A wide flat belt moves vertically upward at constant speed, U, through a large bath of viscous liquid as shown in the figure. The belt carries with it a layer of liquid of constant thickness, h. The motion is steady and fully-developed after a small distance above the liquid surface level. The external pressure is atmospheric (constant) everywhere.



- a. Simplify the governing equations to a form applicable for this particular problem.
- b. State the appropriate boundary conditions
- c. Determine the velocity profile in the liquid.
- d. Determine the volumetric flow rate per unit depth.

SOLUTION:

Make the following assumptions.

- 1. steady flow
- 2. planar flow
- 3. fully-developed flow in the *y*-direction
- 4. gravity acts only in the -y-direction



$$\frac{\partial u_x}{\partial x} + \underbrace{\frac{\partial u_y}{\partial y}}_{=0(\#3)} = 0 \implies \frac{\partial u_x}{\partial x} = 0 \implies u_x = \text{constant} \quad (\text{Note that } u_x \text{ does not vary with either } y \text{ or } z \text{ either.})$$

 $\Rightarrow \partial_{\partial t}(\cdots) = 0$

 $\Rightarrow u_z = \frac{\partial}{\partial z} (\cdots) = 0$

 $\Rightarrow \frac{\partial u_x}{\partial y} = \frac{\partial u_y}{\partial y} = 0$

 $\Rightarrow g_x = g_z = 0, g_y = -g$

(1)

Since there is no flow through the belt,

$$u_x = 0$$
 (Call this condition #5.)

Consider the Navier-Stokes equation in the *x*-direction.

$$\rho \left[\underbrace{\frac{\partial u_x}{\partial t}}_{=0(\#1,\#5)} + \underbrace{u_x \frac{\partial u_x}{\partial x}}_{=0(\#5)} + u_y \underbrace{\frac{\partial u_x}{\partial y}}_{=0(\#3,\#5)} \right] = -\frac{\partial p}{\partial x} + \mu \left(\underbrace{\frac{\partial^2 u_x}{\partial x^2}}_{=0(\#5)} + \underbrace{\frac{\partial^2 u_x}{\partial y^2}}_{=0(\#3,\#5)} \right) + \rho \underbrace{g_x}_{=0(\#4)}$$

$$\therefore \frac{\partial p}{\partial x} = 0$$
(2)

Note that along the free surface of the liquid film the pressure remains constant (= p_{atm}). Hence, from Eqn. (2) the pressure everywhere in the film will be the same, *i.e.* $p(x,y) = p_{atm}$ (call this condition #6.).

Now consider the Navier-Stokes equation in the *y*-direction.

$$\rho \left[\frac{\partial u_y}{\partial t} + \underbrace{u_x}_{=0(\#1)} \frac{\partial u_y}{\partial x} + \underbrace{u_y}_{=0(\#3)} \frac{\partial u_y}{\partial y} \right] = -\frac{\partial p}{\partial y} + \mu \left(\frac{\partial^2 u_y}{\partial x^2} + \frac{\partial^2 u_y}{\partial y^2} \right) + \rho \underbrace{g_y}_{=-g}$$

Note that since u_y is neither a function of y or z, we can replace the partial derivative with an ordinary derivative.

$$0 = \mu \frac{d^2 u_y}{dx^2} - \rho g \tag{3}$$

Solve the differential equation given in Eqn. (3).

$$\frac{du_{y}}{dx} = \frac{\rho g}{\mu} x + c_{1}$$

$$u_{y} = \frac{1}{2} \frac{\rho g}{\mu} x^{2} + c_{1} x + c_{2}$$
(4)

Apply the following boundary conditions.

 $\frac{\text{ho-slip at } x = 0}{\text{ho-slip at } x = 0} \implies u_y(x = 0) = U \implies c_2 = U$

At the free surface, the air will provide a negligible resisting shear stress so:

no shear at
$$x = h$$
 $\Rightarrow \mu \frac{du_y}{dx}(x = h) = 0 \Rightarrow c_1 = -\frac{\rho g}{\mu}h$

Hence,

$$u_{y} = \frac{1}{2} \frac{g}{v} x^{2} - \frac{gh}{v} x + U \qquad (0 \le x \le h)$$
(5)

The volumetric flow rate in the film (per unit depth), Q, is given by:

$$Q = \int_{x=0}^{x=n} u_{y} dx = \int_{x=0}^{x=n} \left(\frac{1}{2} \frac{g}{v} x^{2} - \frac{gh}{v} x + U \right) dx$$
$$= \left[\frac{1}{6} \frac{g}{v} x^{3} - \frac{gh}{2v} x^{2} + Ux \right]_{0}^{h} = \frac{1}{6} \frac{g}{v} h^{3} - \frac{gh}{2v} h^{2} + Uh$$
$$\therefore Q = -\frac{gh^{3}}{3v} + Uh$$
(6)