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Formation Control of the MAXIM L₂ Libration Orbit Mission

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Agenda



- MAXIM Introduction
- MAXIM Formation
- Formation Assumptions
- Formation Definition
- Control Discrete and Continuous
- Results
- Summary

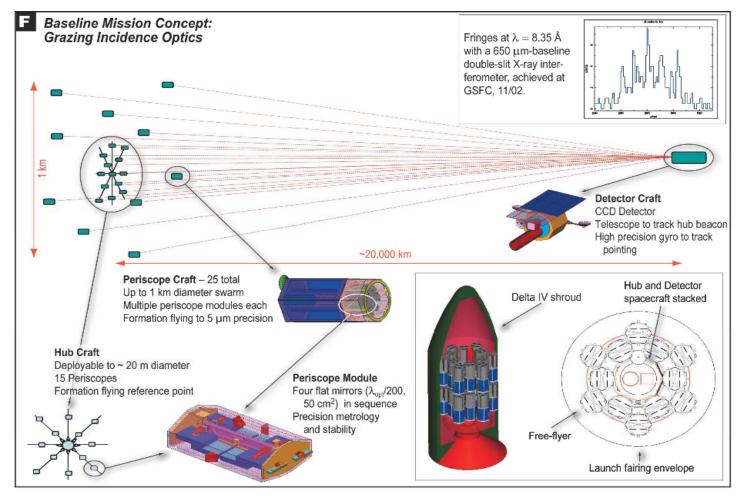


MAXIM Overview



The MAXIM concept for NASA's Black Hole Imager mission utilizes interferometric techniques at the short wavelengths of X-rays

> Very long optical baselines are needed to achieve high-precision angular resolution images



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MAXIM Formation Overview



➢ Multiple free-flying spacecraft comprise a sparse aperture providing collecting area of ~ 1000cm².

> Images are generated through interference patterns gathered from the multiple satellites housing the optical elements that form the aperture.

> The interference patterns or fringes are observed only if the path lengths are controlled to great precision.

> The challenge is to control this path length in the presence of environmental and spacecraft disturbances driving the need for active control systems.

> We focus on the dynamics and control of formation flight in a full ephemeris modeling of the libration orbit to incorporate all gravitational perturbations and solar radiation pressure.

> Analysis focuses on amount and duration of the control effort versus science observation requirements as measured in the formation optics plane





✓ MAXIM formation components;

Hub (1.3 x 2 meters , 331kg) , Freeflyer (periscope) (1.3 x 2 meters, 304kg) , and the Detector (varying area 1.9 m² to 5.6 m² , 619kg)

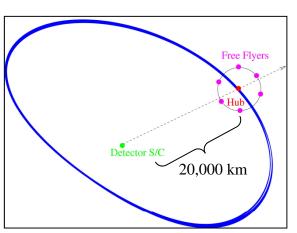
- ✓ Optics Plane:
 - Hub and Freeflyers form a physical configuration perpendicular to detector-hub line of sight (LOS) to a target.
 - Associates physical configuration to science requirements derived from a Fourier transform of the image plane, the UV plane.
- ✓ Observation duration is 100,000 secs
- ✓ Controller options:
 - •Off during observation and on to realign and maintain the formation
 - Continuously on during observations
- ✓ Inertial target of 45⁰ elevation and 45⁰ azimuth
- ✓ Tolerance of radial distance of a Freeflyer from Hub less than 5 microns
- ✓ Detector at 20,000km, six freeflyers at the maximum nominal radial distance of 500 meters from the Hub.

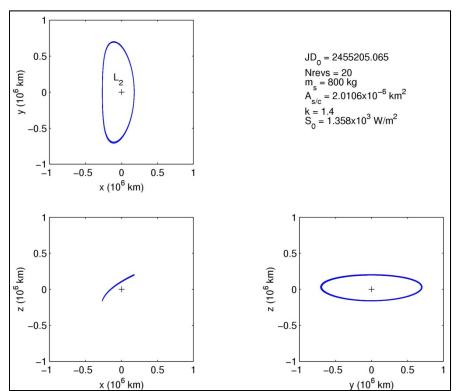




- MAXIM L₂ libration orbit is a typical mission
- $A_v = 700,000 \text{ km}$ and $A_z = 200,000 \text{ km}$
- Halo orbit computed with a full Ephemeris model
 - ✓ Sun, Earth, Moon point mass
 - ✓ Solar Radiation Pressure

