A viscous, incompressible, Newtonian liquid is contained between two infinitely long plates that are separated by a distance, H. There are no pressure gradients in the horizontal direction. The top plate moves at constant velocity, U, and the bottom plate is fixed. No pressure gradients are applied in the *x*-direction. For a laminar flow, determine:

- 1. Determine the velocity distribution for this flow. Clearly state all assumptions and boundary conditions.
- 2. Determine the shear stress acting on the upper wall due to the fluid.



SOLUTION:

Make the following assumptions:

- 1. steady flow $\Rightarrow \frac{\partial}{\partial t} (\cdots) = 0$
- 2. gravity acts in the y-direction $\Rightarrow f_{B,y} = -g, f_{B,x} = 0, f_{B,z} = 0$
- 3. fully-developed flow in the x-direction $\Rightarrow \frac{\partial u_x}{\partial x} = \frac{\partial u_y}{\partial x} = \frac{\partial u_z}{\partial x} = 0$

4. the flow is planar
$$\Rightarrow u_z = 0, \frac{\partial}{\partial z}(\cdots) = 0$$

5. no pressure gradients in the horizontal direction
$$\Rightarrow \frac{\partial p}{\partial x} = \frac{\partial p}{\partial z} = 0$$

Write the continuity and Navier-Stokes equations in Cartesian coordinates for an incompressible fluid with constant viscosity.

$$\frac{\frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} + \frac{\partial u_z}{\frac{\partial z}{=0(4)}} = 0 \implies \frac{\partial u_y}{\partial y} = 0$$

From (3) and (4), $\frac{\partial u_y}{\partial x} = \frac{\partial u_y}{\partial z} = 0 \implies u_y = \text{constant}$

Since there is no flow through the wall boundaries: $u_y = 0$ (condition 6)

$$\rho \left(\frac{\partial u_x}{\partial t} + u_x \frac{\partial u_x}{\partial x} + \frac{u_y}{\partial (3)} \frac{\partial u_x}{\partial (0)} + \frac{u_z}{\partial (2)} \frac{\partial u_x}{\partial (2)} \right) = \rho \underbrace{f_{B,x}}_{=0(2)} - \frac{\partial p}{\partial (3)} + \mu \left(\frac{\partial^2 u_x}{\partial (2)^2} + \frac{\partial^2 u_x}{\partial (2)^2} + \frac{\partial^2 u_x}{\partial (2)^2} + \frac{\partial^2 u_x}{\partial (2)^2} \right)$$

$$\rho \left(\frac{\partial u_y}{\partial t} + u_x \frac{\partial u_y}{\partial (2)^2} + \frac{u_y}{\partial (2)^2} \frac{\partial u_y}{\partial (2)^2} + \frac{\partial^2 u_y}{\partial (2)^2} \right) = \rho \underbrace{f_{B,y}}_{=-g(2)} - \frac{\partial p}{\partial (2)^2} + \mu \left(\frac{\partial^2 u_y}{\partial (2)^2} + \frac{\partial^2 u_y}{\partial (2)^2} + \frac{\partial^2 u_y}{\partial (2)^2} + \frac{\partial^2 u_y}{\partial (2)^2} \right)$$

$$\rho \left(\frac{\partial u_z}{\partial t} + u_x \frac{\partial u_z}{\partial (2)^2} + \frac{\partial u_z}{\partial (2)^2} + \frac{\partial u_z}{\partial (2)^2} + \frac{\partial u_z}{\partial (2)^2} \right) = \rho \underbrace{f_{B,y}}_{=0(2)} - \frac{\partial p}{\partial (2)^2} + \mu \left(\frac{\partial^2 u_z}{\partial (2)^2} + \frac{\partial^2 u_z}{\partial (2)^2} + \frac{\partial^2 u_z}{\partial (2)^2} + \frac{\partial^2 u_z}{\partial (2)^2} \right)$$

Rewriting the momentum equations:

x-direction:
z-direction:
y-direction:

$$\frac{d^2 u_x}{dy^2} = 0$$

$$0 = 0$$

$$\frac{dp}{dy} = -\rho g$$

Note: Since u_x is not a fcn of x or z, we use a d/dy instead of $\partial/\partial y$.

Integrating the *x*-direction momentum equation twice:

$$\frac{d^2 u_x}{dy^2} = 0$$
$$\frac{d u_x}{dy} = c_1$$
$$u_x = c_1 y + c_2$$

Apply boundary conditions:

no-slip at y = 0:

no-slip at y = H:

$$u_x (y=0) = 0 \qquad \Rightarrow c_2 = 0$$
$$u_x (y=H) = U \qquad \Rightarrow c_1 = \frac{U}{H}$$

Thus, the velocity profile is:



The shear stress that the top wall exerts on the fluid is:

$$\sigma_{yx}(y=H) = \mu \left(\frac{\partial u_x}{\partial y} + \frac{\partial u_y}{\partial x}\right)_{y=H} = \frac{\mu U}{H}$$

From Newton's Third Law, the shear stress the fluid exerts on the wall is:

μU $\tau_{\rm on \ top \ wall} =$

shear stress acting on wall, $|\tau_{on \ top \ wall}|$

 \overline{m} shear stress acting on fluid element, σ_{yx} v