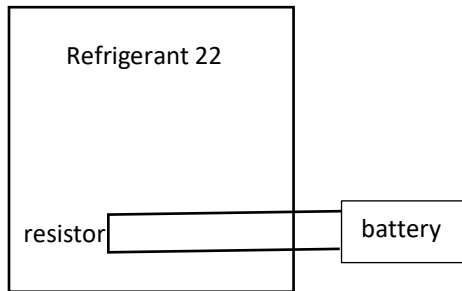


A closed, rigid tank fitted with a fine-wire electric resistor is filled with Refrigerant 22, initially at $-10\text{ }^{\circ}\text{C}$, a quality of 80%, and a volume of 0.01 m^3 . A 12 V battery provides a 5 A current to the resistor for 5 min. If the final temperature of the refrigerant is $40\text{ }^{\circ}\text{C}$, determine the heat transfer, in kJ, from the refrigerant.



SOLUTION:

The heat transferred from the refrigerant to the surroundings may be found using the First Law applied to the refrigerant (our system),

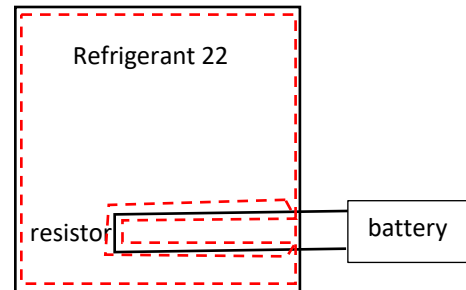
$$\Delta E_{R22} = Q_{R22}^{\text{into}} + W_{R22}^{\text{on}} \Rightarrow Q_{R22}^{\text{into}} = \Delta E_{R22} - W_{R22}^{\text{on}}, \quad (1)$$

where,

$$\Delta E_{R22} = \Delta U_{R22} = U_2 - U_1 = m(u_2 - u_1), \quad (2)$$

assuming that other forms of energy change, e.g., kinetic and potential, are negligible. Note that since the container is closed, the initial and final refrigerant masses will be the same.

Furthermore, the resistor wire is not considered to be part of the system.



The specific internal energy at state 1 is also found using the thermodynamic property tables,

$$u_1 = xu_v + (1-x)u_l, \quad (3)$$

where, at -10°C in the saturated liquid-vapor phase,

$$\begin{aligned} x &= 0.80, \\ u_v &= 223.02 \text{ kJ/kg}, \\ u_l &= 33.27 \text{ kJ/kg}, \\ \Rightarrow u_1 &= 185.07 \text{ kJ/kg}. \end{aligned}$$

The specific volume at state 1 may be found in a similar manner,

$$v_1 = xv_v + (1-x)v_l, \quad (4)$$

where,

$$\begin{aligned} x &= 0.80, \\ v_v &= 0.0652 \text{ m}^3/\text{kg}, \\ v_l &= 0.7606 \cdot 10^{-3} \text{ m}^3/\text{kg}, \\ \Rightarrow v_1 &= 0.0523 \text{ m}^3/\text{kg}. \end{aligned}$$

The mass of the refrigerant may be found from the initial state,

$$m = \frac{V}{v_1}, \quad (\text{The electrical wire volume is assumed negligible compared to the tank volume.}) \quad (5)$$

where,

$$\begin{aligned} V &= 0.01 \text{ m}^3, \\ \Rightarrow m &= 0.191 \text{ kg}. \end{aligned}$$

The specific internal energy at state 2 (after the 5 min) is found using the thermodynamic property tables for Refrigerant 22 at a temperature of 40 °C and a specific volume of,
 $v_2 = v_1$ (since the container volume and refrigerant mass remain constant). (6)

Using the two-phase liquid-vapor thermodynamic table, observe that at the final temperature of $T_2 = 40$ °C, the saturated vapor specific volume is 0.0151 m³/kg, which is smaller than the specific volume at state 2, $v_2 = 0.0523$ m³/kg. Hence, the refrigerant must be in a superheated vapor phase. Interpolating from the superheated vapor table using T_2 and v_2 ,
 $u_2 = 250.33$ kJ/kg.

Combining m , u_2 , and u_1 , Eq. (2) becomes,
 $\Delta U = 12.46$ kJ/kg.

