

1. (30 pts)
  - a) Starting from the differential forms of Maxwell's equations, derive a homogeneous Helmholtz equation (a wave equation) for the electric field valid in a linear, isotropic, source-free medium characterized by dielectric permittivity  $\epsilon_0$  and magnetic permeability  $\mu_0$ . You may find this vector identity useful:  $\nabla \times \nabla \times \vec{A} \equiv \nabla(\nabla \cdot \vec{A}) - \nabla^2 \vec{A}$ , where  $\vec{A}$  is an arbitrary 3-component vector.
  - b) Assuming  $e^{i\omega t}$  time dependence, rewrite your electric field wave equation and give expressions for the electric field vector and the associated magnetic field vector valid for a time-harmonic, linearly polarized, plane wave solution to your wave equation (assume +z wave propagation).
  - c) Find an expression for the phase velocity of the wave in part b) in terms of  $\epsilon_0$  and  $\mu_0$ . Is there dispersion in this medium?

2. (30 pts) A two-conductor transmission line is driven by a voltage source  $V_G$  (with internal resistance  $R_G$ ) and is terminated by a load resistance  $R_L$ , as shown in Figure 1. The transmission line has a characteristic impedance of  $Z_0$  and length  $L$  in the  $x$  direction. The voltage source output has the form  $V_G = V_0 \cos(\omega t)$  volts.
- Assume  $R_L = Z_0/2$ . What resistance  $Z_Q$  can you put in parallel with the line  $\lambda/4$  in front of the load to eliminate reflections on the generator side of that resistance?
  - Assume  $R_L = 0$  (short circuit termination),  $Z_0 = R_G$  and  $L = 2.75\lambda$ . If the voltage source has been on for a long time, find an expression for the voltage between the conductors valid for all values of  $x$ .
  - What are the conditions on  $L$  and  $\omega$  under which this transmission line system could be analyzed using static circuit theory techniques? Explain your answer briefly.

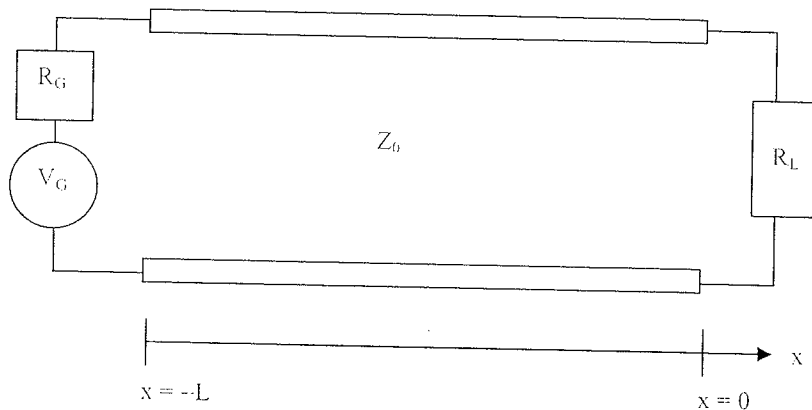


Figure 1: Transmission line (for problem 2).

3. (40 pts) A hollow waveguide with a rectangular cross section and perfectly conducting, metallic walls is shown in Figure 2. The relevant dimensions of the waveguide are also given. The hollow waveguide is filled with a perfect (lossless) dielectric characterized by  $\epsilon_0$  and  $\mu_0$ . The waveguide is several hundred km long.
- Determine an expression for the cutoff frequency of this waveguide and evaluate your answer numerically.
  - Write an expression for the waveguide propagation constant  $\beta$  in terms of the waveguide dimensions and the dielectric constants ( $\epsilon_0$  and  $\mu_0$ ).
  - Write the instantaneous time domain expression for the z-component of the magnetic field ( $H_z$ ) for the lowest-order mode that will propagate in this waveguide.
  - A 12 GHz carrier signal is modulated by a 2.5 GHz data signal (5 GHz total modulation bandwidth) and is transmitted on this waveguide. In the time domain, the electric field for the modulated wave can be written as  $E_0 \cos(\omega_1 t) \cos(\omega_2 t)$ , where  $\omega_1 = 5\pi \times 10^9$  rad/s and  $\omega_2 = 24\pi \times 10^9$  rad/s. Determine what frequencies will exit the waveguide at the far end, and describe the waveguide's effects on the combination of the carrier and modulation waves.

