# Formation Control of the MAXI M $\mathbf{L}_{2}$ Libration Orbit Mission 

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## Agenda

- MAXIM Introduction
- MAXIM Formation
- Formation Assumptions
- Formation Definition
- Control - Discrete and Continuous
- Results
- Summary
> The MAXIM concept for NASA's Black Hole Imager mission utilizes interferometric techniques at the short wavelengths of X-rays
$>$ Very long optical baselines are needed to achieve high-precision angular resolution images

$>$ Multiple free-flying spacecraft comprise a sparse aperture providing collecting area of $\sim 1000 \mathrm{~cm}^{2}$.
$>$ Images are generated through interference patterns gathered from the multiple satellites housing the optical elements that form the aperture.
$>$ The interference patterns or fringes are observed only if the path lengths are controlled to great precision.
$>$ The challenge is to control this path length in the presence of environmental and spacecraft disturbances driving the need for active control systems.
$>$ We focus on the dynamics and control of formation flight in a full ephemeris modeling of the libration orbit to incorporate all gravitational perturbations and solar radiation pressure.
$>$ Analysis focuses on amount and duration of the control effort versus science observation requirements as measured in the formation optics plane
$\checkmark$ MAXIM formation components;
Hub ( $1.3 \times 2$ meters , 331 kg ) , Freeflyer (periscope) ( $1.3 \times 2$ meters, 304 kg ), and the Detector (varying area $1.9 \mathrm{~m}^{2}$ to $5.6 \mathrm{~m}^{2}, 619 \mathrm{~kg}$ )
$\checkmark$ Optics Plane:
-Hub and Freeflyers form a physical configuration perpendicular to detector-hub line of sight (LOS) to a target.
- Associates physical configuration to science requirements derived from a Fourier transform of the image plane, the UV plane.
$\checkmark$ Observation duration is 100,000 secs
$\checkmark$ Controller options:
- Off during observation and on to realign and maintain the formation
- Continuously on during observations
$\checkmark$ Inertial target of $45^{\circ}$ elevation and $45^{\circ}$ azimuth
$\checkmark$ Tolerance of radial distance of a Freeflyer from Hub less than 5 microns
$\checkmark$ Detector at $20,000 \mathrm{~km}$, six freeflyers at the maximum nominal radial distance of 500 meters from the Hub.
- MAXIM $L_{2}$ libration orbit is a typical mission
- $A_{y}=700,000 \mathrm{~km}$ and $A_{z}=200,000 \mathrm{~km}$
- Halo orbit computed with a full Ephemeris model
$\checkmark$ Sun, Earth, Moon point mass
$\checkmark$ Solar Radiation Pressure
- Hub follows Halo orbit


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The MAXIM hub spacecraft is located at the $X, Y, Z$ origin and the angles $\alpha, \delta$ provide the alignment toward the target.

$$
\begin{aligned}
& \hat{w}=C_{\alpha} C_{\delta} \hat{X}+S_{\alpha} C_{\delta} \hat{Y}+S_{\delta} \hat{Z} \\
& \hat{u}=\frac{\hat{Z} \times \hat{w}}{|\hat{Z} \times \hat{w}|} \\
& \hat{v}=\hat{w} \times \hat{u}
\end{aligned}
$$

Direction Cosines for conversion between Optics frame and Inertial Frame

$$
{ }^{I} C^{U}=\left[\begin{array}{ccc}
-S_{\alpha} & -C_{\alpha} S_{\delta} & C_{\alpha} C_{\delta} \\
C_{\alpha} & -S_{\alpha} S_{\delta} & S_{\alpha} C_{\delta} \\
0 & C_{\delta} & S_{\delta}
\end{array}\right]
$$

$>$ Our investigation takes a global view of the large-scale formation flying problem.