• Hub follows Halo orbit





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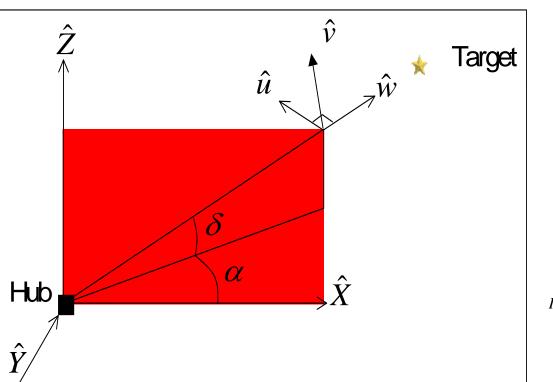
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The MAXIM hub spacecraft is located at the X,Y,Z origin and the angles α , δ provide the alignment toward the target. $\hat{w} = C C_s \hat{X} + S C_s \hat{Y} + S_s \hat{X}$



$$\hat{w} = C_{\alpha}C_{\delta}\hat{X} + S_{\alpha}C_{\delta}\hat{Y} + S_{\delta}\hat{Z}$$
$$\hat{u} = \frac{\hat{Z} \times \hat{w}}{|\hat{z} - z|}$$

 $\left| \hat{Z} \times \hat{w} \right|$

 $\hat{v} = \hat{w} \times \hat{u}$

Direction Cosines for conversion between Optics frame and Inertial Frame

$${}^{I}C^{U} = \begin{bmatrix} -S_{\alpha} & -C_{\alpha}S_{\delta} & C_{\alpha}C_{\delta} \\ C_{\alpha} & -S_{\alpha}S_{\delta} & S_{\alpha}C_{\delta} \\ 0 & C_{\delta} & S_{\delta} \end{bmatrix}$$



> Our investigation takes a global view of the large-scale formation flying problem.

Previous Research:

• Near Earth - minimized gravitational perturbation - no close tracking of a reference solution - or use of non-linear (adaptive) 2-body problems

• Multi-body systems - CRTBP only or controller effectiveness is demonstrated relative to the linear dynamics, not the full nonlinear system -Evolution approximated from the linear dynamics of the integrated lissajous trajectory

• Naturally occurring formations derived from center manifold analysis, as well as a discrete impulsive control approach to maintain a prescribed formation plane

Continuous control approach

Obtain a rough analytical approximation of center manifold motion and determine how continuous optimal control and exact feedback linearization compares, in terms of cost, to the discrete station-keeping approach.



MAXIM Control Strategies



• Previous work demonstrates the efficiency and cost effectiveness of both input feedback linearization (IFL) and output feedback linearization (OFL) methods for formation control in the CRTBP.

• A linear quadratic regulator (LQR), derived from optimal control theory, yields essentially an identical error response and control acceleration history as the IFL approach.

- IFL controller is computationally much less intensive and, by comparison, conceptually simple.
- We address the properties of the IFL controller in defining the MAXIM formation control
- Analysis of position deviation of freeflyer or detector wrt Hub
- For a comparison, a discrete stationkeeping control approach is devised to force the orientation of the formation plane to remain fixed inertially.



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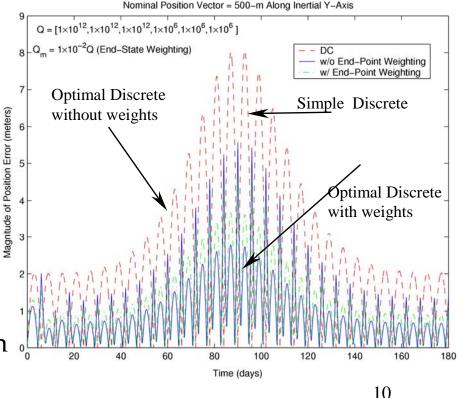
MAXIM Discrete Control



- Accuracy of formation maintenance
- •Simple DC can maintain formation
- Discrete LQR yields optimal magnitude of differential control impulse
- Simple: Target the end state
 Φ = STM
- δ = state perturbation
- Δv_0 = Impulsive ΔV at beginning
- Discrete Optimal Control: (Q_m) Weighted quadratic of end state error
- (Q) Weighted quadratic of state deviation along path
- •Simple has greatest error along path

$$\begin{bmatrix} \delta \overline{r_1} \\ \delta \overline{v_1}^- \end{bmatrix} = \Phi(t_1, t_0) \begin{bmatrix} \delta \overline{r_0} \\ \delta \overline{v_0}^+ \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} \delta \overline{r_0} \\ \delta \overline{v_0}^- + \Delta \overline{v_0} \end{bmatrix}$$

$$\Delta \overline{v}_0 = B^{-1} \left(\delta \overline{r}_1 - A \delta \overline{r}_0 \right) - \delta \overline{v}_0^{-1}$$





MAXIM Nominal Motion and Determination of Vehicle Position Relative to Optics-Frame



The nominal motion is in the local (spherical) coordinates while the control effort is formulated in the inertial focal frame.

