface roughness was measured on a milled piece in the feed direction with the following values. Calculate the arithmetic surface roughness R_a and R_q values. (unit in micron)

1	2	3	4	5	6	7	8	9	10	11	12	average	STD
-0.23	0.42	1.22	-0.5	-0.95	-0.11	1.11	-0.55	-0.95	-0.11	1.42	0.22	0.08	0.82

$$\begin{aligned} R_a &= \frac{\sum |y_i - \bar{y}|}{N} = \frac{0.31 + 0.34 + 1.14 + 0.58 + 1.03 + 0.19 + 1.03 + 0.63 + 1.03 + 0.19 + 1.34 + 0.14}{12} \\ &= \frac{7.955}{12} = 0.663 \end{aligned}$$

$$\begin{aligned} R_q &= \sqrt{\frac{\sum (y_i - \bar{y})^2}{N}} = \sqrt{\frac{0.31^2 + 0.34^2 + 1.14^2 + 0.58^2 + 1.03^2 + 0.19^2 + 1.03^2 + 0.63^2 + 1.03^2 + 0.19^2 + 1.34^2 + 0.14^2}{12}} \\ &= \sqrt{\frac{7.315}{12}} = 0.781 \end{aligned}$$

2. The ultimate tensile strength for a metal specimen in the cylindrical shape is 500 MPa (in terms of true stress), and necking occurs at a true strain of $\varepsilon = 0.23$ during the tensile test of the specimen. The material strain hardening index is $n = 0.23$. The cylindrical sample initial diameter is 15 mm and initial length is 40 mm.

- (a) Determine the material strength coefficient $K = ?$

$$K\varepsilon^n = 500 \text{ MPa}$$

$$K(0.23)^{0.23} = 500 \text{ MPa}$$

$$K = 701 \text{ MPa}$$

- (b) During the tensile test of the specimen, what is the force (in the unit of Newton) required to make the specimen reach the necking point?

$$F = \sigma \cdot A = \sigma \cdot A_0 e^{-\varepsilon}$$

$$\sigma = 500 \text{ MPa}$$

$$A_0 = \frac{\pi}{4} d_0^2 = 1765.7 \times 10^{-1} \text{ m}^2$$

$$\varepsilon = 0.23$$

$$\Rightarrow F = 70.2 \text{ kN}$$

- (c) What are the engineering stress and strain of the specimen when it reaches the necking point?

$$\sigma_e = \sigma_t \cdot A_0 e^{-\varepsilon_t} = 397.3 \text{ MPa}$$

$$\varepsilon_e = e^{\varepsilon_t} - 1 = 0.256$$

- (d) What is the energy per unit volume of material that needs to be supplied to make the specimen material reach **the necking point** (Hint: this is not asking for toughness).

$$\int_0^{0.23} K\varepsilon^n d\varepsilon = 9.35 \times 10^7 \text{ J / m}^3$$

3. An orthogonal machining process has the following parameters: the cutting velocity $V = 2.1$ m/s, $t_0 = 0.15$ mm, chip thickness $t_c = 0.19$ mm, width of cut $w_0 = 7$ mm, the thrust force F_t is 20% of the main cutting force F_c (i.e., $F_t = 0.2 F_c$) and the rake angle is 11° . The workpiece material specific cutting energy is 1.5×10^9 J/m³.
- (a) Determine the main cutting force F_c and the thrust force F_t .

$$F_c = U \cdot w \cdot t_0 = 1575 \text{ N}$$

$$F_t = 0.2 F_c = 315 \text{ N}$$

- (b) Please determine the material removal rate (in the unit of m³/s)

$$MRR = V w t_0 = 2.1 \times 10^6 \times 7 \times 0.15 = 2.2 \times 10^6 \text{ mm}^3/\text{s}$$

- (c) Determine the chip velocity (in the unit of m/s)

$$V \cdot t_0 = V_{chip} \cdot t_c \Rightarrow V_{chip} = 1.66 \text{ m/s}$$

- (d) Determine the average shear stress and normal stress in the shear plane.

$$r = \frac{t_0}{t_c} = 0.7895$$

$$\tan \phi = \frac{r \cos \alpha}{1 - r \sin \alpha} \Rightarrow \phi = 42.4$$

$$F_s = F_c \cos \phi - F_t \sin \phi = 950.7 \text{ N}$$

$$F_N = F_c \sin \phi + F_t \cos \phi = 1294.6 \text{ N}$$

$$A = \frac{w_0 t_0}{\sin \phi} = 1.56 \times 10^{-6} \text{ m}^2$$

$$\sigma_s = \frac{F_s}{A} = 611 \text{ MPa}$$

$$\sigma_N = \frac{F_N}{A} = 832 \text{ MPa}$$

4. A tool life experiment of a turning process was carried out with a cutting tool and the following machining conditions. The tool life equation was established.

feed: 0.025 in/rev

depth of cut: 0.015 in

workpiece diameter: 2 in

length of the cut: 10 in

C_o: operating cost per unit time (\$120/hour)

T_c: time to change the tool (120 seconds)

C_i: initial cost of the tool (\$15 for each cutting tool edge)

- (a) Tool life was determined to be 60 min and 10 min for the cutting speed of 350 fpm and 500 fpm, respectively. Determine the Taylor tool life equation parameters. $VT^n=C$, where V and T are in the unit of *fpm* and minutes, respectively.

