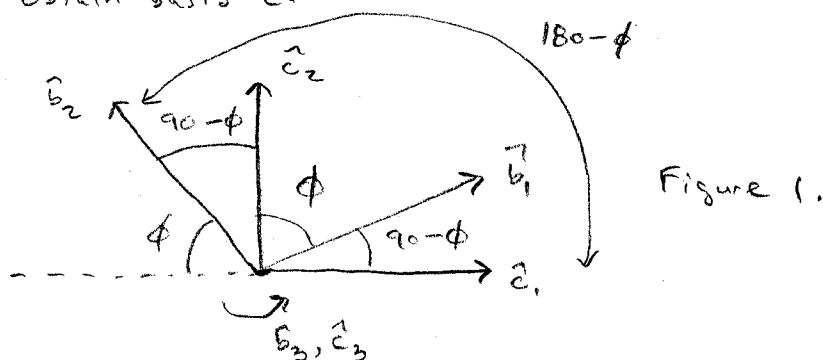


Problem #1

The strategy is to express the satellite position in the b basis first, and then transform the individual components from the b basis to the ENM basis. I will do this through two successive rotations involving an intermediate c basis.

First, I will rotate the b basis about the b_3 axis in order to obtain basis c .



Assume that we have a vector, $\vec{r}(t)$, whose components are expressed in terms of the b basis. In general, we have:

$$\vec{r}(t) = d \vec{b}_1 + e \vec{b}_2 + f \vec{b}_3$$

where d , e , and f are scalar components. Our goal is to express this same vector in terms of the c basis:

$$\vec{r}(t) = g \vec{c}_1 + h \vec{c}_2 + m \vec{c}_3$$

So we must compute g , h , and m . In order to compute g , for example, we must find out "how much" of $\vec{r}(t)$ is in the direction of g . So, we take the dot product of $\vec{r}(t)$ with \hat{c}_1 , which is the unit vector associated with g .

$$g = \vec{r}(t) \cdot \hat{c}_1$$

(2)

In general, portions of components d , e , and f could contribute to component g , so all three unit vectors \hat{b}_1 , \hat{b}_2 and \hat{b}_3 must be dotted with \hat{c}_1 in order to ensure that the appropriate amounts of d , e , and f are "fully represented" in g . So:

$$g = \vec{r}(t)_{|b} \cdot \hat{c}_1 = d(\hat{b}_1 \cdot \hat{c}_1) + e(\hat{b}_2 \cdot \hat{c}_1) + f(\hat{b}_3 \cdot \hat{c}_1)$$

Using a similar analysis, we can compute the component h . Again, we must add up the appropriate contributions of d , e , and f .

The "appropriate contributions" are found quantitatively by taking the dot products of \hat{b}_1 , \hat{b}_2 and \hat{b}_3 with \hat{c}_2 respectively.

$$h = \vec{r}(t)_{|b} \cdot \hat{c}_2 = d(\hat{b}_1 \cdot \hat{c}_2) + e(\hat{b}_2 \cdot \hat{c}_2) + f(\hat{b}_3 \cdot \hat{c}_2)$$

Finally, m can be computed in an analogous fashion

$$m = \vec{r}(t)_{|b} \cdot \hat{c}_3 = d(\hat{b}_1 \cdot \hat{c}_3) + e(\hat{b}_2 \cdot \hat{c}_3) + f(\hat{b}_3 \cdot \hat{c}_3)$$

The three equations written above may be written more compactly in matrix format:

$$\begin{bmatrix} g \\ h \\ m \end{bmatrix} = \begin{bmatrix} (\hat{b}_1 \cdot \hat{c}_1) & (\hat{b}_2 \cdot \hat{c}_1) & (\hat{b}_3 \cdot \hat{c}_1) \\ (\hat{b}_1 \cdot \hat{c}_2) & (\hat{b}_2 \cdot \hat{c}_2) & (\hat{b}_3 \cdot \hat{c}_2) \\ (\hat{b}_1 \cdot \hat{c}_3) & (\hat{b}_2 \cdot \hat{c}_3) & (\hat{b}_3 \cdot \hat{c}_3) \end{bmatrix} \begin{bmatrix} d \\ e \\ f \end{bmatrix}$$

The dot product between vectors \vec{A} & \vec{B} is defined as

$$\vec{A} \cdot \vec{B} = \|\vec{A}\| \|\vec{B}\| \cos \beta$$

where the angle β is the angle formed when the two vectors are connected tail to tail while maintaining the same relative orientation to each other. In the special case of two unit vectors, $\|\vec{A}\|$ and $\|\vec{B}\|$ are always one, so the dot product just reduces