 $\overline{r}^{HD_i} = r\hat{d}_1$ Freeflyer / Detector Kinematics are ${}^{U}\dot{\overline{r}}^{HD_{i}} = \dot{r}\hat{d}_{1} + r\dot{v}C_{\varepsilon}\hat{d}_{2} + r\dot{\varepsilon}\hat{d}_{3}$ written as $\hat{d}_1 = C_{\varepsilon}C_{\nu}\hat{u} + C_{\varepsilon}S_{\nu}\hat{v} + S_{\varepsilon}\hat{w}$ $v = \tan^{-1}\left(\frac{\tilde{z}}{\tilde{y}}\right) \quad \varepsilon = \tan^{-1}\left(\frac{\tilde{x}}{\sqrt{\tilde{y}^2 + \tilde{z}^2}}\right)$ Cartesian coordinates to Free Flyer (D_i) spherical: SO $\tilde{x} = rC_v C_\varepsilon$ NOMINAL MOTION: FF₁: $\nu^{\circ} = 0^{\circ}$, $\varepsilon^{\circ} = 0^{\circ}$, $|\overline{r}_w| = 500 \text{ m}$ $\tilde{y} = rS_{v}C_{\varepsilon}$ V FF₂: $v^{\circ} = 60^{\circ}, \quad \varepsilon^{\circ} = 0^{\circ}, \quad |\overline{r}_w| = 500 \text{ m}$ Hub (H) û FF₃: $\nu^{\circ} = 120^{\circ}, \ \varepsilon^{\circ} = 0^{\circ}, \ |\overline{r_w}| = 500 \text{ m}$ $\tilde{z} = rS_{c}$ FF₄: $v^{\circ} = 180^{\circ}, \varepsilon^{\circ} = 0^{\circ}, |\overline{r}_w| = 500 \text{ m}$ $\dot{\tilde{x}} = \dot{r}C_{v}C_{\varepsilon} - r\dot{v}S_{v}C_{\varepsilon} - r\dot{\varepsilon}C_{v}S_{\varepsilon}$ FF₅: $v^{\circ} = 240^{\circ}, \ \varepsilon^{\circ} = 0^{\circ}, \ |\overline{r}_w| = 500 \text{ m}$ FF₆: $\nu^{\circ} = 300^{\circ}, \varepsilon^{\circ} = 0^{\circ}, |\overline{r}_w| = 500 \text{ m}$ $\dot{\tilde{y}} = \dot{r}S_{v}C_{\varepsilon} + r\dot{v}C_{v}C_{\varepsilon} - r\dot{\varepsilon}S_{v}S_{\varepsilon}$ Detector: $v^{\circ} = 0^{\circ}$, $\varepsilon^{\circ} = -90^{\circ}$, $|\overline{r_w}| = 20,000 \text{ km}$ $\dot{\tilde{z}} = \dot{r}S_{\varepsilon} + r\dot{\varepsilon}C_{\varepsilon}$ Detector

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Control of Equations of Motion (EOM) in Ephemeris Frame Wrt Earth (P₂)

MAXIM IFL Controller Development

o EOM for Freeflyer/detector ${}^{I}\ddot{\overline{r}}_{I}{}^{P_{2}D_{i}} = \overline{f}\left(\overline{r}_{I}{}^{P_{2}D_{i}}, {}^{I}\dot{\overline{r}}_{I}{}^{P_{2}D_{i}}\right) + \overline{u}_{I}{}^{(D_{i})}(t)$ o EOM for Hub ${}^{I}\ddot{\overline{r}}_{I}{}^{P_{2}H} = \overline{f}\left(\overline{r}_{I}{}^{P_{2}H}, {}^{I}\dot{\overline{r}}_{I}{}^{P_{2}H}\right)$