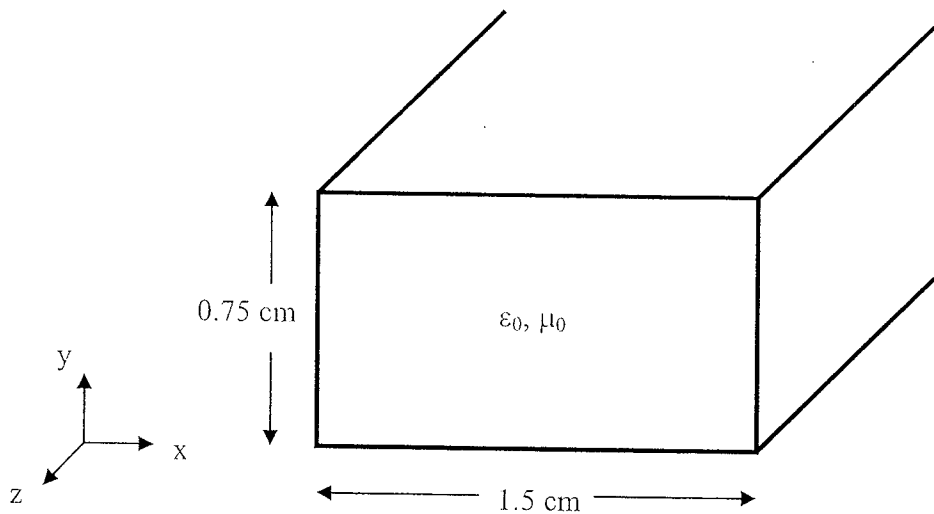


Figure 2: Hollow waveguide with perfectly conducting walls (for problem 3).

Maxwell's Equations, in differential and integral form are: Other potentially useful relationships are:

$$\begin{aligned} \vec{\nabla} \times \vec{E} &= -\frac{\partial \vec{B}}{\partial t} & \oint_c \vec{E} \cdot d\vec{\ell} &= -\frac{\partial}{\partial t} \int_s \vec{B} \cdot d\vec{s} & \vec{D} &= \epsilon_0 \vec{E} + \vec{P} = \epsilon_0 \vec{E} \\ \vec{\nabla} \times \vec{H} &= \vec{J} + \frac{\partial \vec{D}}{\partial t} & \oint_c \vec{H} \cdot d\vec{\ell} &= \int_s \left( \vec{J} + \frac{\partial \vec{D}}{\partial t} \right) \cdot d\vec{s} & \vec{B} &= \mu_0 (\vec{H} + \vec{M}) = \mu \vec{H} \\ \vec{\nabla} \cdot \vec{D} &= \rho & \oint_s \vec{D} \cdot d\vec{s} &= Q & \lambda &= \frac{2\pi}{\beta} = \frac{u}{f} = \frac{1}{f\sqrt{\mu\epsilon}} \\ \vec{\nabla} \cdot \vec{B} &= 0 & \oint_s \vec{B} \cdot d\vec{s} &= 0 & \epsilon_0 &= 8.854 \times 10^{-12} \text{ F/m} \\ & & & & \mu_0 &= 4\pi \times 10^{-7} \text{ H/m} \end{aligned}$$

Vector Differential Relationships in Cylindrical Coordinates (r, φ, z)

$$\vec{\nabla} V = \hat{a}_r \frac{\partial V}{\partial r} + \hat{a}_\phi \frac{\partial V}{r \partial \phi} + \hat{a}_z \frac{\partial V}{\partial z}$$

$$\vec{\nabla} \cdot \vec{A} = \frac{1}{r} \frac{\partial}{\partial r} (r A_r) + \frac{\partial A_\phi}{r \partial \phi} + \frac{\partial A_z}{\partial z}$$

$$\vec{\nabla} \times \vec{A} = \hat{a}_r \left( \frac{\partial A_z}{r \partial \phi} - \frac{\partial A_\phi}{\partial z} \right) + \hat{a}_\phi \left( \frac{\partial A_r}{\partial z} - \frac{\partial A_z}{\partial r} \right) + \hat{a}_z \frac{1}{r} \left[ \frac{\partial}{\partial r} (r A_\phi) - \frac{\partial A_r}{\partial \phi} \right]$$

$$\nabla^2 V = \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial V}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 V}{\partial \phi^2} + \frac{\partial^2 V}{\partial z^2}$$

Divergence Thm:  $\int_v \vec{\nabla} \cdot \vec{A} dv = \oint_s \vec{A} \cdot d\vec{s}$

For lossless transmission lines:

Stokes Thm:  $\int_v \vec{\nabla} \times \vec{A} \cdot d\vec{s} = \oint_c \vec{A} \cdot d\vec{\ell}$

$$Z_{in} = R_o \frac{Z_L + jR_o \tan \beta \ell}{R_o + jZ_L \tan \beta \ell}$$