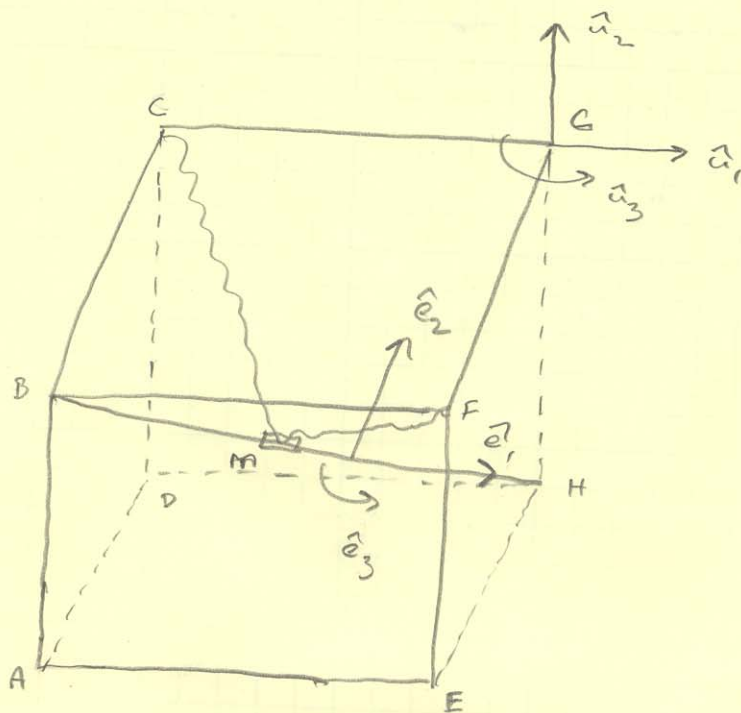
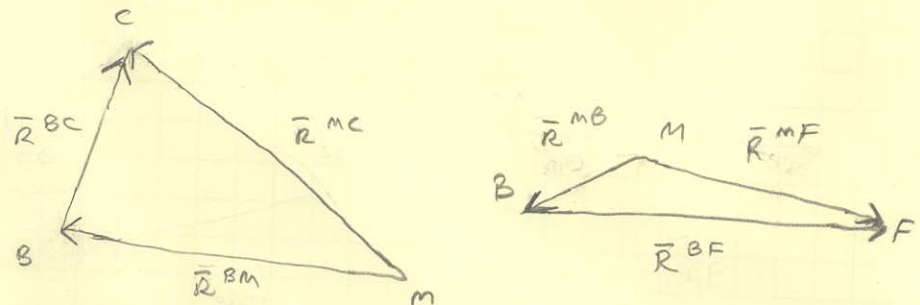


Define two bases as shown below.



We need expressions for the two unit vectors that point along the springs. Consider triangles BMC and BMF.



From vector addition, we know that

$$\vec{r}^{MC} = \vec{r}^{MB} + \vec{r}^{BC} \quad \text{and}$$

$$\vec{r}^{MF} = \vec{r}^{MB} + \vec{r}^{BF}$$

Substituting in appropriate numbers, we have

$$\vec{r}^{MC} = -x\hat{e}_1 - 12c\hat{u}_3 \quad \text{cm}$$

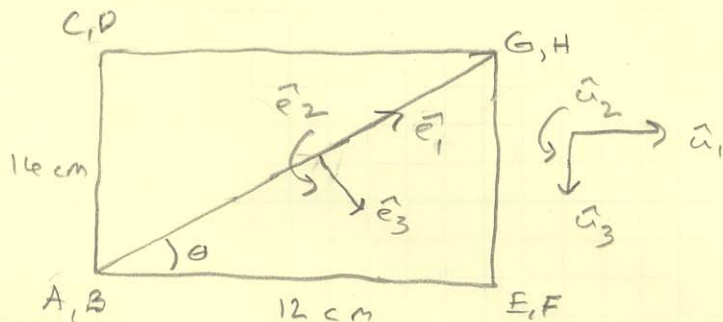
$$\vec{r}^{MF} = -x\hat{e}_1 + 12\hat{u}_1 \quad \text{cm}$$

(2)

Convert the \hat{u} basis into the \hat{e} basis. We can define each unit vector in \hat{e} as follows

$$\hat{e}_1 = \frac{\vec{r}^{BH}}{|\vec{r}^{BH}|} = \frac{12\hat{u}_1 - 12\hat{u}_2 - 16\hat{u}_3}{\sqrt{12^2 + (-12)^2 + (-16)^2}} = .514\hat{u}_1 - .514\hat{u}_2 - .686\hat{u}_3$$