o Controller is selected as type of response as a critical damped

o Control in the local frame ${}^{U}\ddot{\overline{r}}_{U}{}^{HD_{i}} = \left\{{}^{U}C^{I}\right\}\Delta\overline{f}_{I} + \left\{{}^{U}C^{I}\right\}\overline{u}_{I}{}^{(D_{i})}(t) = \left\{{}^{U}C^{I}\right\}\Delta\overline{f}_{I} + \tilde{u}^{(D_{i})}(t)$

o Controller eliminates system dynamics terms yields critical response control $\tilde{u}^{(D_i)}(t) = -\left\{ {}^{U}C^{I} \right\} \Delta \overline{f}_{I}^{(D_i)} - 2\omega_n \left({}^{U} \dot{\overline{r}}_{U} {}^{HD_i} - \dot{\overline{r}}^* \right) - \omega_n {}^{2} \left(\overline{\overline{r}}_{U} {}^{HD_i} - \overline{\overline{r}}^* \right)$

$${}^{I} \overline{\overrightarrow{r}_{I}}{}^{HD_{i}} = \Delta \overline{f}_{I} + \overline{u}_{I}^{(D_{i})}(t) \longrightarrow \left\{ {}^{I}C^{U} \right\} {}^{U} \overline{\overrightarrow{r}_{U}}{}^{HD_{i}} = \Delta \overline{f}_{I} + \overline{u}_{I}^{(D_{i})}(t)$$

o Once control determined in optics frame, rotate into inertial frame for controller $\overline{u}_{I}^{(D_{i})}(t) = \{{}^{I}C^{U}\} \tilde{u}^{(D_{i})}(t)$

(Note: Full state feedback for IFL and no constraints) 12

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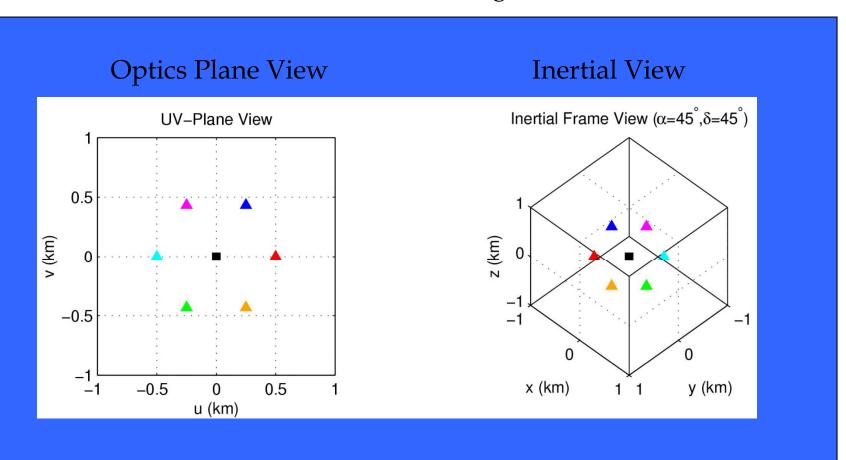
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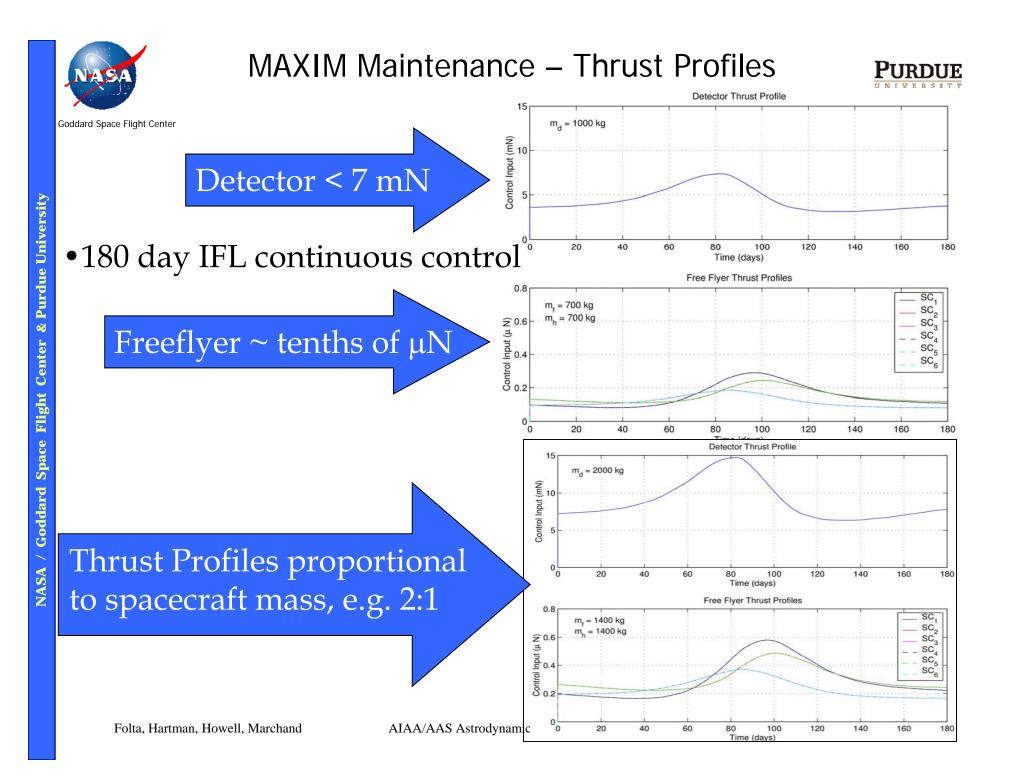