There is no work acting on the refrigerant since the container volume remains constant and because the electrical work goes into the wire, which is not part of the system,

$$W_{\text{on R22}} = 0. \quad (7)$$

There is, however, heat that is transferred from the wire into the system. This heat may be found by applying the 1st Law to the wire. Assuming steady conditions so that the change in total energy of the wire is zero, the total heat from the wire will equal the total (electrical) work done on the wire,

$$\underbrace{\Delta E_{\text{wire}}}_{=0 \text{ (steady)}} = -Q_{\text{from wire}} + W_{\text{on wire}} \Rightarrow Q_{\text{from wire}} = W_{\text{on wire}}, \quad (8)$$

where the total work done on the wire is,

$$W_{\text{on wire}} = VI\Delta t \text{ (assuming that neither the voltage nor current change over time } \Delta t), \quad (9)$$

with,

$$V = 12 \text{ V,}$$

$$I = 5 \text{ A,}$$

$$\Delta t = 5 \text{ min} = 300 \text{ s,}$$

$$\Rightarrow W_{\text{on wire}} = 18 \text{ kJ} \Rightarrow Q_{\text{from wire}} = 18 \text{ kJ.}$$

Break the heat into the refrigerant into two heat components, one from the wire and one from the remainder of the surroundings,

$$Q_{\text{into R22}} = Q_{\text{into R22, from wire}} + Q_{\text{into R22, from elsewhere}}. \quad (10)$$

Substituting the expressions for heat, work, and energy into Eq. (1),

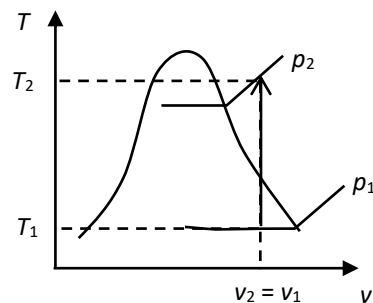
$$Q_{\text{into R22, from elsewhere}} = \Delta U - Q_{\text{into R22, from wire}}, \quad (11)$$

$$\Rightarrow Q_{\text{into R22, from elsewhere}} = -5.54 \text{ kJ.}$$

Since we're interested in the heat from the refrigerant,

$$Q_{\text{from R22, into elsewhere}} = -Q_{\text{into R22, from elsewhere}} = 5.54 \text{ kJ.} \quad (12)$$

The process and states are shown schematically in the following T - v plot.



SLVM Table for R22 (from Moran et al., 8th ed., Wiley).