\hat{e}_3 is \perp to the plane ABGH. If we look "down" on the figure, we see



$$\hat{e}_3 = \sin\theta \hat{u}_1 + \cos\theta \hat{u}_3$$

$$\sin\theta = \frac{16}{\sqrt{12^2 + 16^2}} = .8$$

$$\cos\theta = \frac{12}{\sqrt{12^2 + 16^2}} = .6$$

$$\hat{e}_3 = .8\hat{u}_1 + .6\hat{u}_3$$

\hat{e}_2 completes a right-handed set, so we have

$$\hat{e}_2 = \hat{e}_3 \times \hat{e}_1 = (.8\hat{u}_1 + .6\hat{u}_3) \times (.514\hat{u}_1 - .514\hat{u}_2 - .686\hat{u}_3)$$

$$= (.8\hat{u}_1 \times .514\hat{u}_1) + (.8\hat{u}_1 \times -.514\hat{u}_2) + (.8\hat{u}_1 \times -.686\hat{u}_3) \\ + (.6\hat{u}_3 \times .514\hat{u}_1) + (.6\hat{u}_3 \times -.514\hat{u}_2) + (.6\hat{u}_3 \times -.686\hat{u}_3)$$

$$= -.4112\hat{u}_3 + .5488\hat{u}_2 + .3084\hat{u}_2 + .3084\hat{u}_1$$

$$= .3084\hat{u}_1 + .8572\hat{u}_2 - .4112\hat{u}_3$$

(3)

I can convert the \hat{u} components to the \hat{e} components now:

$$\begin{aligned}\vec{r}^{MC} &= -x\hat{e}_1 - 16(-.686)\hat{e}_1 - 16(-.4112)\hat{e}_2 - 16(.6)\hat{e}_3 \\ &= (10.976 - x)\hat{e}_1 + 6.5792\hat{e}_2 - 9.6\hat{e}_3\end{aligned}$$

$$\begin{aligned}\vec{r}^{MF} &= -x\hat{e}_1 + 12(.514)\hat{e}_1 + 12(.3084)\hat{e}_2 + 12(.8)\hat{e}_3 \\ &= (6.168 - x)\hat{e}_1 + 3.7008\hat{e}_2 + 9.6\hat{e}_3\end{aligned}$$

These spring vectors can be converted into unit vectors:

$$\hat{e}^{MC} = \frac{(10.976 - x)\hat{e}_1 + 6.5792\hat{e}_2 - 9.6\hat{e}_3}{\sqrt{(10.976 - x)^2 + (6.5792)^2 + (-9.6)^2}}$$

$$\hat{e}^{MF} = \frac{(6.168 - x)\hat{e}_1 + 3.7008\hat{e}_2 + 9.6\hat{e}_3}{\sqrt{(6.168 - x)^2 + (3.7008)^2 + (9.6)^2}}$$

The unit vector for the weight force is

$$\begin{aligned}\hat{e}_w &= -\hat{u}_2 \quad \text{OR after converting to the } \hat{e} \text{ basis} \\ &= .514\hat{e}_1 - .8572\hat{e}_2\end{aligned}$$

The normal force that the rod exerts on the mass will have two orthogonal components. Note that the rod does not exert a force parallel to it since it is frictionless.

$$\hat{e}_{n1} = \hat{e}_2$$

$$\hat{e}_{n2} = \hat{e}_3$$

We need expressions for the spring forces. Since both springs are linear, they obey Hooke's Law:

$$\vec{F}_{\text{spring}} = k(y - l)\hat{u}_{\text{spring}}$$

where " l " is the unloaded length of the spring, " y " is the

(4)

loaded length of the spring, and k is the spring constant, \hat{u}_{spring} is the unit vector pointed in the direction of spring extension, and \vec{F}_{spring} is the force that the spring exerts. The usual negative sign has been omitted since we are assuming positive displacements to be in the direction of spring extension. The spring constant k is given for both springs, as is the equilibrium length " l ." \hat{u}_{spring} for each spring was computed on page 3. The loaded length, " y ," is just the magnitude of the position vectors along the springs, $\|\vec{r}^{MC}\|$ and $\|\vec{r}^{MF}\|$. These magnitudes appear in the denominators of the unit vectors \hat{e}^{MC} and \hat{e}^{MF} , computed on page 3. We can substitute those expressions into Hooke's Law for both springs and also write down the vector force equations for the other forces.