MAXIM Freeflyer Placement



Freeflyers at a maximum 500 meters from hub evenly spaced in azimuth at 60 degrees





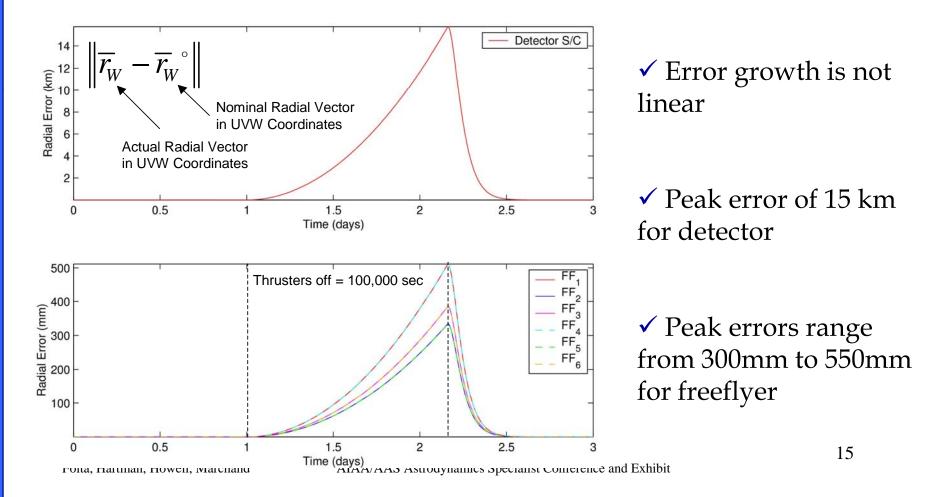


MAXIM Maintenance and Recovery



• Maintenance for 1 day

- Control off during observation of 100,000 seconds
- Increase in radial errors of detector and freeflyer
- Recovery back to original positions in ¹/₂ day