③

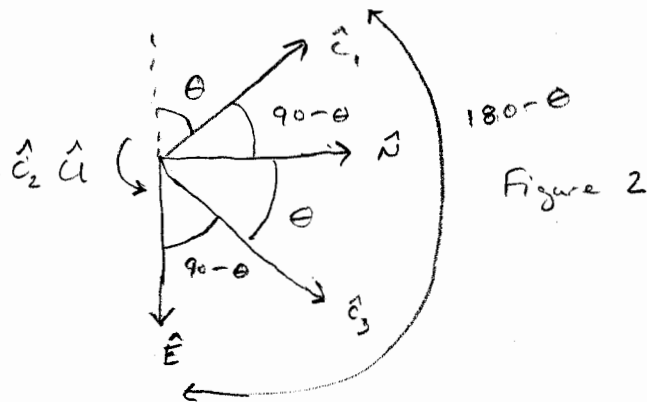
to the cosine of the angle between them. After examining Figure 1, it should be clear what the matrix elements are in terms of ϕ :

$$\begin{bmatrix} g \\ h \\ m \end{bmatrix} = \begin{bmatrix} \cos(90-\phi) & \cos(180-\phi) & 0 \\ \cos \phi & \cos(90-\phi) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} d \\ e \\ f \end{bmatrix}$$

From trig. identities, we know that $\cos(90-\phi) = \sin \phi$ and $\cos(180-\phi) = -\cos \phi$. Making these substitutions, we have

$$\begin{bmatrix} g \\ h \\ m \end{bmatrix} = \begin{bmatrix} \sin \phi & -\cos \phi & 0 \\ \cos \phi & \sin \phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} d \\ e \\ f \end{bmatrix}$$

This is our 1st rotation matrix. We need to rotate the e basis about the \hat{c}_2 axis in order to obtain the ENU basis, which is our ultimate goal.



We wish to express $\vec{R}(t)_{|c}$, currently using components $g, h, \& m,$ in terms of components in the ENU basis:

$$\vec{R}(t)_{|ENU} = n \hat{E} + p \hat{N} + q \hat{c}_1$$

(4)

Using the same analysis used previously, we can compute the n , p , and q components in terms of the components of g , h , and m using 3 equations:

$$n = \bar{R}(t)_{1c} \cdot \hat{E} = g(\hat{c}_1 \cdot \hat{E}) + h(\hat{c}_2 \cdot \hat{E}) + m(\hat{c}_3 \cdot \hat{E})$$

$$p = \bar{R}(t)_{2c} \cdot \hat{N} = g(\hat{c}_1 \cdot \hat{N}) + h(\hat{c}_2 \cdot \hat{N}) + m(\hat{c}_3 \cdot \hat{N})$$

$$q = \bar{R}(t)_{3c} \cdot \hat{U} = g(\hat{c}_1 \cdot \hat{U}) + h(\hat{c}_2 \cdot \hat{U}) + m(\hat{c}_3 \cdot \hat{U})$$

In matrix format,

$$\begin{bmatrix} n \\ p \\ q \end{bmatrix} = \begin{bmatrix} (\hat{c}_1 \cdot \hat{E}) & (\hat{c}_2 \cdot \hat{E}) & (\hat{c}_3 \cdot \hat{E}) \\ (\hat{c}_1 \cdot \hat{N}) & (\hat{c}_2 \cdot \hat{N}) & (\hat{c}_3 \cdot \hat{N}) \\ (\hat{c}_1 \cdot \hat{U}) & (\hat{c}_2 \cdot \hat{U}) & (\hat{c}_3 \cdot \hat{U}) \end{bmatrix} \begin{bmatrix} g \\ h \\ m \end{bmatrix}$$

Looking at Figure 2, the dot products can be replaced:

$$\begin{bmatrix} n \\ p \\ q \end{bmatrix} = \begin{bmatrix} \cos(180-\theta) & 0 & \cos(90-\theta) \\ \cos(90-\theta) & 0 & \cos\theta \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} g \\ h \\ m \end{bmatrix}$$

Using trig identities, the matrix can be written as:

$$\begin{bmatrix} n \\ p \\ q \end{bmatrix} = \begin{bmatrix} -\cos\theta & 0 & \sin\theta \\ \sin\theta & 0 & \cos\theta \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} g \\ h \\ m \end{bmatrix}$$