$$\vec{F}_{MC} = k \left[\sqrt{(10.926-x)^2 + (6.5792)^2 + (-9.6)^2} - l \right] \hat{e}_{MC}$$

$$\vec{F}_{MF} = k \left[\sqrt{(6.168-x)^2 + (3.7008)^2 + (-9.6)^2} - l \right] \hat{e}_{MF}$$

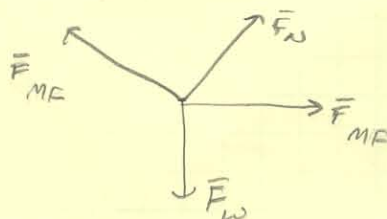
where \hat{e}_{MC} and \hat{e}_{MF} are given on page 3.

$$\vec{F}_N = F_{N1} \hat{e}_2 + F_{N2} \hat{e}_3$$

$$\vec{F}_W = (1.5 \text{ kg}) \left(9.806 \frac{\text{m}}{\text{s}^2} \right) \hat{e}_W$$

where \hat{e}_W is given on page 3.

A free-body diagram for the block appears below



5

From static equilibrium, we have

$$\Sigma \vec{F} = \vec{F}_{MC} + \vec{F}_{MF} + \vec{F}_N + \vec{F}_W = 0$$

This is a vector equation, so it can be split up into 3 scalar equations. I am substituting in $k = 1.22 \frac{N}{cm}$, $l = 6cm$, and the expressions for \vec{e}_{MC} , \vec{e}_{MF} , and \vec{e}_W as well.

$$(1.22) \left[\sqrt{(10.976-x)^2 + (6.5792)^2 + (-9.6)^2} - 6 \right]$$

$$\rightarrow \left[\frac{10.976-x}{\sqrt{(10.976-x)^2 + (6.5792)^2 + (-9.6)^2}} \right]$$

$$+ (1.22) \left[\sqrt{(6.168-x)^2 + (3.7008)^2 + (-9.6)^2} - 6 \right] \quad mg(0.514)$$

$$\rightarrow \left[\frac{6.168-x}{\sqrt{(6.168-x)^2 + (3.7008)^2 + (-9.6)^2}} \right] + 2.5201 = 0$$

$$(1.22) \left[\sqrt{(10.976-x)^2 + (6.5792)^2 + (-9.6)^2} - 6 \right]$$

$$\rightarrow \left[\frac{6.5792}{\sqrt{(10.976-x)^2 + (6.5792)^2 + (-9.6)^2}} \right]$$

$$+ (1.22) \left[\sqrt{(6.168-x)^2 + (3.7008)^2 + (-9.6)^2} \right]$$

$$\rightarrow \left[\frac{3.7008}{\sqrt{(6.168-x)^2 + (3.7008)^2 + (-9.6)^2}} \right] + F_{N1} - 4.203 = 0$$

(6)

$$(1.22) \left[\sqrt{(10.976-x)^2 + (6.5792)^2 + (-9.6)^2} - 6 \right]$$
$$\rightarrow \left[\frac{-9.6}{\sqrt{(10.976-x)^2 + (6.5792)^2 + (-9.6)^2}} \right]$$

$$+ (1.22) \left[\sqrt{(6.168-x)^2 + (3.7008)^2 + (-9.6)^2} - 6 \right]$$
$$\rightarrow \left[\frac{9.6}{\sqrt{(6.168-x)^2 + (3.7008)^2 + (-9.6)^2}} \right] + F_{N2} = 0$$

You will notice that the first equation contains only one variable, x , the variable that we are solving for. Because we transformed all of the vectors to a basis that was "lined up" with the rod, the two normal force components appeared in only two equations. If we had chosen a different basis, then at least one of the normal force components would have appeared in all 3 equations, complicating the solution process.

The first equation was solved numerically in MATLAB. See the attached M files for the details. If you run HW6, you will get $x = 10.78 \text{ cm}$ for an answer.

We were not asked to solve for the normal force components, but you could certainly do so using the second and third equations.

```
function F = spr3(x)
```

```
F = 1.22.*(sqrt((10.976 - x).^2 + (6.5856).^2 + (-9.6).^2) - 6).*(10.976 - x)./(sqrt((10.976 - x).^2 + (6.5856).^2 + (-9.6).^2)) + 1.22.*(sqrt((6.168 - x).^2 + (3.7044).^2 + (-9.6).^2) - 6).*(6.168 - x)./(sqrt((6.168 - x).^2 + (3.7044).^2 + (-9.6).^2)) + 2.5201;  
return
```

N:\AAE 203 Solutions\HW6.m
November 8, 2004

Page 1
10:41:37 AM

```
clear  
format long
```

```
x = fsolve(@spr3, 10)
```