

#### DESIGN AND CONTROL OF FORMATIONS NEAR THE LIBRATION POINTS OF THE SUN-EARTH/MOON EPHEMERIS SYSTEM

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## **Reference Motions**

- Natural Formations
  - String of Pearls
  - Others: Identify via Floquet controller (CR3BP)
    - Quasi-Periodic Relative Orbits (2D-Torus)
    - Nearly Periodic Relative Orbits
    - Slowly Expanding Nearly Vertical Orbits
- Non-Natural Formations
  - Fixed Relative Distance and Orientation

+ Stable Manifolds

RLP

Inertial

- Fixed Relative Distance, Free Orientation
- Fixed Relative Distance & Rotation Rate
- Aspherical Configurations (Position & Rates)





## **Natural Formations**





## Natural Formations: String of Pearls





# $\begin{array}{r} \overset{\bullet}{} \overset{\bullet}{} \overset{\bullet}{} \end{array} \\ \hline \mathsf{Natural Formations:} \\ \mathsf{Quasi-Periodic Relative Orbits} \rightarrow 2-\mathsf{D Torus} \end{array}$





## Natural Formations: Nearly Periodic Relative Motion



10 Revolutions = 1,800 days



## Evolution of Nearly Vertical Orbits Along the *yz*-Plane



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## Natural Formations: Slowly Expanding Vertical Orbits



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## **Non-Natural Formations**



## PURDUE NIVERSITY Nominal Formation Keeping Cost (Configurations Fixed in the RLP Frame) $\Delta V = \int_{0}^{180 \text{ days}} \sqrt{\overline{u}^{\circ}(t) \cdot \overline{u}^{\circ}(t)} dt$





## Max./Min. Cost Formations (Configurations Fixed in the RLP Frame)



## Formation Keeping Cost Variation Along the SEM $L_1$ and $L_2$ Halo Families (Configurations Fixed in the RLP Frame)





## Discrete vs. Continuous Control



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## Discrete Control: Linear Targeter



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## Achievable Accuracy via Targeter Scheme



#### S I R **Continuous Control:** LQR vs. Input Feedback Linearization

LQR for <u>Time-Varying</u> Nominal Motions

 $\dot{\overline{x}}(t) = \begin{bmatrix} \dot{\overline{r}} & \ddot{\overline{r}} \end{bmatrix}^T = \overline{f}(t, \overline{x}(t), \overline{u}(t))$  $\rightarrow \overline{x}(0) = \overline{x}_0$  $\dot{P} = -A^{T}(t)P(t) - P(t)A(t) + P(t)B(t)R^{-1}B^{T}(t)P(t) - Q \rightarrow P(t_{f}) = 0$ 

Optimal Control Law:  

$$\overline{u}(t) = \overbrace{\overline{u}^{\circ}(t)}^{\text{Nominal Control Input}} + \begin{cases} -R^{-1}B^T P(t)(\overline{x}(t) - \overline{x}^{\circ}(t)) \\ \text{Optimal Control, Relative to Nominal, from LQR} \end{cases}$$

Input Feedback Linearization (IFL)

$$\ddot{\overline{r}}(t) = \overline{F}(\overline{r}(t)) + \overline{u}(t) \quad \blacksquare$$

$$\overline{u}(t) = -\overline{F}(\overline{r}(t)) + \overline{\overline{g}(\overline{r}(t), \overline{r}(t))}^{\text{Desired Dynamic Response}}$$

Anihilate Natural Dynamics

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 $(t), \overline{r}(t)$ 

## Dynamic Response to Injection Error $\rho = 5000 \text{ km}, \xi = 90^{\circ}, \beta = 0^{\circ}$

 $\delta \overline{x}(0) = [7 \text{ km} -5 \text{ km} 3.5 \text{ km} 1 \text{ mps} -1 \text{ mps} 1 \text{ mps}]^T$ 





## Output Feedback Linearization (Radial Distance Control)

**Formation Dynamics** 

 $\ddot{r} = \Delta \overline{f}(\overline{r}) + \overline{u}(t) \longrightarrow \text{Generalized Relative EOMs}$ 

 $y = l(\overline{r}) \longrightarrow$  Measured Output

Measured Output Response (Radial Distance)



$$h\left(\overline{r}(t), \frac{\dot{r}}{r}(t)\right) - \overline{u}(t)^{T} \overline{r}(t) = 0$$



## **Output Feedback Linearization (OFL)**

(Radial Distance Control in the Ephemeris Model)

| $y = l\left(\overline{r}, \dot{\overline{r}}\right)$ | Control Law  |
|--|--|
| r  | $\overline{u}(t) = \frac{h(\overline{r}, \dot{\overline{r}})}{r} \hat{r}$ Geometric Approach:<br>Radial inputs only  |
| r  | $\overline{u}(t) = \left\{ \frac{g\left(\overline{r}, \dot{\overline{r}}\right)}{r} - \frac{\dot{\overline{r}}^{T} \dot{\overline{r}}}{r^{2}} \right\} \overline{r} + \left(\frac{\dot{r}}{r}\right) \dot{\overline{r}} - \Delta \overline{f}(\overline{r})$ |
| $r^2$  | $\overline{u}(t) = \left\{\frac{1}{2}\frac{g(\overline{r}, \dot{\overline{r}})}{r^2} - \frac{\dot{\overline{r}}^T \dot{\overline{r}}}{r^2}\right\}\overline{r} - \Delta \overline{f}(\overline{r})$  |
| $\frac{1}{r}$  | $\overline{u}(t) = \left\{-rg\left(\overline{r}, \dot{\overline{r}}\right) - \frac{\dot{\overline{r}}^{T}\dot{\overline{r}}}{r^{2}}\right\}\overline{r} + 3\left(\frac{\dot{r}}{r}\right)\dot{\overline{r}} - \Delta\overline{f}(\overline{r})$              |