This is our 2nd rotation matrix. Remember that our ultimate goal was to transform the components in the b basis, or d , e , and f in this case, to the components in the ENU basis, or n , p , and q in this case. So, we eliminate the 3×1 matrix containing g , h , and m by substituting the matrix equation containing the 1st rotation matrix into the matrix equation containing the 2nd rotation matrix. The resulting matrix equation looks like this:

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$$\begin{bmatrix} n \\ p \\ q \end{bmatrix} = \underbrace{\begin{bmatrix} -\cos\theta & 0 & \sin\theta \\ \sin\theta & 0 & \cos\theta \\ 0 & 1 & 0 \end{bmatrix}}_{2^{\text{nd}} \text{ rotation matrix}} \underbrace{\begin{bmatrix} \sin\phi & -\cos\phi & 0 \\ \cos\phi & \sin\phi & 0 \\ 0 & 0 & 1 \end{bmatrix}}_{1^{\text{st}} \text{ rotation matrix}} \begin{bmatrix} d \\ e \\ f \end{bmatrix}$$

If the two rotation matrices are multiplied together, the result is

$$\begin{bmatrix} n \\ p \\ q \end{bmatrix} = \begin{bmatrix} -\cos\theta \sin\phi & \cos\theta \cos\phi & \sin\theta \\ \sin\theta \sin\phi & -\sin\theta \cos\phi & \cos\theta \\ \cos\phi & \sin\phi & 0 \end{bmatrix} \begin{bmatrix} d \\ e \\ f \end{bmatrix}$$

Transformation matrix from b basis to ENU basis.

So, we have achieved our goal. θ and ϕ are functions of t which are given in the notes. I have not yet explicitly stated what d , e , and f are. Remember that the b basis rotates such that the \hat{b}_1 unit vector maintains a perfect lock on the satellite as it moves around. Thus, the range of the satellite has only a \hat{b}_1 component; the \hat{b}_2 and \hat{b}_3 components are always 0 for the direction of the tracking. In mathematical terms,

$$\vec{r}(t)_{|b} = d\hat{b}_1 + \cancel{e\hat{b}_2} + \cancel{f\hat{b}_3} = d\hat{b}_1, \text{ where}$$

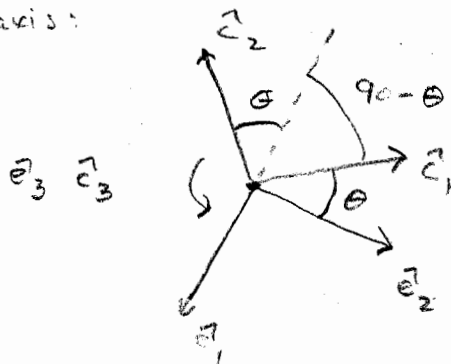
$d = 8000 + 10.0t$ km, as given in the problem.

Sample MATLAB code and the plot are included.

Problem #2

Part 1:

Define an intermediate basis c . Rotate the e basis about the \hat{e}_3 or \hat{c}_3 axis:

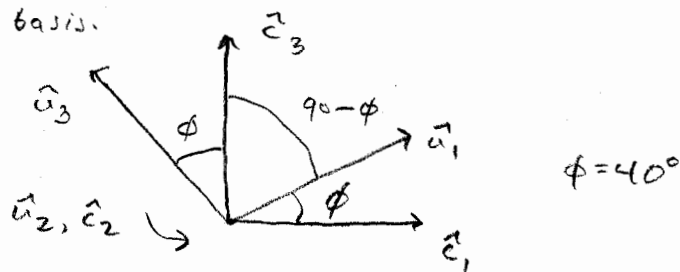


The first rotation matrix is

$$\begin{bmatrix} \hat{c}_1 \cdot \hat{e}_1 & \hat{c}_1 \cdot \hat{e}_2 & \hat{c}_1 \cdot \hat{e}_3 \\ \hat{c}_2 \cdot \hat{e}_1 & \hat{c}_2 \cdot \hat{e}_2 & \hat{c}_2 \cdot \hat{e}_3 \\ \hat{c}_3 \cdot \hat{e}_1 & \hat{c}_3 \cdot \hat{e}_2 & \hat{c}_3 \cdot \hat{e}_3 \end{bmatrix} = \begin{bmatrix} -\sin\theta & \cos\theta & 0 \\ -\cos\theta & -\sin\theta & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Note that $\theta = 25^\circ$ rather than 115° because I have chosen to measure c from the \hat{e}_2 axis rather than the \hat{e}_1 axis.