Previous Research:

- Near Earth - minimized gravitational perturbation - no close tracking of a reference solution - or use of non-linear (adaptive) 2-body problems
- Multi-body systems - CRTBP only or controller effectiveness is demonstrated relative to the linear dynamics, not the full nonlinear system Evolution approximated from the linear dynamics of the integrated lissajous trajectory
- Naturally occurring formations derived from center manifold analysis, as well as a discrete impulsive control approach to maintain a prescribed formation plane
$>$ Continuous control approach
Obtain a rough analytical approximation of center manifold motion and determine how continuous optimal control and exact feedback linearization compares, in terms of cost, to the discrete station-keeping approach.
- Previous work demonstrates the efficiency and cost effectiveness of both input feedback linearization (IFL) and output feedback linearization (OFL) methods for formation control in the CRTBP.
- A linear quadratic regulator (LQR), derived from optimal control theory, yields essentially an identical error response and control acceleration history as the IFL approach.
- IFL controller is computationally much less intensive and, by comparison, conceptually simple.
- We address the properties of the IFL controller in defining the MAXIM formation control
- Analysis of position deviation of freeflyer or detector wrt Hub
- For a comparison, a discrete stationkeeping control approach is devised to force the orientation of the formation plane to remain fixed inertially.
- Accuracy of formation maintenance
- Simple DC can maintain formation
- Discrete LQR yields optimal magnitude $\quad \Delta \bar{v}_{0}=B^{-1}\left(\delta \bar{r}_{1}-A \delta \bar{r}_{0}\right)-\delta \bar{v}_{0}^{-}$ of differential control impulse
- Simple: Target the end state $\Phi=$ STM
$\delta=$ state perturbation
$\Delta \nu_{0}=$ Impulsive $\Delta \mathrm{V}$ at beginning
- Discrete Optimal Control:
$\left(Q_{m}\right)$ Weighted quadratic of end state error
(Q) Weighted quadratic of state deviation along path
- Simple has greatest error along path


# MAXIM Nominal Motion and Determination of Vehicle Position Relative to Optics-Frame 

The nominal motion is in the local (spherical) coordinates while the control effort is formulated in the inertial focal frame.

$$
\begin{array}{ll}
\text { Freeflyer / Detector } & \bar{r}^{H D_{i}}=r \hat{d}_{1} \\
\text { Kinematics are } & U \dot{\bar{r}}^{H D_{i}}=\dot{r} \hat{d}_{1}+r \dot{v} C_{\varepsilon} \hat{d}_{2}+r \dot{\varepsilon} \hat{d}_{3} \\
\text { written as } & \hat{d}_{1}=C_{\varepsilon} C_{v} \hat{u}+C_{\varepsilon} S_{v} \hat{v}+S_{\varepsilon} \hat{w}
\end{array}
$$

Cartesian coordinates to spherical:

$$
\begin{gathered}
\tilde{x}=r C_{V} C_{\varepsilon} \\
\tilde{y}=r S_{\nu} C_{\varepsilon} \\
\tilde{z}=r S_{\varepsilon} \\
\dot{\tilde{x}}=\dot{r} C_{V} C_{\varepsilon}-r \dot{\nu} S_{\nu} C_{\varepsilon}-r \dot{\varepsilon} C_{\nu} S_{\varepsilon} \\
\dot{\tilde{y}}=\dot{r} S_{V} C_{\varepsilon}+r \dot{\nu} C_{V} C_{\varepsilon}-r \dot{\varepsilon} S_{\nu} S_{\varepsilon} \\
\dot{\tilde{z}}=\dot{r} S_{\varepsilon}+r \dot{\varepsilon} C_{\varepsilon}
\end{gathered}
$$


o EOM for Freeflyer/detector ${ }^{\stackrel{\Gamma}{r}_{I}{ }^{P_{2} D_{i}}}=\bar{f}\left(\bar{r}_{I}^{P_{2} D_{i}},{ }^{I} \dot{\bar{r}}_{I}^{\mathcal{P}_{I} D_{i}}\right)+\bar{u}_{I}^{\left(D_{1}\right)}(t)$
o EOM for Hub

$$
{ }^{I} \ddot{\bar{P}}_{I} P_{2} H=\bar{f}\left(\bar{r}_{I}^{P_{2} H}, I_{\dot{r}_{I}}^{P_{2} H}\right)
$$

o Controller is selected as type of response as a critical damped
o Control in the local frame ${ }^{U} \ddot{\bar{r}}_{U}{ }^{H D_{i}}=\left\{{ }^{U} C^{I}\right\} \Delta \bar{f}_{I}+\left\{{ }^{U} C^{I}\right\} \bar{u}_{I}^{\left(D_{i}\right)}(t)=\left\{{ }^{U} C^{I}\right\} \Delta \bar{f}_{I}+\tilde{u}^{\left(D_{i}\right)}(t)$
o Controller eliminates system dynamics terms yields critical response control