Taylor's tool life equation, $VT^n = C$

$$350 \times 60^n = C$$

$$500 \times 10^n = C$$

$$6^n = 1.43 \Rightarrow n = 0.2$$

$$C = 350 \times 60^{0.2} = 793.8$$

- (b) Calculate the optimal cutting speed for this operation to yield the minimum machining cost per part. (Hint: pay attention to the units).

$$T_{\min} = \left(\frac{1}{n} - 1 \right) \left(\frac{C_i + T_c C_o}{C_o} \right) = \left(\frac{1}{0.2} - 1 \right) \left(\frac{15 + 2 \times 2}{2} \right)$$

$$= 11.4 \text{ min}$$

$$V_{\min} = \frac{C}{T_{\min}^n} = \frac{793.8}{11.4^{0.2}} = 487.9 \text{ fpm}$$

- (c) Calculate the estimated power consumption for this material if the specific cutting energy for this material is known to be 0.6 hp/in³/min?

$$HP = HP_s \times MRR$$

$$= 0.6 \times 0.025 \times 0.015 \times 487.9 \times 12$$

$$= 1.38 \text{ hp}$$

- (d) Calculate the cost per part at the optimal cutting speed calculated in part (b), assuming that the loading and unloading time per part is 120 seconds in total. (Hint: the operating cost for the time spent on the part loading and unloading is the handling cost C_4).

$$CT = \frac{L}{f_m} = \frac{L}{f_r N} = \frac{L\pi D}{f_r 12V} = \frac{10 \times \pi \times 2}{0.025 \times 12 \times 383.5} = 0.55 \text{ min}$$

$$C = CT \cdot \left(C_0 + \frac{C_t + C_0 T_c}{T} \right) + \$2 \times 2$$

$$= 0.55 \times \left(2 + \frac{15 + 2 \times 2}{38} \right) + \$2 \times 2$$

$$= 1.1 + 0.22 + 0.06 + 4$$

$$= 1.375 + 4 = \$5.375$$

5. Multiple Choice Problems. Select the right answer to the question. There is only one answer for each question. (40 pts)
- A. Which of the following mechanical properties of a medium carbon steel typically increases with the temperature:
- (a) Ultimate tensile strength
 - (b) Fatigue life
 - (c) True strain right before fracture
 - (d) Hardness
- B. Metal A has a higher yield strength but smaller elastic modulus (Young's modulus) than Metal B. Both Metal A and B are linear elastic material up to their yield points. Which of the following statements is definitely correct for Metal A and B specimens during tensile tests:
- (a) Metal A has a larger strain at the yield point than Metal B.
 - (b) Metal A has a smaller hardness than Metal B
 - (c) Metal A has a smaller resilience than Metal B
 - (d) Metal A has a shorter fatigue life than B.
- C. For a turning process on a given workpiece using a given cutting tool, if the cutting speed V is increased, the feed per round (f_r) is increased and the cutting depth remains the same, then which of the following statements is correct:
- (a) The material removal rate decreases.
 - (b) The spindle speed N increases
 - (c) The main cutting force decreases
 - (d) The cutting power remains the same
- D. Which of the following statements about cutting tools is correct:
- (a) A tungsten carbide cutting tool has no metallic component.
 - (b) To produce coated tungsten carbide cutting tools, people can use either physical vapor deposition or chemical vapor deposition.
 - (c) A polycrystalline diamond cutting tool can be suitably used to cut low carbon steel.
 - (d) A Sialon cutting tool can be suitably used to cut steels.

- E. Which of the following typically increases the fatigue strength of a metal workpiece
- (a) A higher environmental temperature
 - (b) A smoother surface
 - (c) Tensile surface residual stresses and compressive residual stresses in the workpiece's inner region
 - (d) A larger number of cracks
- F. Which one of the following gage blocks represents the grade with the **highest** accuracy?
- (a) 0.5
 - (b) 1
 - (c) 2
 - (d) 3
- G. Choose an incorrect statement:
- (a) Job shop is a general purpose manufacturing operation like student machine shop.
 - (b) Flow shop is like a chemical plant.
 - (c) Cell shop **may** consists of various programmable CNC machines that can be used for machining of various parts
 - (d) Project shop represents operations such as construction of a bridge.
- H. Which one of the following workpiece properties is NOT a critical factor to machinability?
- (a) Microstructure and the resulting hardness
 - (b) Chemistry
 - (c) Fatigue strength
 - (d) Compatibility with cutting tool material
- I. Choose an incorrect statement related to milling.
- (a) In upmilling, chip thickness changes from thin to thick.
 - (b) Higher clamping force is needed in upmilling than in downmilling
 - (c) Downmilling is more likely to induce chatter than upmilling
 - (d) Downmilling is also called climb milling.