Now I will do a second rotation to transform from the c basis to the u basis.



$$\begin{bmatrix} \hat{u}_1 \cdot \hat{c}_1 & \hat{u}_1 \cdot \hat{c}_2 & \hat{u}_1 \cdot \hat{c}_3 \\ \hat{u}_2 \cdot \hat{c}_1 & \hat{u}_2 \cdot \hat{c}_2 & \hat{u}_2 \cdot \hat{c}_3 \\ \hat{u}_3 \cdot \hat{c}_1 & \hat{u}_3 \cdot \hat{c}_2 & \hat{u}_3 \cdot \hat{c}_3 \end{bmatrix} = \begin{bmatrix} \cos\phi & 0 & \sin\phi \\ 0 & 1 & 0 \\ -\sin\phi & 0 & \cos\phi \end{bmatrix}$$

(7)

So, the full transformation matrix from the e basis to the u basis is:

$$\begin{bmatrix} \cos\phi & 0 & \sin\phi \\ 0 & 1 & 0 \\ -\sin\phi & 0 & \cos\phi \end{bmatrix} \begin{bmatrix} -\sin\theta & \cos\theta & 0 \\ -\cos\theta & -\sin\theta & 0 \\ 0 & 0 & 1 \end{bmatrix} =$$

$$\begin{bmatrix} -\cos\phi \sin\theta & \cos\phi \cos\theta & \sin\phi \\ -\cos\theta & -\sin\theta & 0 \\ \sin\phi \sin\theta & -\sin\phi \cos\theta & \cos\phi \end{bmatrix}$$

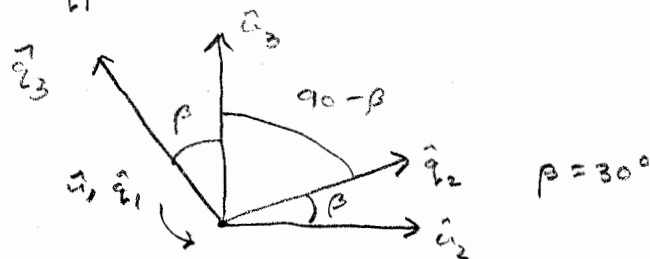
Now substitute in $\theta = 25^\circ$ and $\phi = 40^\circ$

$$\begin{bmatrix} -.32 & .69 & .64 \\ -.91 & -.42 & 0 \\ -.27 & -.58 & .77 \end{bmatrix}$$

$e \rightarrow u$

Part #2:

First find the matrix from u to q . This requires only one rotation about \hat{u}_1 or \hat{q}_1 :



The rotation matrix is:

$$\begin{bmatrix} \hat{u}_1 \cdot \hat{q}_1 & \hat{u}_2 \cdot \hat{q}_1 & \hat{u}_3 \cdot \hat{q}_1 \\ \hat{u}_1 \cdot \hat{q}_2 & \hat{u}_2 \cdot \hat{q}_2 & \hat{u}_3 \cdot \hat{q}_2 \\ \hat{u}_1 \cdot \hat{q}_3 & \hat{u}_2 \cdot \hat{q}_3 & \hat{u}_3 \cdot \hat{q}_3 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\beta & \sin\beta \\ 0 & -\sin\beta & \cos\beta \end{bmatrix}$$

Now we can go from $e \rightarrow u \rightarrow q$. We already know the transformation matrix for $e \rightarrow u$: since it was calculated in part 1.

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Now I simply need to multiply the matrix that I just computed by the one obtained in part 1 to obtain the transformation matrix from $e \rightarrow q$.

$$\begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\beta & \sin\beta \\ 0 & -\sin\beta & \cos\beta \end{bmatrix} \begin{bmatrix} -.32 & .69 & .64 \\ -.91 & -.42 & 0 \\ .27 & -.58 & -.77 \end{bmatrix} = \begin{bmatrix} -.32 & .69 & .64 \\ -.65 & -.65 & .38 \\ .69 & -.29 & .67 \end{bmatrix}$$

$\beta = 30^\circ$ $e \rightarrow q$

Part #3:

a) Since we are transforming from the e basis to the q basis, use the matrix computed in part 2.