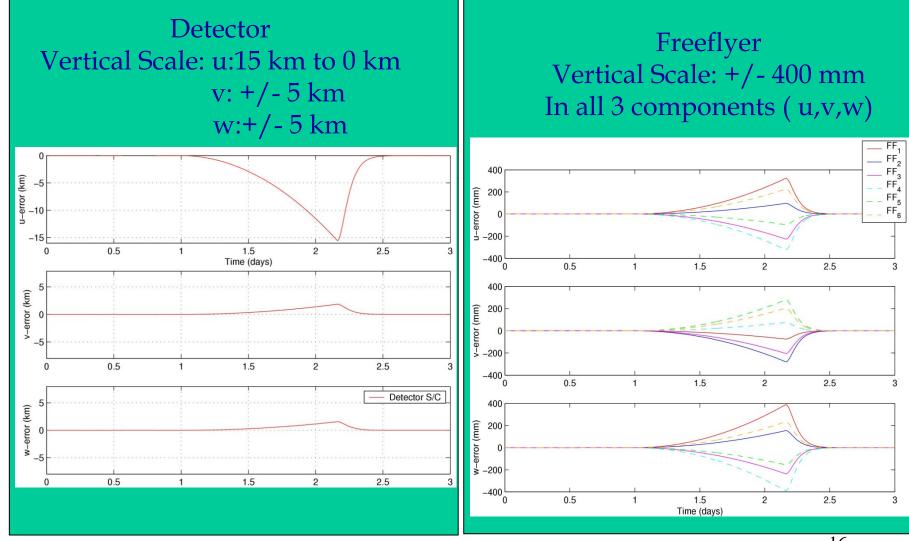


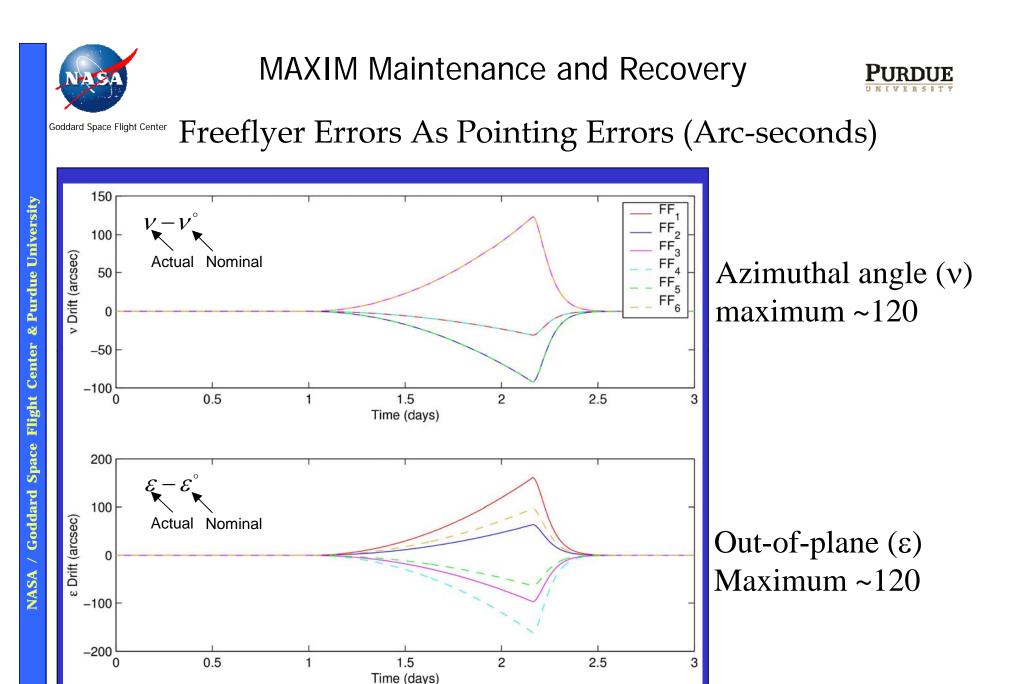
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MAXIM Maintenance and Recovery



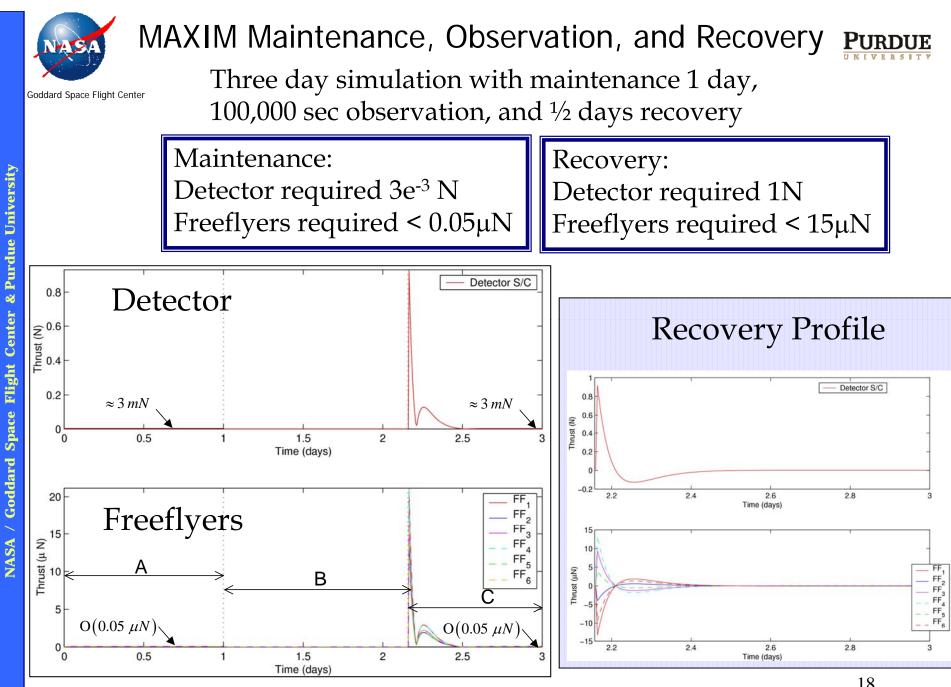
Deviation in the Optics Plane During Observation With Control Off