- Critically damped output response achieved in all cases
- Total  $\Delta V$  can vary significantly for these four controllers





## OFL Control of Spherical Formations Radial Dist. + Rotation Rate









## Conclusions

- Continuous Control in the Ephemeris Model:
  - Non-Natural Formations
    - LQR/IFL  $\rightarrow$  essentially identical responses & control inputs
    - IFL appears to have some advantages over LQR in this case
    - OFL  $\rightarrow$  spherical configurations + unnatural rates
    - Low acceleration levels  $\rightarrow$  Implementation Issues
- Discrete Control of Non-Natural Formations
  - Targeter Approach
    - Small relative separations  $\rightarrow$  Good accuracy
    - Large relative separations  $\rightarrow$  Require nearly continuous control
    - Extremely Small ∆V's (10<sup>-5</sup> m/sec)
- Natural Formations
  - Nearly periodic & quasi-periodic formations in the RLP frame
  - Floquet controller: numerically ID solutions + stable manifolds



## Backups



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## Targeter Maneuver Schedule



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### LQR vs. IFL (CR3BP) Control Accelerations





## IFL Response in the Ephemeris Model





## OFL Control in the Ephemeris Model









## Stability of T-Periodic Orbits

Linear Variational Equation:

 $\delta \overline{x}(t) = \Phi(t,0) \delta \overline{x}(0)$ 

 $\delta \overline{x}(t) \rightarrow$  measured relative to periodic orbit







### Eigenstructure Near Halo Orbit



Floquet Decomposition of  $\Phi(t,0)$ :

 $\Phi(t,0) = \left\{ P(t)S \right\} e^{Jt} \left\{ P(0)S \right\}^{-1}$ 

Floquet Modal Matrix:

 $E(t) = P(t)S = \Phi(t,0)E(0)e^{-Jt}$ 

Solution to Variational Eqn. in terms of Floquet Modes:

$$\delta \overline{x}(t) = \sum_{j=1}^{6} \delta \overline{x}_{j}(t) = \sum_{j=1}^{6} c_{j}(t) \overline{e}_{j}(t) = E(t)\overline{c}$$

![](_page_31_Picture_10.jpeg)

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#### Floquet Controller (Remove Unstable + 2 Center Modes)

Find  $\Delta \overline{v}$  that removes undesired response modes:

$$\sum_{j=1}^{6} \delta \overline{x}_{j} + \begin{bmatrix} 0_{3} \\ I_{3} \end{bmatrix} \Delta \overline{v} = \sum_{\substack{j=2,3,4 \\ \text{or} \\ j=2,5,6}} \left(1 + \alpha_{j}\right) \delta \overline{x}_{j}$$

Remove Modes 1, 3, and 4:

$$\begin{bmatrix} \overline{\alpha} \\ \Delta \overline{\nu} \end{bmatrix} = \begin{bmatrix} \delta \overline{x}_{2\overline{r}} & \delta \overline{x}_{5\overline{r}} & \delta \overline{x}_{6\overline{r}} & 0_3 \\ \delta \overline{x}_{2\overline{\nu}} & \delta \overline{x}_{5\overline{\nu}} & \delta \overline{x}_{6\overline{\nu}} & -I_3 \end{bmatrix}^{-1} \left( \delta \overline{x}_1 + \delta \overline{x}_3 + \delta \overline{x}_4 \right)$$

Remove Modes 1, 5, and 6:

$$\begin{bmatrix} \overline{\alpha} \\ \Delta \overline{v} \end{bmatrix} = \begin{bmatrix} \delta \overline{x}_{2\overline{r}} & \delta \overline{x}_{3\overline{r}} & \delta \overline{x}_{4\overline{r}} & 0_3 \\ \delta \overline{x}_{2\overline{v}} & \delta \overline{x}_{3\overline{v}} & \delta \overline{x}_{4\overline{v}} & -I_3 \end{bmatrix}^{-1} \left( \delta \overline{x}_1 + \delta \overline{x}_5 + \delta \overline{x}_6 \right)$$

![](_page_32_Picture_9.jpeg)

![](_page_33_Picture_0.jpeg)

## Deployment into Torus (Remove Modes 1, 5, and 6)

![](_page_33_Figure_2.jpeg)

![](_page_33_Picture_4.jpeg)

#### Deployment into Natural Orbits (Remove Modes 1, 3, and 4)

![](_page_34_Figure_2.jpeg)

![](_page_34_Picture_3.jpeg)

V Ε R SITY N **Floquet Control** (Large Formations – Example 1) y (10<sup>6</sup> km) -2∟ -2 -1 0 x (10<sup>6</sup> km) 2 1

![](_page_35_Figure_1.jpeg)

## Floquet Controller Maneuver Schedule (For Example 1)

![](_page_36_Figure_2.jpeg)

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### Nearly Periodic Formations (Inertial Perspective)

![](_page_37_Figure_2.jpeg)

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## Nearly Vertical Formations (Inertial Perspective)

![](_page_38_Figure_2.jpeg)

![](_page_38_Picture_3.jpeg)