$$\begin{bmatrix} q_1 \\ q_2 \\ q_3 \end{bmatrix} = \begin{bmatrix} -.32 & .69 & .64 \\ -.65 & -.65 & .38 \\ .69 & -.29 & .67 \end{bmatrix} \begin{bmatrix} 0.5 \\ -1.3 \\ -0.5 \end{bmatrix} = \begin{bmatrix} -1.38 \\ .33 \\ .39 \end{bmatrix}$$

e

Therefore, $\vec{r} = -1.38q_1 + .33q_2 + .39q_3$ cm

b) Here we are transforming from $w \rightarrow q_1$, so use the second rotation matrix computed in part 2:

$$\begin{bmatrix} q_1 \\ q_2 \\ q_3 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & .87 & .50 \\ 0 & -.50 & .87 \end{bmatrix} \begin{bmatrix} 13.1 \\ 5.5 \\ -2.4 \end{bmatrix} = \begin{bmatrix} 13.1 \\ 3.56 \\ -4.83 \end{bmatrix}$$

Therefore, $\vec{\omega} = 13.1q_1 + 3.56q_2 - 4.83q_3$ sec^{-1}

Part #4:

a) The goal is to go from $w \rightarrow e$, so we use the transpose of the matrix that was computed in part 1:

(9)

$$\begin{bmatrix} e_1 \\ e_2 \\ e_3 \end{bmatrix} = \begin{bmatrix} -.32 & -.91 & -.27 \\ .69 & -.42 & -.58 \\ .64 & 0 & .77 \end{bmatrix} \begin{bmatrix} 2.5 \times 10^3 \\ 10.4 \times 10^3 \\ -1.1 \times 10^3 \end{bmatrix} = \begin{bmatrix} -1.05 \times 10^4 \\ -2.0 \times 10^4 \\ .08 \times 10^4 \end{bmatrix}$$

Therefore, $\vec{r} = (-1.05 \times 10^4) \vec{e}_1 - (2.0 \times 10^4) \vec{e}_2 + (.08 \times 10^4) \vec{e}_3$ km

b)

We are going from $q \rightarrow e$, so I will use the transpose of the matrix that was computed in problem #2:

$$\begin{bmatrix} e_1 \\ e_2 \\ e_3 \end{bmatrix} = \begin{bmatrix} -.32 & -.65 & .69 \\ .69 & -.65 & -.29 \\ .64 & .38 & .67 \end{bmatrix} \begin{bmatrix} 3.1 \\ -9.9 \\ 3.1 \end{bmatrix} = \begin{bmatrix} 7.61 \\ 7.70 \\ .24 \end{bmatrix}$$

Therefore $\vec{\omega} = 7.61 \vec{e}_1 + 7.71 \vec{e}_2 + .24 \vec{e}_3$ sec⁻¹

```
clear
format long
step = .01;
t = 0: step: 60;
num_t = length(t);
deg_rad = pi./180;
a = 1;
for a = 1:num_t,
    phi(1, a) = (75 - 1.5.*t(1, a)).*deg_rad;
    a = a + 1;
end
b = 1;
for b = 1:num_t,
    theta(1, b) = (80 + 0.75.*t(1, b)).*deg_rad;
    b = b + 1;
end
c = 1;
for c = 1:num_t,
    range(c, 1) = 8000 + 10.*t(1, c);
    c = c + 1;
end
d = 1;
for d = 1:num_t,
    trans_b_enu = [-cos(theta(1, d)).*sin(phi(1, d)), cos(theta(1, d)).*cos(phi(1, d)),
sin(theta(1, d));
    sin(theta(1, d)).*sin(phi(1, d)), -sin(theta(1, d)).*cos(phi(1, d)), cos(theta(1,
d));
    cos(phi(1, d)), sin(phi(1, d)), 0];
    e_n_u = trans_b_enu*[range(d, 1); 0; 0];
    enu_E(1, d) = e_n_u(1, 1);
    enu_N(1, d) = e_n_u(2, 1);
    enu_U(1, d) = e_n_u(3, 1);
    d = d + 1;
end
plot(t, enu_E, 'k', t, enu_N, 'g', t, enu_U, 'r')
title('E, N, and U, components of satellite position vs. time, by Philip Haberlen')
xlabel('t, seconds')
ylabel('E, N, and U components, kilometers')
legend('E - black', 'N - green', 'U - red', 'Location', 'NorthEastOutside')
```

E, N, and U, components of satellite position vs. time, by Philip Habermen