Tables in SI Units 937

TABLE A-7

Pressure Conversions:
 1 bar = 0.1 MPa
 = 10² kPa

Properties of Saturated Refrigerant 22 (Liquid-Vapor): Temperature Table

Temp. °C	Press. bar	Specific Volume m ³ /kg		Internal Energy kJ/kg		Enthalpy kJ/kg			Entropy kJ/kg · K		Temp. °C
		Sat. Liquid <i>v_f</i> × 10 ³	Sat. Vapor <i>v_g</i>	Sat. Liquid <i>u_f</i>	Sat. Vapor <i>u_g</i>	Sat. Liquid <i>h_f</i>	Evap. <i>h_{fg}</i>	Sat. Vapor <i>h_g</i>	Sat. Liquid <i>s_f</i>	Sat. Vapor <i>s_g</i>	
-60	0.3749	0.6833	0.5370	-21.57	203.67	-21.55	245.35	223.81	-0.0964	1.0547	-60
-50	0.6451	0.6966	0.3239	-10.89	207.70	-10.85	239.44	228.60	-0.0474	1.0256	-50
-45	0.8290	0.7037	0.2564	-5.50	209.70	-5.44	236.39	230.95	-0.0235	1.0126	-45
-40	1.0522	0.7109	0.2052	-0.07	211.68	0.00	233.27	233.27	0.0000	1.0005	-40
-36	1.2627	0.7169	0.1730	4.29	213.25	4.38	230.71	235.09	0.0186	0.9914	-36
-32	1.5049	0.7231	0.1468	8.68	214.80	8.79	228.10	236.89	0.0369	0.9828	-32
-30	1.6389	0.7262	0.1355	10.88	215.58	11.00	226.77	237.78	0.0460	0.9787	-30
-28	1.7819	0.7294	0.1252	13.09	216.34	13.22	225.43	238.66	0.0551	0.9746	-28
-26	1.9345	0.7327	0.1159	15.31	217.11	15.45	224.08	239.53	0.0641	0.9707	-26
-22	2.2698	0.7393	0.0997	19.76	218.62	19.92	221.32	241.24	0.0819	0.9631	-22
-20	2.4534	0.7427	0.0926	21.99	219.37	22.17	219.91	242.09	0.0908	0.9595	-20
-18	2.6482	0.7462	0.0861	24.23	220.11	24.43	218.49	242.92	0.0996	0.9559	-18
-16	2.8547	0.7497	0.0802	26.48	220.85	26.69	217.05	243.74	0.1084	0.9525	-16
-14	3.0733	0.7533	0.0748	28.73	221.58	28.97	215.59	244.56	0.1171	0.9490	-14
-12	3.3044	0.7569	0.0698	31.00	222.30	31.25	214.11	245.36	0.1258	0.9457	-12
-10	3.5485	0.7606	0.0652	33.27	223.02	33.54	212.62	246.15	0.1345	0.9424	-10
-8	3.8062	0.7644	0.0610	35.54	223.73	35.83	211.10	246.93	0.1431	0.9392	-8
-6	4.0777	0.7683	0.0571	37.83	224.43	38.14	209.56	247.70	0.1517	0.9361	-6
-4	4.3638	0.7722	0.0535	40.12	225.13	40.46	208.00	248.45	0.1602	0.9330	-4
-2	4.6647	0.7762	0.0501	42.42	225.82	42.78	206.41	249.20	0.1688	0.9300	-2
0	4.9811	0.7803	0.0470	44.73	226.50	45.12	204.81	249.92	0.1773	0.9271	0
2	5.3133	0.7844	0.0442	47.04	227.17	47.46	203.18	250.64	0.1857	0.9241	2
4	5.6619	0.7887	0.0415	49.37	227.83	49.82	201.52	251.34	0.1941	0.9213	4
6	6.0275	0.7930	0.0391	51.71	228.48	52.18	199.84	252.03	0.2025	0.9184	6
8	6.4105	0.7974	0.0368	54.05	229.13	54.56	198.14	252.70	0.2109	0.9157	8
10	6.8113	0.8020	0.0346	56.40	229.76	56.95	196.40	253.35	0.2193	0.9129	10
12	7.2307	0.8066	0.0326	58.77	230.38	59.35	194.64	253.99	0.2276	0.9102	12
16	8.1268	0.8162	0.0291	63.53	231.59	64.19	191.02	255.21	0.2442	0.9048	16
20	9.1030	0.8263	0.0259	68.33	232.76	69.09	187.28	256.37	0.2607	0.8996	20
24	10.164	0.8369	0.0232	73.19	233.87	74.04	183.40	257.44	0.2772	0.8944	24
28	11.313	0.8480	0.0208	78.09	234.92	79.05	179.37	258.43	0.2936	0.8893	28
32	12.556	0.8599	0.0186	83.06	235.91	84.14	175.18	259.32	0.3101	0.8842	32
36	13.897	0.8724	0.0168	88.08	236.83	89.29	170.82	260.11	0.3265	0.8790	36
40	15.341	0.8858	0.0151	93.18	237.66	94.53	166.25	260.79	0.3429	0.8738	40
45	17.298	0.9039	0.0132	99.65	238.59	101.21	160.24	261.46	0.3635	0.8672	45
50	19.433	0.9238	0.0116	106.26	239.34	108.06	153.84	261.90	0.3842	0.8603	50
60	24.281	0.9705	0.0089	120.00	240.24	122.35	139.61	261.96	0.4264	0.8455	60

$v_f = (\text{table value})/1000$

SHV Table for R22 (from Moran et al., 8th ed., Wiley)

(Continued)