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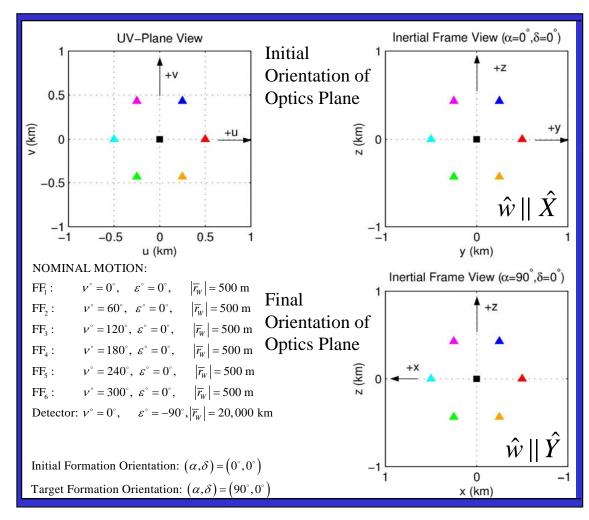
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MAXIM Reorientation



- •90 degrees rotation about the z-axis
- Target initially along the inertial x-axis
- •x-axis reoriented into y-axis direction • Elevation angle set to zero

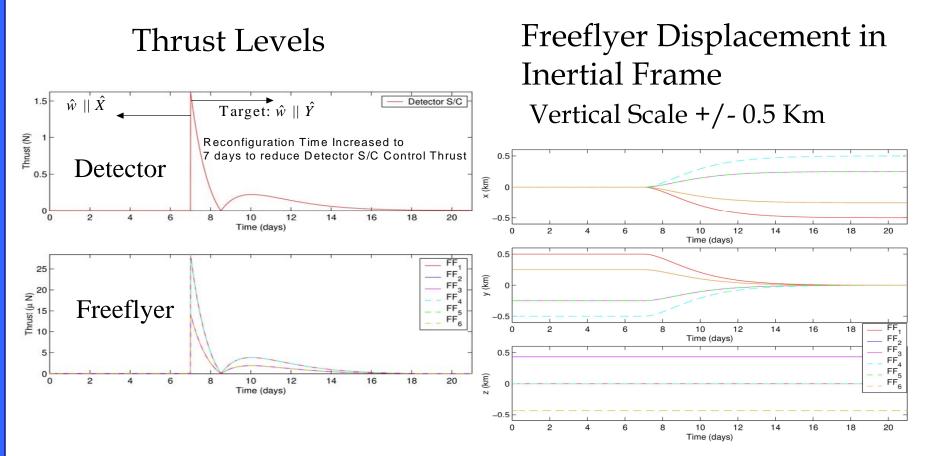


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MAXIM Reorientation

- •7 day Simulation
- Detector ~ 1.5 N
- Freeflyer ~ $2.5 \ \mu N$





Summary



•Two Approaches, Discrete and Continuous, Were Investigated for the Control of the Maxim Formation.

Simple or Optimal Discrete or by Input Feedback Linearization (IFL) Control.
✓ Discrete Control Approaches Continuous Time Interval Effort.
✓ IFL Continuous Control Combines the Effect of Annihilating the Environmental Dynamics While Adding a Specific User-defined Critically Damped Response

- The Total Maintenance Control Effort Requires
 ✓ Detector Thrust Level that Ranges From 4 mN to 7 mN
 ✓ Freeflyer Thrust Levels of 0.1 μN to 0.3 μN.
- Formation Recovery
 - ✓ Detector Thrust Less than 1 N
 - \checkmark Freeflyers Less than 15 μN
- These Efforts Do Not Include Navigation or Maneuver Errors or Navigation Measurement Updates.
- The Challenge Is Propulsion System Implementation and Required Power Levels as Current Propulsion Technology Can Meet Minimum Thrust Levels 21

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