$$
\begin{aligned}
& \tilde{u}^{\left(D_{i}\right)}(t)=-\left\{{ }^{U} C^{I}\right\} \Delta \bar{f}_{I}^{\left(D_{i}\right)}-2 \omega_{n}\left({ }^{U} \dot{\vec{r}}_{U}^{H D_{i}}-\dot{\bar{r}}^{*}\right)-\omega_{n}^{2}\left(\bar{r}_{U}^{H D_{i}}-\bar{r}^{*}\right) \\
& { }^{I} \ddot{\bar{r}}_{I}^{H D_{i}}=\Delta \bar{f}_{I}+\bar{u}_{I}^{\left(D_{i}\right)}(t) \quad \rightarrow \quad\left\{{ }^{I} C^{U}\right\}^{U} \ddot{\bar{r}}_{U}^{H D_{i}}=\Delta \bar{f}_{I}+\bar{u}_{I}^{\left(D_{i}\right)}(t)
\end{aligned}
$$

o Once control determined in optics frame, rotate into inertial frame for controller

$$
\bar{u}_{I}^{\left(D_{i}\right)}(t)=\left\{{ }^{I} C^{U}\right\} \tilde{u}^{\left(D_{i}\right)}(t)
$$

(Note: Full state feedback for IFL and no constraints)

Freeflyers at a maximum 500 meters from hub evenly spaced in azimuth at 60 degrees


MAXIM Maintenance - Thrust Profiles
Detector Thrust Profile



- 180 day IFL continuous control

Free Flyer Thrust Profiles

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    Freeflyer ~ tenths of }\mu\textrm{N
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- Maintenance for 1 day
- Control off during observation of 100,000 seconds
- Increase in radial errors of detector and freeflyer
- Recovery back to original positions in $1 / 2$ day


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## Deviation in the Optics Plane During Observation With Control Off


${ }^{\text {cousasas spere farmecanes }}$ Freeflyer Errors As Pointing Errors (Arc-seconds)


Azimuthal angle (v) maximum $\sim 120$

Out-of-plane ( $\varepsilon$ )
Maximum ~120

## MAXIM Maintenance, Observation, and Recovery Purdue

 Three day simulation with maintenance 1 day,100,000 sec observation, and $1 / 2$ days recovery Three day simulation with maintenance 1 day,
100,000 sec observation, and $1 / 2$ days recovery

| Maintenance: |
| :--- |
| Detector required $3 \mathrm{e}^{-3} \mathrm{~N}$ |
| Freeflyers required $<0.05 \mu \mathrm{~N}$ |

## Recovery:

Detector required 1 N
Freeflyers required $<15 \mu \mathrm{~N}$



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- 90 degrees rotation about the z -axis
- Target initially along the inertial x -axis
- x-axis reoriented into $y$-axis direction
- Elevation angle set to zero

- 7 day Simulation
- Detector ~ 1.5 N
- Freeflyer ~ $2.5 \mu \mathrm{~N}$

Thrust Levels



Freeflyer Displacement in Inertial Frame
Vertical Scale $+/-0.5 \mathrm{Km}$


-Two Approaches, Discrete and Continuous, Were Investigated for the Control of the Maxim Formation.

- Simple or Optimal Discrete or by Input Feedback Linearization (IFL) Control.
$\checkmark$ Discrete Control Approaches Continuous Time Interval Effort.
$\checkmark$ IFL Continuous Control Combines the Effect of Annihilating the Environmental Dynamics While Adding a Specific User-defined Critically Damped Response
- The Total Maintenance Control Effort Requires
$\checkmark$ Detector Thrust Level that Ranges From 4 mN to 7 mN
$\checkmark$ Freeflyer Thrust Levels of $0.1 \mu \mathrm{~N}$ to $0.3 \mu \mathrm{~N}$.
-Formation Recovery
$\checkmark$ Detector Thrust Less than 1 N
$\checkmark$ Freeflyers Less than $15 \mu \mathrm{~N}$
- These Efforts Do Not Include Navigation or Maneuver Errors or Navigation Measurement Updates.
- The Challenge Is Propulsion System Implementation and Required Power Levels as Current Propulsion Technology Can Meet Minimum Thrust Levels