T °C	v m ³ /kg	u kJ/kg	h kJ/kg	s kJ/kg · K	v m ³ /kg	u kJ/kg	h kJ/kg	s kJ/kg · K
$p = 2.5 \text{ bar} = 0.25 \text{ MPa}$ ($T_{\text{sat}} = -19.51^\circ\text{C}$)				$p = 3.0 \text{ bar} = 0.30 \text{ MPa}$ ($T_{\text{sat}} = -14.66^\circ\text{C}$)				
Sat.	0.09097	219.55	242.29	0.9586	0.07651	221.34	244.29	0.9502
-15	0.09303	222.03	245.29	0.9703	0.07833	223.96	247.46	0.9623
-10	0.09528	224.79	248.61	0.9831	0.08025	226.78	250.86	0.9751
-5	0.09751	227.55	251.93	0.9956	0.08214	229.61	254.25	0.9876
0	0.09971	230.33	255.26	1.0078	0.08400	232.44	257.64	0.9999
5	0.10189	233.12	258.59	1.0199	0.08585	235.28	261.04	1.0120
10	0.10405	235.92	261.93	1.0318	0.08767	238.14	264.44	1.0239
15	0.10619	238.74	265.29	1.0436	0.08949	241.01	267.85	1.0357
20	0.10831	241.58	268.66	1.0552	0.09128	243.89	271.28	1.0472
25	0.11043	244.44	272.04	1.0666	0.09307	246.80	274.72	1.0587
30	0.11253	247.31	275.44	1.0779	0.09484	249.72	278.17	1.0700
35	0.11461	250.21	278.86	1.0891	0.09660	252.66	281.64	1.0811
40	0.11669	253.13	282.30	1.1002				
$p = 3.5 \text{ bar} = 0.35 \text{ MPa}$ ($T_{\text{sat}} = -10.39^\circ\text{C}$)				$p = 4.0 \text{ bar} = 0.40 \text{ MPa}$ ($T_{\text{sat}} = -6.56^\circ\text{C}$)				
Sat.	0.06605	222.88	246.00	0.9431	0.05812	224.24	247.48	0.9370
-10	0.06619	223.10	246.27	0.9441	0.05860	225.16	248.60	0.9411
-5	0.06789	225.99	249.75	0.9572	0.06011	228.09	252.14	0.9542
0	0.06956	228.86	253.21	0.9700	0.06160	231.02	255.66	0.9670
5	0.07121	231.74	256.67	0.9825	0.06306	233.95	259.18	0.9795
10	0.07284	234.63	260.12	0.9948	0.06450	236.89	262.69	0.9918
15	0.07444	237.52	263.57	1.0069	0.06592	239.83	266.19	1.0039
20	0.07603	240.42	267.03	1.0188	0.06733	242.77	269.71	1.0158
25	0.07760	243.34	270.50	1.0305	0.06872	245.73	273.22	1.0274
30	0.07916	246.27	273.97	1.0421	0.07010	248.71	276.75	1.0390
35	0.08070	249.22	227.46	1.0535	0.07146	251.70	280.28	1.0504
40	0.08224	252.18	280.97	1.0648	0.07282	254.70	283.83	1.0616
45	0.08376	255.17	284.48	1.0759				
$p = 4.5 \text{ bar} = 0.45 \text{ MPa}$ ($T_{\text{sat}} = -3.08^\circ\text{C}$)				$p = 5.0 \text{ bar} = 0.50 \text{ MPa}$ ($T_{\text{sat}} = 0.12^\circ\text{C}$)				
Sat.	0.05189	225.45	248.80	0.9316	0.04686	226.54	249.97	0.9269
0	0.05275	227.29	251.03	0.9399	0.04810	229.52	253.57	0.9399
5	0.05411	230.28	254.63	0.9529	0.04934	232.55	257.22	0.9530
10	0.05545	233.26	258.21	0.9657	0.05056	235.57	260.85	0.9657
15	0.05676	236.24	261.78	0.9782	0.05175	238.59	264.47	0.9781
20	0.05805	239.22	265.34	0.9904	0.05293	241.61	268.07	0.9903
25	0.05933	242.20	268.90	1.0025	0.05409	244.63	271.68	1.0023
30	0.06059	245.19	272.46	1.0143	0.05523	247.66	275.28	1.0141
35	0.06184	248.19	276.02	1.0259	0.05636	250.70	278.89	1.0257
40	0.06308	251.20	279.59	1.0374	0.05748	253.76	282.50	1.0371
45	0.06430	254.23	283.17	1.0488	0.05859	256.82	286.12	1.0484
50	0.06552	257.28	286.76	1.0600	0.05969	259.90	289.75	1.0595
55	0.06672	260.34	290.36	1.0710				

SHV Table for R22 (from Moran et al., 8th ed., Wiley)

TABLE A-9
(Continued)

T °C	v m ³ /kg	u kJ/kg	h kJ/kg	s kJ/kg · K	v m ³ /kg	u kJ/kg	h kJ/kg	s kJ/kg · K
$p = 5.5 \text{ bar} = 0.55 \text{ MPa}$ ($T_{\text{sat}} = 3.08^\circ\text{C}$)				$p = 6.0 \text{ bar} = 0.60 \text{ MPa}$ ($T_{\text{sat}} = 5.85^\circ\text{C}$)				
Sat.	0.04271	227.53	251.02	0.9226	0.03923	228.44	251.98	0.9186
5	0.04317	228.72	252.46	0.9278				
10	0.04333	231.81	256.20	0.9411	0.04015	231.05	255.14	0.9299
15	0.04347	234.89	259.90	0.9540	0.04122	234.18	258.91	0.9431
20	0.04358	237.95	263.57	0.9667	0.04227	237.29	262.65	0.9560
25	0.04368	241.01	267.23	0.9790	0.04330	240.39	266.37	0.9685
30	0.04375	244.07	270.88	0.9912	0.04431	243.49	270.07	0.9808
35	0.04382	247.13	274.53	1.0031	0.04530	246.58	273.76	0.9929
40	0.05086	250.20	278.17	1.0148	0.04628	249.68	277.45	1.0048
45	0.05190	253.27	281.82	1.0264	0.04724	252.78	281.13	1.0164
50	0.05293	256.36	285.47	1.0378	0.04820	255.90	284.82	1.0279
55	0.05394	259.46	289.13	1.0490	0.04914	259.02	288.51	1.0393
60	0.05495	262.58	292.80	1.0601	0.05008	262.15	292.20	1.0504
$p = 7.0 \text{ bar} = 0.70 \text{ MPa}$ ($T_{\text{sat}} = 10.91^\circ\text{C}$)				$p = 8.0 \text{ bar} = 0.80 \text{ MPa}$ ($T_{\text{sat}} = 15.45^\circ\text{C}$)				
Sat.	0.03371	230.04	253.64	0.9117	0.02953	231.43	255.05	0.9056
15	0.03451	232.70	256.86	0.9229				
20	0.03547	235.92	260.75	0.9363	0.03033	234.47	258.74	0.9182
25	0.03639	239.12	264.59	0.9493	0.03118	237.76	262.70	0.9315
30	0.03730	242.29	268.40	0.9619	0.03202	241.04	266.66	0.9448
35	0.03819	245.46	272.19	0.9743	0.03283	244.28	270.54	0.9574
40	0.03906	248.62	275.96	0.9865	0.03363	247.52	274.42	0.9700
45	0.03992	251.78	279.72	0.9984	0.03440	250.74	278.26	0.9821
50	0.04076	254.94	283.48	1.0101	0.03517	253.96	282.10	0.9941
55	0.04160	258.11	287.23	1.0216	0.03592	257.18	285.92	1.0058
60	0.04242	261.29	290.99	1.0330	0.03667	260.40	289.74	1.0174
65	0.04324	264.48	294.75	1.0442	0.03741	263.64	293.56	1.0287
70	0.04405	267.68	298.51	1.0552	0.03814	266.87	297.38	1.0400
$p = 9.0 \text{ bar} = 0.90 \text{ MPa}$ ($T_{\text{sat}} = 19.59^\circ\text{C}$)				$p = 10.0 \text{ bar} = 1.00 \text{ MPa}$ ($T_{\text{sat}} = 23.40^\circ\text{C}$)				
Sat.	0.02623	232.64	256.25	0.9001	0.02358	233.71	257.28	0.8952
20	0.02630	232.92	256.59	0.9013				
30	0.02789	239.73	264.83	0.9289	0.02457	238.34	262.91	0.9139
40	0.02939	246.37	272.82	0.9549	0.02598	245.18	271.17	0.9407
50	0.03082	252.95	280.68	0.9795	0.02732	251.90	279.22	0.9660
60	0.03219	259.49	288.46	1.0033	0.02860	258.56	287.15	0.9902
70	0.03353	266.04	296.21	1.0262	0.02984	265.19	295.03	1.0135
80	0.03483	272.62	303.96	1.0484	0.03104	271.84	302.88	1.0361
90	0.03611	279.23	311.73	1.0701	0.03221	278.52	310.74	1.0580
100	0.03736	285.90	319.53	1.0913	0.03337	285.24	318.61	1.0794
110	0.03860	292.63	327.37	1.1120	0.03450	292.02	326.52	1.1003
120	0.03982	299.42	335.26	1.1323	0.03562	298.85	334.46	1.1207
130	0.04103	306.28	343.21	1.1523	0.03672	305.74	342.46	1.1408
140	0.04223	313.21	351.22	1.1719	0.03781	312.70	350.51	1.1605
150	0.04342	320.21	359.29	1.1912	0.03889	319.74	358.63	1.1790

Pressure Conversions:
1 bar = 0.1 MPa
= 10² kPa